

**TO:** Mr. Marten Walters, President, KEMWorks Technology, Inc.  
**CC:** Mr. Neville Bergin, General Manager, MINEMAKERS Limited.

**FROM:** Dr. Francisco J. Sotillo, President, PerUsa EnviroMet, Inc.

**SUBJECT:** Screen Analysis and Assays of the HPGR Head Samples for Composite A, B, and C for MPH Samples from Arruwurra Wonarah Phosphate Project–Data Analysis.

**DATE:** March 05, 2014

---

### **SUMMARY, CONCLUSIONS AND RECOMMENDATIONS**

- The analysis of the data on the particle size distributions (PSD) and screen assays of the HPGR Head Samples of Composite A, B, and C indicated that the Model prepared could predict the HPGR + Attrition Scrubbing results for MPH Phosphate Ore for Composites A and B.
- The data analysis confirmed that selective grinding occurred due to the difference in hardness of the mineral species. The data indicated the P<sub>2</sub>O<sub>5</sub> bearing minerals were the hardest, followed by SiO<sub>2</sub> bearing minerals, Al<sub>2</sub>O<sub>3</sub> bearing minerals being the softest.
- The Head Samples data supported the selected HPGR operating conditions chosen to carry out the comminution tests for Composite A and B: **40 bars of Applied Pressure and 0.77 m/s of Rolls Speed.**

### **INTRODUCTION**

Following recommendations on the report of January 27, 2014, screen analysis and assays of the Head Samples of Composites A, B, and C were carried out to validate the Model prepared to predict the results of the HPGR + Attrition Scrubbing on Composite A and B from data obtained from HPGR + Attrition Scrubbing of Composite C. Moreover, these tests were suggested to confirm the HPGR operating conditions selected to be used for Composites A and B. The following Excel Files were prepared on screen analysis of Composite A, B, and C; and screen assays of Composite A, Composite B and Composite C, respectively:

- KEMWorks-PN2069-K12013 HPGR Comp A-C Head Sizing-1.
- KEMWorks-PN2069-K12023SA20.
- KEMWorks-PN2069-K12023SA21.
- KEMWorks-PN2069-K12023SA22.

As in previous reports, a bullet form for easy following is presented in the following paragraphs.

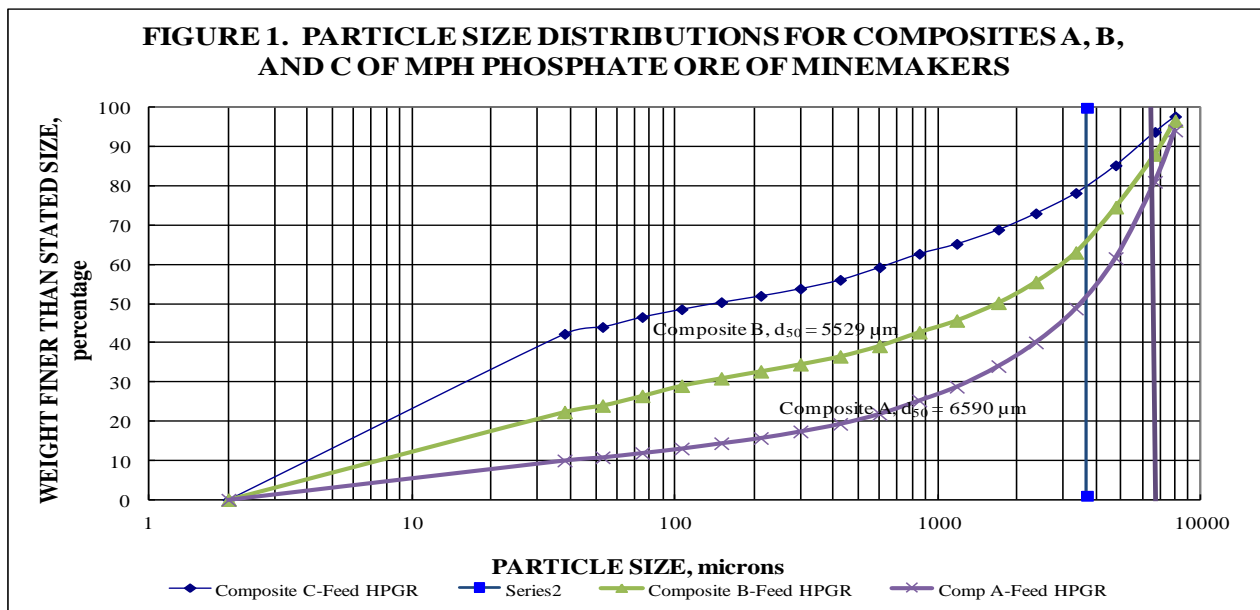
### **SCREEN ANALYSIS**

- Screen analyses of the HPGR Head Samples are presented in Figures 1 and 2, and in Table 5. The data included for completion the Head Samples chemical analysis obtained from the Screen Assays. Composite A reported 2.65% Al<sub>2</sub>O<sub>3</sub> and 22.82% P<sub>2</sub>O<sub>5</sub>,

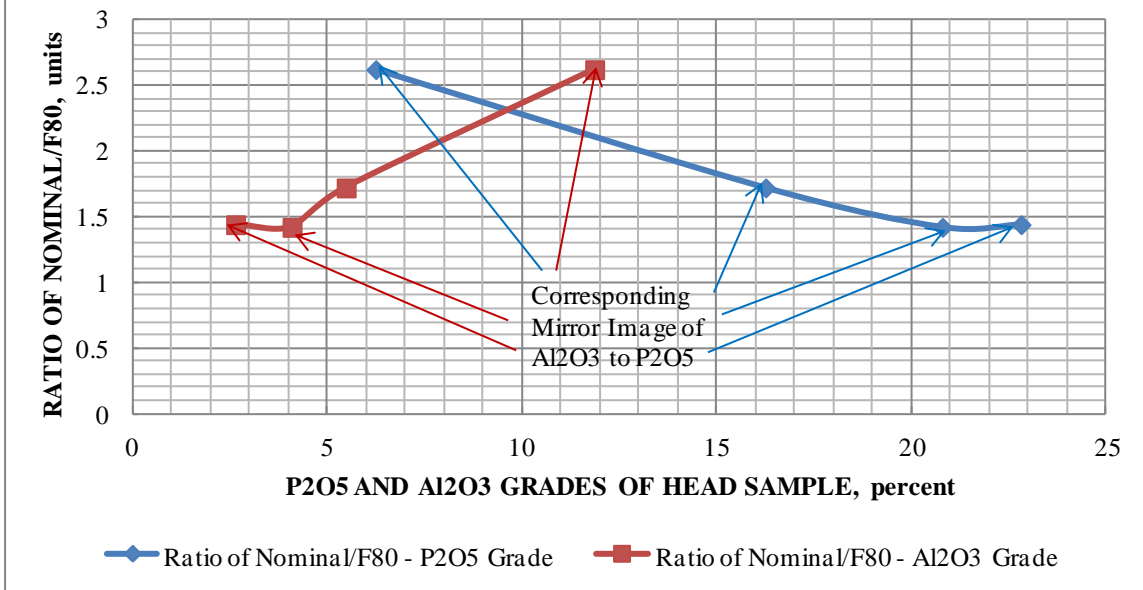
Composite B analyzed 5.49% Al<sub>2</sub>O<sub>3</sub> and 16.26% P<sub>2</sub>O<sub>5</sub>, and Composite C reported 11.87% Al<sub>2</sub>O<sub>3</sub> and 6.04% P<sub>2</sub>O<sub>5</sub>.

- The data showed that the higher the P<sub>2</sub>O<sub>5</sub> content and the lower the Al<sub>2</sub>O<sub>3</sub> content, the lower the value of the Ratio of F<sub>80</sub> and the Ratio of Nominal/F<sub>80</sub>, indicating that a stronger-harder phosphate ore will be submitted to HPGR comminution.
- Knowing that the Standard process produces 63.45% of P<sub>2</sub>O<sub>5</sub> recovery and 69.82% of Al<sub>2</sub>O<sub>3</sub>rejection at about 1.42 Ratio of Nominal/F<sub>80</sub>, larger ratio should result in better liberation under similar conditions; thus, improved results. This is in agreement with the concept of the effect of Al<sub>2</sub>O<sub>3</sub> and P<sub>2</sub>O<sub>5</sub> contents on the hardness of the ore.
- Since selective comminution of Al<sub>2</sub>O<sub>3</sub> bearing minerals by P<sub>2</sub>O<sub>5</sub> and SiO<sub>2</sub> bearing minerals was demonstrated in previous reports, it is expected that the results predicted by the Model be achieved.

TABLE 5. NOMINAL, F <sub>80</sub> , AND P <sub>80</sub> VALUES FOR MPH COMPOSITE SAMPLES											
TEST 4											
Composite	Nominal	Ratio of	Particle	Ratio of	Ratio of	Crushing	Ratio of	Attrition	Ratio of	Head Grades	
MPH Ore	Feed Size	Nominal	F <sub>80</sub>	F <sub>80</sub>	Nominal/	HPGR	Reduction	P <sub>80</sub>	Reduction	P <sub>2</sub> O <sub>5</sub>	Al <sub>2</sub> O <sub>3</sub>
Type	mm	Size	µm	Particle	F <sub>80</sub>	P <sub>80</sub> , µm	HPGR, R <sub>80</sub>	µm	Attrition, R <sub>80</sub>	%	%
Standard	-12.7	--	8900.00	--	1.43	--	--	--	--		
Standard	-2	6.35	1410.00	6.31	1.42	--	--	550.00	2.56	20.8	4.1
Composite A	-9.5	1.34	6590.00	1.35	1.44					22.82	2.65
Composite B	-9.5	1.34	5529.00	1.61	1.72					16.26	5.49
Composite C, 0.77 m/s	-9.5	1.34	3625.00	2.46	2.62	395.00	9.18	95.00	4.16	6.25	11.87



**FIGURE 2. CORRELATION OF GRADES OF P<sub>2</sub>O<sub>5</sub> AND AL<sub>2</sub>O<sub>3</sub> WITH RATIO OF REDUCTION FOR HPGR HEAD SAMPLES OF MPH PHOSPHATE ORE OF MINEMAKERS**



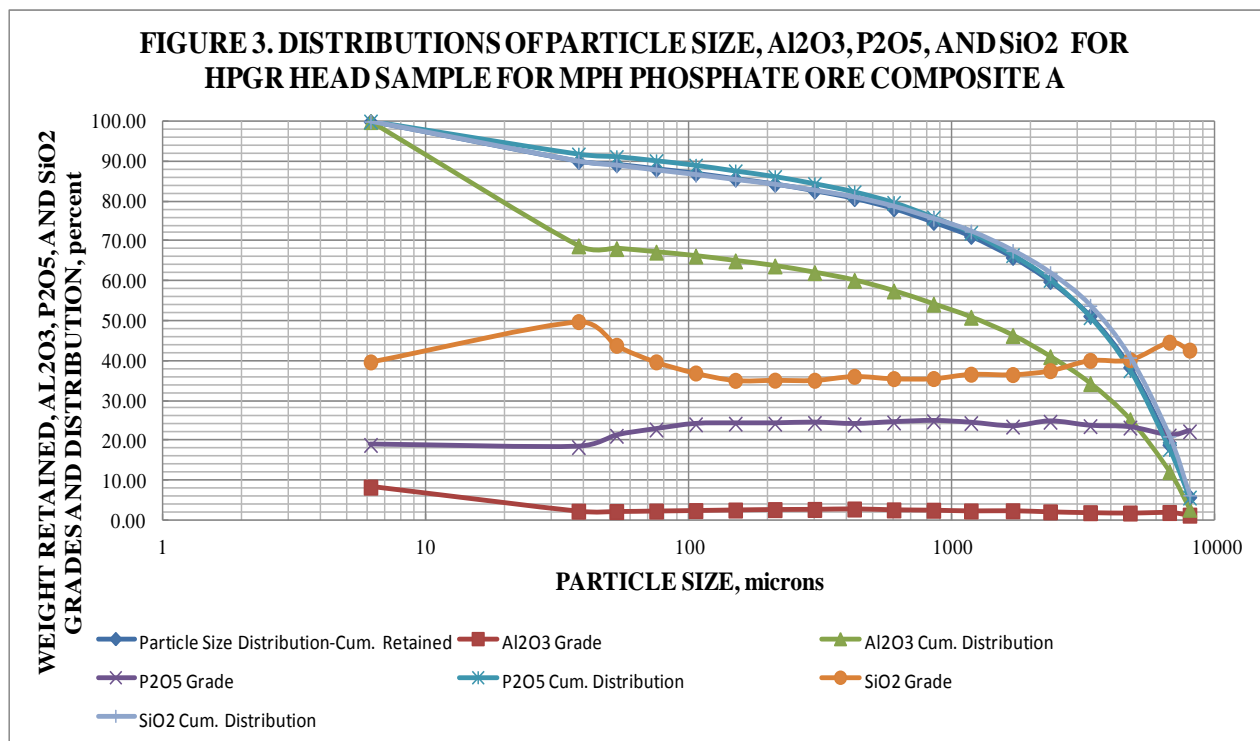
- Figure 2 showed that there was clear proportionality of the Head Samples Ratio of Nominal/F<sub>80</sub> with the P<sub>2</sub>O<sub>5</sub> and Al<sub>2</sub>O<sub>3</sub> Head Samples grades, validating the basis for the applied Model. **Moreover, this information confirmed the HPGR operating conditions selected 40 bars of Applied Pressure and 0.77 m/s of Rolls Speed.**

## SCREEN ASSAYS

### Composite A

- Composite A Head Samples analyzed 2.65% Al<sub>2</sub>O<sub>3</sub> and 22.82% P<sub>2</sub>O<sub>5</sub>. Clearly, this composite corresponded to the hardest phosphate ore since only 10.01% by weight reported to the -38-μm size fraction. Moreover, Al<sub>2</sub>O<sub>3</sub> material concentrated in this size fraction, resulting in 8.27% Al<sub>2</sub>O<sub>3</sub> with 18.86% P<sub>2</sub>O<sub>5</sub>. Thus, 31.19% of Al<sub>2</sub>O<sub>3</sub> is present in the -38-μm size fraction containing only 8.27% of P<sub>2</sub>O<sub>5</sub>.
- Again, the +2360-μm size fraction of the Composite A Head Sample showed a hard phosphate ore as indicated by 59.87% by weight in this size fraction. This material was low in Al<sub>2</sub>O<sub>3</sub> (1.82%) and high in P<sub>2</sub>O<sub>5</sub> (22.97%). Therefore, it appeared that after submitting Composite A to HPGR most of the +2360-μm material will report to the product (2360x38 μm). In the +2360-μm size fraction, 41.01% of Al<sub>2</sub>O<sub>3</sub> with 60.26% of P<sub>2</sub>O<sub>5</sub> was reported, P<sub>2</sub>O<sub>5</sub> being expected to be recovered in the 2360x38-μm size fraction after comminution in a HPGR.

- Product size, 2360x38  $\mu\text{m}$  corresponded to 30.11% by weight with 2.45%  $\text{Al}_2\text{O}_3$  and 23.85%  $\text{P}_2\text{O}_5$ . This size fraction contained 27.80% of  $\text{Al}_2\text{O}_3$  and 31.46% of  $\text{P}_2\text{O}_5$ . After HPGR comminution, it is expected to reduce  $\text{Al}_2\text{O}_3$  below 2.00%, the  $\text{Al}_2\text{O}_3$  reporting in the -38- $\mu\text{m}$  size fraction; whereas, most of the  $\text{P}_2\text{O}_5$  content remaining in the product, 2360x38  $\mu\text{m}$ .
- Consequently, it is expected above 90% of the  $\text{Al}_2\text{O}_3$  being reported in the -38- $\mu\text{m}$  size fraction with a total recovered in the 2360x38- $\mu\text{m}$  size fraction of  $\text{P}_2\text{O}_5$  of about 87%.
- Figure 3 presented the Distributions of  $\text{Al}_2\text{O}_3$ ,  $\text{P}_2\text{O}_5$ , and  $\text{SiO}_2$  for Composite A. These Distributions showed that the weight Retained (PSD) was dominated by the  $\text{P}_2\text{O}_5$  and  $\text{SiO}_2$  bearing minerals species (same locus of the curve); whereas, the  $\text{Al}_2\text{O}_3$  corresponded to a different locus, indicating that  $\text{Al}_2\text{O}_3$  bearing minerals will be preferentially comminuted by the harder material ( $\text{P}_2\text{O}_5$  and  $\text{SiO}_2$ ). The locus of the Grade Distribution Curves showed that  $\text{P}_2\text{O}_5$  was slightly higher in grade in the 2360x38- $\mu\text{m}$  size fraction decreasing in grade in the -38- $\mu\text{m}$  size fraction.  $\text{SiO}_2$  grade increased in the +2360  $\mu\text{m}$  and -38- $\mu\text{m}$  size fractions; whereas,  $\text{Al}_2\text{O}_3$  was flat for all size fractions increasing only at -38  $\mu\text{m}$ .

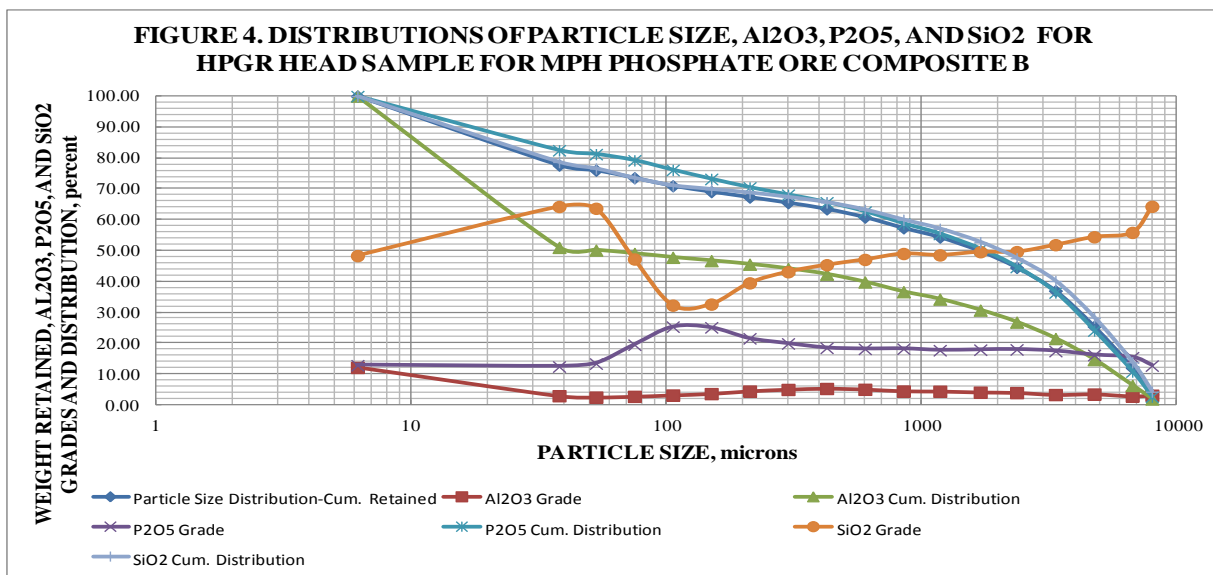


### Composite B

- Composite B Head Sample behaved similar than Composite A. This composite reported 5.49%  $\text{Al}_2\text{O}_3$  and 16.26%  $\text{P}_2\text{O}_5$  and higher weight fraction retained in the -38 $\mu\text{m}$ , 22.37%; thus, a medium-hard phosphate ore. As expected,  $\text{Al}_2\text{O}_3$  concentrated in the -

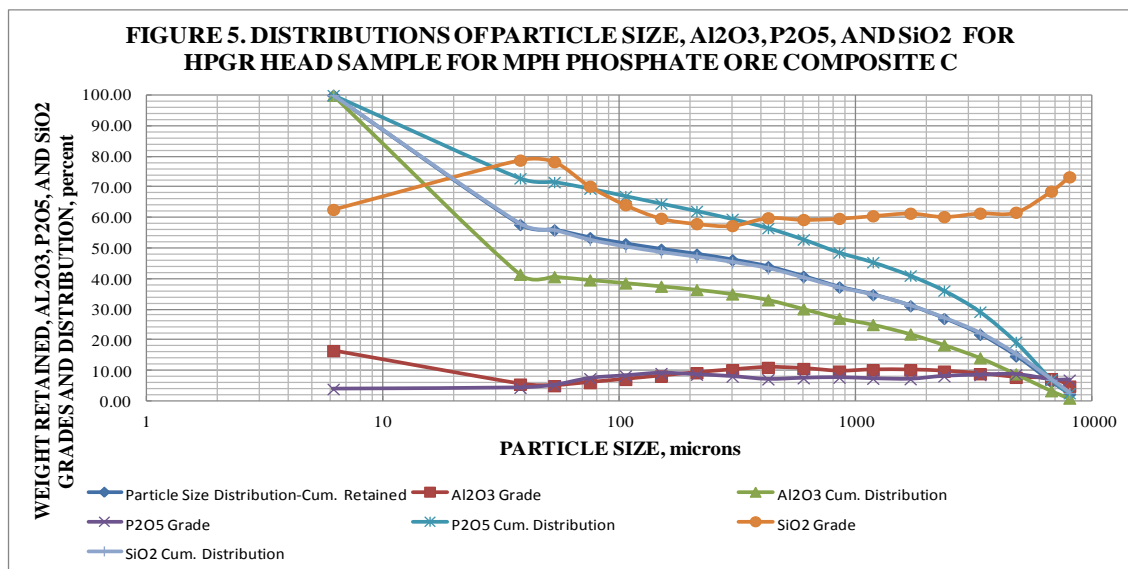
38- $\mu\text{m}$  size fraction, reporting 12.04%  $\text{Al}_2\text{O}_3$  and 12.76%  $\text{P}_2\text{O}_5$  corresponding to 49.05% of  $\text{Al}_2\text{O}_3$  content and 17.55% of  $\text{P}_2\text{O}_5$  content.

- The +2360- $\mu\text{m}$  size fraction corresponded to 44.45% by weight of the material with higher  $\text{Al}_2\text{O}_3$  (3.30%) and lower  $\text{P}_2\text{O}_5$  (16.32%) than those observed for Composite A. Again, it is assumed that by submitting this size fraction to HPGR comminution most of the material will report to the Product, 2360x38  $\mu\text{m}$ . The +2360- $\mu\text{m}$  material contained 26.74% of  $\text{Al}_2\text{O}_3$  and 44.62% of  $\text{P}_2\text{O}_5$  that it is expected to be recovered in the 2360x38- $\mu\text{m}$  size fraction after HPGR comminution.
- The Product size fraction, 2360x38  $\mu\text{m}$ , was 33.18% by weight, similar than that reported for the Composite A, which may indicate that the +2360- $\mu\text{m}$  material may trend to report in the 2360x38  $\mu\text{m}$  after comminution. 2360x38- $\mu\text{m}$  material analyzed 4.01%  $\text{Al}_2\text{O}_3$  and 18.54%  $\text{P}_2\text{O}_5$ , containing 24.21% of  $\text{Al}_2\text{O}_3$  and 37.82% of  $\text{P}_2\text{O}_5$  similar values than those of the Standard process. Thus, it is expected that  $\text{Al}_2\text{O}_3$  grade will drop below 2.00%, the  $\text{Al}_2\text{O}_3$  reporting in the -38- $\mu\text{m}$  size fraction; whereas, the  $\text{P}_2\text{O}_5$  remaining in the 2360x38- $\mu\text{m}$  size fraction.
- It is expected that about 92% of  $\text{Al}_2\text{O}_3$  being reported in the -38- $\mu\text{m}$  size fraction and above 82% of  $\text{P}_2\text{O}_5$  being recovered in the 2360x38  $\mu\text{m}$ .
- Figure 4 presented the Distributions of  $\text{Al}_2\text{O}_3$ ,  $\text{P}_2\text{O}_5$ , and  $\text{SiO}_2$  for Composite B. Similar to Composite A, the Distributions Curves showed that the PSD and the  $\text{SiO}_2$  Distribution shared the same locus; whereas, the locus of the  $\text{P}_2\text{O}_5$  Distribution Curve was slightly above the PSD, indicating that the phosphate bearing minerals were the hardest species (coarser material), the  $\text{Al}_2\text{O}_3$  bearing minerals being the softest (finer material). Thus, it was expected that the  $\text{Al}_2\text{O}_3$  bearing minerals will be preferentially ground by the harder  $\text{P}_2\text{O}_5$  and  $\text{SiO}_2$  bearing minerals. The Grade Distribution Curves showed that  $\text{P}_2\text{O}_5$  grade remained almost constant from 2360x200  $\mu\text{m}$ , increasing at 200x75  $\mu\text{m}$ , and decreasing in the -75- $\mu\text{m}$  size range.  $\text{SiO}_2$  decreased in grade from 8000  $\mu\text{m}$  to 106  $\mu\text{m}$ , increasing at -106- $\mu\text{m}$  size fraction.  $\text{Al}_2\text{O}_3$  grade increased in the size fraction 1700x150  $\mu\text{m}$ , increasing again in the -38- $\mu\text{m}$  size fraction.



## Composite C

- HPGR effect on Composite C has been analyzed in previous reports (January 27, 2014). However, Composite C Head Sample showed some important information that needed to be addressed. First, it was found that the  $P_{80}$  for Composite C was 3625  $\mu\text{m}$  instead of 3152  $\mu\text{m}$  reported by JK Tech. Since the difference corresponded to a coarser Head sample, the results clearly demonstrated that Composite C was the softest phosphate ore producing even large Ratio of Nominal/ $F_{80}$  than those already reported, and that selective comminution of  $\text{Al}_2\text{O}_3$  bearing minerals occurred,  $\text{P}_2\text{O}_5$  bearing minerals being ground at a slower rate. Therefore, Composite C Head Sample reported 11.87%  $\text{Al}_2\text{O}_3$  and 6.04%  $\text{P}_2\text{O}_5$ , the -38- $\mu\text{m}$  size fraction weight being 42.32%. Composite C  $\text{Al}_2\text{O}_3$  grade in the -38- $\mu\text{m}$  size fraction was 16.43% and that of  $\text{P}_2\text{O}_5$  was 3.88%. This corresponded to 58.58% of  $\text{Al}_2\text{O}_3$  and 27.19% of  $\text{P}_2\text{O}_5$  contents.
- Composite C +2360- $\mu\text{m}$  size fraction corresponded to 26.93% by weight with 8.08%  $\text{Al}_2\text{O}_3$  and 8.09%  $\text{P}_2\text{O}_5$ . The size fraction contained 18.33% of  $\text{Al}_2\text{O}_3$  and 36.74% of  $\text{P}_2\text{O}_5$ .
- The 2360x38- $\mu\text{m}$  size fraction reported 30.74% by weight analyzing 8.92%  $\text{Al}_2\text{O}_3$  and 7.21%  $\text{P}_2\text{O}_5$ , corresponding to 23.10% of  $\text{Al}_2\text{O}_3$  and 36.72% of  $\text{P}_2\text{O}_5$ .
- Figure 5 presented the Distributions of  $\text{Al}_2\text{O}_3$ ,  $\text{P}_2\text{O}_5$ , and  $\text{SiO}_2$  for Composite C. The Distributions Curves showed that the locus of the  $\text{P}_2\text{O}_5$  Distribution Curve corresponded to a much coarser product than that of other minerals. The PSD and  $\text{SiO}_2$  locus of the Distribution Curves were identical; whereas, the locus of the  $\text{Al}_2\text{O}_3$  Distribution showed the finest material in the phosphate ore. In the case of the Grade Distribution Curves, it was clear that  $\text{SiO}_2$  grade decreased in the 8000x4000- $\mu\text{m}$  size fraction, maintaining a constant grade for the 400x200- $\mu\text{m}$  size range, the  $\text{SiO}_2$  grade increasing in the -200- $\mu\text{m}$  fine fraction.  $\text{P}_2\text{O}_5$  grade increased from 800x500- $\mu\text{m}$ , level off from 500x200  $\mu\text{m}$ , and decreased in the -200- $\mu\text{m}$  size fraction.  $\text{Al}_2\text{O}_3$  grade increased in the 800x400- $\mu\text{m}$  range, decreased from 400x38  $\mu\text{m}$ , and increased again in the -38- $\mu\text{m}$  size fraction.



















**TABLE 1. NOMINAL, F<sub>80</sub>, AND P<sub>80</sub> VALUES FOR MPH (C)  
TESTS 3 AND 6**

<b>Composite MPH Ore Type</b>	<b>Nominal Feed Size mm</b>	<b>Ratio of Nominal Size</b>	<b>Particle F<sub>80</sub> μm</b>	<b>Ratio of F<sub>80</sub> Particle</b>	<b>Ratio of Nominal / F<sub>80</sub></b>	<b>Crushing HPGR P<sub>80</sub>, μm</b>
Standard	-12.7	--	8900.00	--	1.43	--
Standard	-2	6.35	1410.00	6.31	1.42	--
Composite C, 0.38 m/s	-9	1.41	3152.00	2.82	2.86	243.00
Composite C, 0.77 m/s	-9	1.41	3152.00	2.82	2.86	152.00

**COMPOSITE SAMPLES**

<b>Ratio of Reduction HPGR, R<sub>80</sub></b>	<b>Attrition P<sub>80</sub> μm</b>	<b>Ratio of Reduction Attrition, R<sub>80</sub></b>
--	--	--
--	550.00	2.56
12.97	92.00	2.64
20.74	86.00	1.77

**K12023 ATTRITIONING TEST 88 RESULTS (Composite C/HPGR Test 6 Product : 15 min attritioning time at 47.5% solids pulp density and 1200 rpm )**

PRODUCT	WEIGHT WEIGHT		ASSAY																DISTRIBUTION, %																
	g	%	Al <sub>2</sub> O <sub>3</sub> %	CaO %	Fe <sub>2</sub> O <sub>3</sub> %	K <sub>2</sub> O %	MgO %	MnO %	Na <sub>2</sub> O %	P <sub>2</sub> O <sub>5</sub> %	SiO <sub>2</sub> %	TiO <sub>2</sub> %	As ppm	Cd ppm	Pb ppm	Zn ppm	U ppm	LOI %	Al <sub>2</sub> O <sub>3</sub>	CaO	Fe <sub>2</sub> O <sub>3</sub>	K <sub>2</sub> O	MgO	MnO	Na <sub>2</sub> O	P <sub>2</sub> O <sub>5</sub>	SiO <sub>2</sub>	TiO <sub>2</sub>	As	Cd	Pb	Zn	U	LOI	
Attritioned +3350 µm Fraction	12.76	1.51	2.34	7.17	1.25	0.16	0.08	0.02	0.01	5.66	81.06	0.08	5.30	0.44	127	82	19	1.67	0.29	1.39	0.54	0.19	0.18	1.57	0.36	1.41	1.97	0.20	1.44	1.27	0.97	1.06	1.65	0.46	
Attritioned -3350+2360 µm Fraction	14.12	1.68	2.82	6.16	4.79	0.17	0.08	0.01	0.01	5.03	78.79	0.11	9.80	0.43	118	158	16	2.35	0.39	1.32	2.27	0.22	0.20	0.87	0.40	1.39	2.12	0.31	2.95	1.37	1.00	2.26	1.54	0.71	
(Attritioned +2360 µm Fraction)	(26.88)	(3.19)	(2.59)	(6.64)	(3.11)	(0.17)	(0.08)	(0.01)	(0.01)	(5.33)	(79.87)	(0.10)	(7.66)	(0.43)	(122)	(122)	(17)	(2.03)	(0.69)	(2.72)	(2.81)	(0.42)	(0.38)	(2.44)	(0.75)	(2.80)	(4.08)	(0.52)	(4.39)	(2.64)	(1.97)	(3.32)	(3.19)	(1.17)	
Attritioned -2360+1400 µm Fraction	23.27	2.76	3.35	10.57	4.51	0.23	0.11	0.03	0.02	7.71	69.72	0.12	15.20	0.66	189	137	21	3.01	0.77	3.75	3.52	0.50	0.45	4.30	1.30	3.50	3.08	0.56	7.54	3.47	2.64	3.23	3.33	1.51	
(Attritioned +1400 µm Fraction)	(50.15)	(5.95)	(2.94)	(8.46)	(3.76)	(0.20)	(0.09)	(0.02)	(0.01)	(6.43)	(75.16)	(0.11)	(11.16)	(0.54)	(153)	(129)	(19)	(2.48)	(1.45)	(6.46)	(6.33)	(0.92)	(0.83)	(6.75)	(2.06)	(6.30)	(7.17)	(1.08)	(11.94)	(6.11)	(4.61)	(6.55)	(6.52)	(2.68)	
Attritioned -1400+425 µm Fraction	46.45	5.51	4.53	12.55	4.97	0.32	0.16	0.07	0.02	9.60	64.22	0.17	14.20	0.83	259	201	27	3.56	2.07	8.88	7.75	1.39	1.32	20.04	2.60	8.70	5.67	1.58	14.07	8.71	7.21	9.46	8.54	3.56	
(Attritioned +425 µm Fraction)	(96.60)	(11.47)	(3.71)	(10.43)	(4.34)	(0.26)	(0.13)	(0.04)	(0.02)	(7.96)	(69.90)	(0.14)	(12.62)	(0.68)	(204)	(164)	(23)	(3.00)	(3.52)	(15.34)	(14.08)	(2.31)	(2.15)	(26.79)	(4.66)	(15.00)	(12.84)	(2.66)	(26.00)	(14.82)	(11.82)	(16.00)	(15.05)	(6.23)	
Attritioned -425+106 µm Fraction	46.49	5.52	3.96	13.23	3.77	0.26	0.15	0.08	0.03	10.03	64.67	0.16	11.20	0.79	307	160	26	2.99	1.81	9.37	5.88	1.13	1.24	22.92	3.91	9.10	5.72	1.49	11.10	8.30	8.56	7.53	8.23	2.99	
(Attritioned +106 µm Fraction)	(143.09)	(16.99)	(3.79)	(11.34)	(4.16)	(0.26)	(0.13)	(0.06)	(0.02)	(8.63)	(68.20)	(0.14)	(12.16)	(0.72)	(238)	(162)	(24)	(3.00)	(5.33)	(24.71)	(19.96)	(3.44)	(3.39)	(49.71)	(8.57)	(24.10)	(18.55)	(4.15)	(37.11)	(23.12)	(20.38)	(23.54)	(23.28)	(9.22)	
Attritioned -106+20 µm Fraction	116.66	13.85	4.10	7.76	2.16	0.39	0.18	0.02	0.03	5.86	76.41	0.35	3.80	0.42	174	74	17	2.37	4.71	13.79	8.46	4.26	3.72	14.38	9.81	13.34	16.95	8.19	9.45	11.07	12.17	8.74	13.50	5.95	
(Attritioned +20 µm Fraction)	(259.75)	(30.83)	(3.93)	(9.73)	(3.26)	(0.32)	(0.15)	(0.04)	(0.03)	(7.39)	(71.89)	(0.24)	(8.41)	(0.58)	(209)	(46)	(9)	(2.72)	(10.04)	(38.50)	(28.42)	(7.71)	(7.11)	(64.09)	(18.37)	(37.45)	(35.50)	(12.34)	(46.56)	(34.18)	(32.56)	(12.06)	(16.69)	(15.17)	
Attritioned -20 µm Fraction	582.69	69.17	15.69	6.93	3.66	1.69	0.90	0.01	0.05	5.50	58.22	0.75	4.30	0.50	193	149	21	6.77	89.96	61.50	71.58	92.29	92.89	35.91	81.63	62.55	64.50	87.66	53.44	65.82	67.44	87.94	83.31	84.83	
(Calculated Head)	(842.44)	(100.00)	(12.06)	(7.79)	(3.54)	(1.27)	(0.67)	(0.02)	(0.04)	(6.08)	(62.43)	(0.59)	(5.57)	(0.53)	(198)	(117)	(17)	(5.52)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)

Assayed Head

**K12023 ATTRITIONING TEST 88 RESULTS (Composite C/HPGR Test 6 Product : 15 min attritioning time at 47.5% solids pulp density and 1200 rpm )**

PRODUCT	WEIGHT WEIGHT		CUM %	PASSING WEIGHT %	ASSAY					CUM. ASSAY					DISTRIBUTION, %					CUM. DISTRIBUTION, %					Size Fraction Opening µm
	g	%			Al <sub>2</sub> O <sub>3</sub> %	CaO %	Fe <sub>2</sub> O <sub>3</sub> %	P <sub>2</sub> O <sub>5</sub> %	SiO <sub>2</sub> %	Al <sub>2</sub> O <sub>3</sub> %	CaO %	Fe <sub>2</sub> O <sub>3</sub> %	P <sub>2</sub> O <sub>5</sub> %	SiO <sub>2</sub> %	Al <sub>2</sub> O <sub>3</sub> %	CaO %	Fe <sub>2</sub> O <sub>3</sub> %	P <sub>2</sub> O <sub>5</sub> %	SiO <sub>2</sub> %	Al <sub>2</sub> O <sub>3</sub> %	CaO %	Fe <sub>2</sub> O <sub>3</sub> %	P <sub>2</sub> O <sub>5</sub> %	SiO <sub>2</sub> %	
										CUM	CUM	CUM	CUM	CUM							CUM	CUM	CUM	CUM	
Attritioned +3350 µm Fraction	12.76	1.51	1.51	98.49	2.34	7.17	1.25	5.66	81.06	2.34	7.17	1.25	5.66	81.06	0.29	1.39	0.54	1.41	1.97	0.29	1.39	0.54	1.41	1.97	3350
Attritioned -3350+2360 µm Fraction	14.12	1.68	3.19	96.81	2.82	6.16	4.79	5.03	78.79	2.59	6.64	3.11	5.33	79.87	0.39	1.32	2.27	1.39	2.12	0.69	2.72	2.81	2.80	4.08	2360
Attritioned -2360+1400 µm Fraction	23.27	2.76	5.95	94.05	3.35	10.57	4.51	7.71	69.72	2.94	8.46	3.76	6.43	75.16	0.77	3.75	3.52	3.50	3.08	1.45	6.46	6.33	6.30	7.17	1400
Attritioned -1400+425 µm Fraction	46.45	5.51	11.47	88.53	4.53	12.55	4.97	9.60	64.22	3.71	10.43	4.34	7.96	69.90	2.07	8.88	7.75	8.70	5.67	3.52	15.34	14.08	15.00	12.84	425
Attritioned -425+106 µm Fraction	46.49	5.52	16.99	83.01	3.96	13.23	3.77	10.03	64.67	3.79	11.34	4.16	8.63	68.20	1.81	9.37	5.88	9.10	5.72	5.33	24.71	19.96	24.10	18.55	106
Attritioned -106+20 µm Fraction	116.66	13.85	30.83	69.17	4.10	7.76	2.16	5.86	76.41	3.93	9.73	3.26	7.39	71.89	4.71	13.79	8.46	13.34	16.95	10.04	38.50	28.42	37.45	35.50	20
Attritioned -20 µm Fraction	582.69	69.17	100.00	0.00	15.69	6.93	3.66	5.50	58.22	12.06	7.79	3.54	6.08	62.43	89.96	61.50	71.58	62.55	64.50	100.00	100.00	100.00	100.00	100.00	4.47
(Calculated Head)	(842.44)	(100.00)			(12.06)	(7.79)	(3.54)	(6.08)	(62.43)						(100.00)	(100.00)	(100.00)	(100.00)	(100.00)						

**SUMMARY K12023 ATTRITIONING TEST 88 RESULTS (Composite C/HPGR Test 6 Product : 15 min attritioning time at 47.5% solids pulp density and 1200 rpm )**

(Attritioned +2360 µm Fraction)	26.88	3.19	3.19	96.81	2.59	6.64	3.11	5.33	79.87						0.69	2.72	2.81	2.80	4.08					
(Attritioned 2360x20 µm Fraction)	232.87	27.64	27.64	69.17	4.08	10.09	3.28	7.62	64.22						9.36	35.78	25.61	34.65	31.42					
Attritioned -20 µm Fraction	582.69	69.17	100.00	0.00	15.69	6.93	3.66	5.50	58.22	12.06	7.79	3.54	6.08	62.43	89.96	61.50	71.58	62.55	64.50	100.00	100.00	100.00	100.00	100.00

**SUMMARY K12023 SIZE-ASSAY RESULTS (Composite C HPGR Test 6 Product)**

Product Size +2360	32.08	3.81	3.81	96.19	3.74	9.70	4.56	7.24	74.76						1.20	4.69	4.84	4.51	4.57					
Product Size 2360x38	221.00	26.06	26.06	70.13	5.20	10.99	3.86	8.28	66.76						11.38	36.31	28.02	35.25	27.87					
Product Size -38 µm Fraction	589.97	70.13	100.00	0.00	14.85	6.64	3.44	5.26	60.14	11.91	7.89	3.59	6.12	62.42	87.42	59.01	67.15	60.25	67.56	100.00	100.00	100.00	100.00	100.00

**K12023 ATTRITIONING TEST 89 (duplicate of Test 88) RESULTS (Composite C/HPGR Test 6 Product : 15 min attritioning time at 47.5% solids pulp density and 1200 rpm )**

PRODUCT	WEIGHT WEIGHT		ASSAY																DISTRIBUTION, %															
	g	%	Al <sub>2</sub> O <sub>3</sub> %	CaO %	Fe <sub>2</sub> O <sub>3</sub> %	K <sub>2</sub> O %	MgO %	MnO %	Na <sub>2</sub> O %	P <sub>2</sub> O <sub>5</sub> %	SiO <sub>2</sub> %	TiO <sub>2</sub> %	As ppm	Cd ppm	Pb ppm	Zn ppm	U ppm	LOI %	Al <sub>2</sub> O <sub>3</sub>	CaO	Fe <sub>2</sub> O <sub>3</sub>	K <sub>2</sub> O	MgO	MnO	Na <sub>2</sub> O	P <sub>2</sub> O <sub>5</sub>	SiO <sub>2</sub>	TiO <sub>2</sub>	As	Cd	Pb	Zn	U	LOI
Attritioned +3350 µm Fraction	9.90	1.17	2.06	4.23	2.14	0.14	0.06	0.01	0.01	3.48	86.38	0.08	3.10	0.32	94	65	11	1.73	0.20	0.63	0.70	0.13	0.10	0.56	0.23	0.67	1.62	0.16	0.34	0.73	0.55	0.61	0.74	0.36
Attritioned -3350+2360 µm Fraction	12.95	1.53	3.20	9.47	3.27	0.23	0.10	0.01	0.03	7.44	73.89	0.11	8.20	0.62	143	160	20	2.44	0.41	1.86	1.40	0.27	0.22	0.73	0.92	1.87	1.82	0.28	1.18	1.84	1.10	1.97	1.76	0.66
(Attritioned +2360 µm Fraction)	(22.85)	(2.71)	(2.71)	(7.20)	(2.78)	(0.19)	(0.08)	(0.01)	(0.02)	(5.72)	(79.30)	(0.10)	(5.99)	(0.49)	(122)	(119)	(16)	(2.13)	(0.61)	(2.49)	(2.11)	(0.40)	(0.32)	(1.29)	(1.15)	(2.54)	(3.44)	(0.44)	(1.52)	(2.56)	(1.65)	(2.58)	(2.50)	(1.02)
Attritioned -2360+1400 µm Fraction	23.80	2.82	3.77	10.14	5.18	0.25	0.12	0.05	0.01	7.85	70.59	0.14	12.70	1.33	204	397	22	3.09	0.88	3.66	4.09	0.55	0.49	6.71	0.56	3.62	3.19	0.66	3.37	7.24	2.88	8.96	3.56	1.53
(Attritioned +1400 µm Fraction)	(46.65)	(5.53)																																



**K12023 SIZE-ASSAY RESULTS (HPGR Composite A -9.5 mm Head Sample)**

PRODUCT	WEIGHT		ASSAY																DISTRIBUTION, %															
	g	%	Al <sub>2</sub> O <sub>3</sub> %	CaO %	Fe <sub>2</sub> O <sub>3</sub> %	K <sub>2</sub> O %	MgO %	MnO %	Na <sub>2</sub> O %	P <sub>2</sub> O <sub>5</sub> %	SiO <sub>2</sub> %	TiO <sub>2</sub> %	As ppm	Cd ppm	Pb ppm	Zn ppm	U ppm	LOI %	Al <sub>2</sub> O <sub>3</sub>	CaO	Fe <sub>2</sub> O <sub>3</sub>	K <sub>2</sub> O	MgO	MnO	Na <sub>2</sub> O	P <sub>2</sub> O <sub>5</sub>	SiO <sub>2</sub>	TiO <sub>2</sub>	As	Cd	Pb	Zn	U	LOI
Product Size +8000 µm Fraction	57.79	5.79	1.25	30.31	0.96	0.13	0.07	0.01	0.01	22.27	42.65	0.06	2	2.00	159	217	17	1.38	2.72	5.68	4.60	3.01	3.85	1.54	3.20	5.65	6.23	2.75	3.31	4.94	3.63	4.93	5.04	4.65
Product Size +6700 µm Fraction	130.92	13.11	1.91	28.59	0.97	0.21	0.08	0.01	0.01	21.20	44.64	0.10	4	2.10	185	183	17	1.44	9.43	12.13	10.54	11.01	9.98	3.49	7.24	12.18	14.78	10.37	14.98	11.75	9.58	9.41	11.41	11.00
Product Size +4750 µm Fraction	194.23	19.45	1.78	31.39	0.78	0.18	0.08	0.03	0.01	23.21	40.24	0.09	1	2.30	211	172	18	1.32	13.04	19.76	12.57	14.00	14.81	15.52	10.74	19.78	19.76	13.84	5.56	19.09	16.21	13.12	17.93	14.96
Product Size +3350 µm Fraction	128.55	12.87	1.87	31.34	0.95	0.20	0.08	0.03	0.01	23.58	40.08	0.10	4	2.20	197	190	19	1.39	9.07	13.06	10.13	10.30	9.80	10.28	7.11	13.30	13.03	10.18	14.71	12.09	10.02	9.59	12.52	10.43
Product Size +2360 µm Fraction	86.39	8.65	2.07	32.69	1.01	0.21	0.08	0.04	0.01	24.68	37.50	0.11	3	2.50	285	227	20	1.52	6.75	9.15	7.24	7.27	6.59	9.21	4.78	9.36	8.19	7.52	7.41	9.23	9.74	7.70	8.86	7.66
Product Size +1700 µm Fraction	60.35	6.04	2.34	32.53	1.29	0.21	0.10	0.04	0.03	23.46	36.52	0.11	3	2.40	265	284	21	1.53	5.33	6.36	6.46	5.08	5.75	6.43	10.01	6.21	5.57	5.26	5.18	6.19	6.33	6.73	6.50	5.39
Product Size +1180 µm Fraction	52.60	5.27	2.30	33.19	1.33	0.23	0.15	0.04	0.03	24.35	36.61	0.12	4	2.50	266	273	21	1.63	4.56	5.66	5.80	4.85	7.52	5.61	8.73	5.62	4.87	5.00	6.02	5.62	5.53	5.64	5.66	5.00
Product Size +850 µm Fraction	35.10	3.52	2.48	33.76	1.41	0.25	0.10	0.05	0.03	24.80	35.52	0.12	7	2.50	301	292	21	1.68	3.28	3.84	4.11	3.51	3.34	4.68	5.82	3.82	3.15	3.33	7.03	3.75	4.18	4.03	3.78	3.44
Product Size +600 µm Fraction	34.11	3.42	2.57	33.60	1.60	0.25	0.10	0.05	0.01	24.49	35.50	0.13	1	2.90	323	339	22	1.76	3.31	3.71	4.53	3.42	3.25	4.54	1.89	3.67	3.06	3.51	0.98	4.23	4.36	4.54	3.85	3.50
Product Size +425 µm Fraction	25.37	2.54	2.79	32.26	1.79	0.26	0.10	0.07	0.03	24.03	36.07	0.14	6	2.60	343	374	22	1.88	2.67	2.65	3.77	2.64	2.42	4.73	4.21	2.67	2.31	2.81	4.36	2.82	3.44	3.73	2.86	2.78
Product Size +300 µm Fraction	19.23	1.93	2.68	33.10	1.93	0.26	0.10	0.08	0.03	24.38	35.09	0.13	6	2.70	390	404	22	1.96	1.94	2.06	3.08	2.00	1.83	4.10	3.19	2.06	1.71	1.98	3.30	2.22	2.97	3.05	2.17	2.20
Product Size +212 µm Fraction	16.76	1.68	2.64	32.88	2.00	0.25	0.10	0.09	0.03	24.19	35.11	0.13	6	2.70	393	424	22	1.96	1.67	1.79	2.78	1.68	1.60	4.02	2.78	1.78	1.49	1.73	2.88	1.93	2.61	2.79	1.89	1.92
Product Size +150 µm Fraction	13.32	1.33	2.53	33.33	2.15	0.24	0.10	0.10	0.01	24.19	35.07	0.13	3	2.60	402	454	23	1.94	1.27	1.44	2.38	1.28	1.27	3.55	0.74	1.41	1.18	1.37	1.14	1.48	2.12	2.38	1.57	1.51
Product Size +106 µm Fraction	13.46	1.35	2.39	32.47	1.94	0.22	0.10	0.09	0.01	24.05	36.91	0.13	10	2.60	390	435	23	2.01	1.21	1.42	2.17	1.19	1.28	3.23	0.74	1.42	1.26	1.39	3.85	1.50	2.08	2.30	1.59	1.58
Product Size +75 µm Fraction	11.42	1.14	2.27	31.02	1.78	0.22	0.10	0.08	0.04	22.74	39.71	0.14	6	2.40	363	424	21	1.86	0.98	1.15	1.69	1.01	1.09	2.43	2.53	1.14	1.15	1.27	1.96	1.17	1.64	1.90	1.23	1.24
Product Size +53 µm Fraction	11.01	1.10	2.16	28.79	1.53	0.22	0.10	0.07	0.04	21.15	43.86	0.15	6	2.20	334	376	20	1.85	0.90	1.03	1.40	0.97	1.05	2.05	2.44	1.02	1.22	1.31	1.89	1.04	1.45	1.63	1.13	1.19
Product Size +38 µm Fraction	7.98	0.80	2.24	25.25	1.39	0.24	0.10	0.06	0.04	18.32	49.81	0.17	5	2.10	305	354	18	1.74	0.67	0.65	0.92	0.77	0.76	1.28	1.76	0.64	1.01	1.07	1.14	0.72	0.96	1.11	0.74	0.81
Product Size -38 µm Fraction	99.98	10.01	8.27	26.07	1.91	0.65	0.25	0.05	0.04	18.86	39.69	0.32	5	2.40	333	393	22	3.55	31.19	8.45	15.84	26.03	23.82	13.32	22.11	8.27	10.03	25.33	14.30	10.25	13.17	15.43	11.28	20.72
(Calculated Head)	(998.57)	(100.00)	(2.65)	(30.89)	(1.21)	(0.25)	(0.11)	(0.04)	(0.02)	(22.82)	(39.61)	(0.13)	(4)	(2.34)	(253)	(255)	(20)	(1.72)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)	(100.00)

Assayed Head





**TO:** Mr. Marten Walters, President, KEMWorks Technology, Inc.  
**CC:** Mr. Neville Bergin, General Manager, MINEMAKERS Limited.

**FROM:** Dr. Francisco J. Sotillo, President, PerUSA EnviroMet, Inc.

**SUBJECT:** Laboratory Tests to Determine the Potential Use of High Pressure Grinding Roll (HPGR) and Attrition Tests 86 to 93 for MPH Samples from Arruwurra Wonarah Phosphate Project, Composite C and Duplicates – Data Analysis .

**DATE:** January 27, 2014

**SUMMARY, MODEL, AND RECOMMENDATIONS**

- Table 4 presented the Summary of data for all HPGR and HPGR = attrition tests carried out for Composite C:

**TABLE 4. SUMMARY OF RESULTS OF HPGR - COMPOSITE C FOR MPH PHOSPHATE ORE - MINEMAKERS**

Product/HPGR Test	Pressure bars*	Rolls Speed m/s	P <sub>80</sub> HPGR µm	P <sub>80</sub> Crush + Attrition, µm	HPGR/Crusher				HPGR + Attrition				Feed	
					Grades**		Al <sub>2</sub> O <sub>3</sub>	P <sub>2</sub> O <sub>5</sub>	Grades		Al <sub>2</sub> O <sub>3</sub>	P <sub>2</sub> O <sub>5</sub>	Grades	
					Al <sub>2</sub> O <sub>3</sub> , %	P <sub>2</sub> O <sub>5</sub> , %	Rejec., %	Reco., %	Al <sub>2</sub> O <sub>3</sub> , %	P <sub>2</sub> O <sub>5</sub> , %	Rejec., %	Reco., %	Al <sub>2</sub> O <sub>3</sub> , %	P <sub>2</sub> O <sub>5</sub> , %
Standard	10			550.00	4.10	20.80	0.00	100.00	1.98	21.11	69.82	63.45	4.10	20.80
Test 1	40	0.38	266.00	95.00	6.09	8.82	84.61	39.74	4.39	8.17	88.65	37.59	11.89	6.18
Test 2	50	0.38	289.00	95.00	6.37	8.68	83.92	40.44	4.44	8.07	88.48	36.57	11.93	6.24
Test 3	70	0.38	243.00	92.00	5.75	8.17	84.99	38.11	4.09	7.80	89.67	35.30	11.98	6.14
Standard	10			550.00	4.10	20.80	0.00	100.00	1.98	21.11	69.82	63.45	4.10	20.80
Test 4	40	0.77	395.00	95.00	6.90	8.33	80.81	42.45	4.38	8.11	88.66	36.83	11.87	6.25
Test 5	50	0.77	205.00	83.00	6.05	8.33	84.68	37.60	4.12	7.85	89.91	34.70	11.97	6.28
Test 6	70	0.77	152.00	86.00	5.51	8.13	86.60	35.57	4.11	7.63	89.96	34.59	12.08	6.10

- For Composite C (soft phosphate ore), the use of 40 bar and 0.77 m/s Rolls Speed (Test 4) shows advantages:
  - Reducing the excessive grinding due to high Applied Pressure
  - Reporting the highest capacity
  - Obtaining the lowest Specific net Comminution Energy (E<sub>cs(net0)</sub>)
  - Selective grinding of Al<sub>2</sub>O<sub>3</sub> bearing minerals with respect to P<sub>2</sub>O<sub>5</sub> and SiO<sub>2</sub> bearing minerals
  - Higher P<sub>2</sub>O<sub>5</sub> recovery and Al<sub>2</sub>O<sub>3</sub> rejection in the 2360x20-µm product than those tests at 0.77 m/s Rolls Speed even though excessive grinding takes place using HPGR on Composite C (see Excel File KEMWorks-PN2069-HPGR-K12023 MPH AT90\_91).

	Test 1	Test 4	Ratio	Observation
+ Throughput, t/h =	1.44	2.84	1.97	more capacity
+ Sp. Energy, KWh/t =	1.36	1.34	0.99	less energy

- Processing of HPGR Tests 1 and 4 and HPGR Tests 2 and 5 results were carried out not only to determine the effect of Applied Pressure and Rolls Speed. Moreover, all data were required to predict the results at the best operating conditions for HPGR obtained for Composite C for Composite A and Composite B.
- A model was developed to try to extrapolate the results obtained for Composite C to those to be obtained on Composite A and B based on different composition of the MPH Phosphate Ore. This Model is presented in Excel File KEMWorks-PN2069-HPGR-K12023 MPH AT90\_91 too. The predicted results were:

<b>COMPOSITE B</b>	<b>Maximum P<sub>2</sub>O<sub>5</sub> Recovery =</b>	$((\text{Standard} - \text{HPGR} + \text{attrition Recoveries}) * \text{Factor}) + \text{HPGR} + \text{attrition Recovery} =$	<b>73.19 %</b>
	<b>Maximum Al<sub>2</sub>O<sub>3</sub> Rejection =</b>	$((\text{HPGR} + \text{attrition Recoveries} - \text{Standard}) / \text{Factor}) + \text{Standard Recovery} =$	<b>83.61 %</b>
<b>COMPOSITE A</b>	<b>Maximum P<sub>2</sub>O<sub>5</sub> Recovery =</b>	$((\text{Standard} - \text{HPGR} + \text{attrition Recoveries}) * \text{Factor}^2) + \text{HPGR} + \text{attrition Recovery} =$	<b>86.50 %</b>
	<b>Maximum Al<sub>2</sub>O<sub>3</sub> Rejection =</b>	Data showed that there is a plateau at about 89% Al <sub>2</sub> O <sub>3</sub> Rejection =	<b>89.00 %</b>

- Since the operating conditions of the HPGR crushing (Applied Pressure and Rolls Speed) depends on the hardness of the ore (Al<sub>2</sub>O<sub>3</sub> content), it is of utmost importance to determine the F<sub>80s</sub> of Composites A and B prepared at Nominal size -9 mm for the HPGR tests, and compare them with the Standard and Composite C. This is required to validate the Model prediction for P<sub>2</sub>O<sub>5</sub> recovery and Al<sub>2</sub>O<sub>3</sub> rejection with the Applied Pressure and Rolls Speed selected from Composite C tests, and applied those operating conditions to Composite A and B for HPGR testing based in potential ratios of reduction (R<sub>80</sub>).

## INTRODUCTION

As requested by Minemakers Australia PTY LTD, the analysis of the Interim Test Results of:

- HPGR Test 1 (40 bar Applied Pressure and 0.38 m/s Rolls Speed),
- HPGR Test 2 (50 bar Applied Pressure and 0.38 m/s Rolls Speed),
- HPGR Test 4 (40 bar Applied Pressure and 0.77 m/s Rolls Speed),
- HPGR Test 5 (50 bar Applied Pressure and 0.77 m/s Rolls Speed),

the previous reviewed data for:

- HPGR Test 3 (70 bar Applied Pressure and 0.38 m/s Rolls Speed) and
- HPGR Test 6 (70 bar Applied Pressure and 0.77 m/s Rolls Speed),

and their corresponding attrition scrubbing of HPGR Tests 1, 2, 3, 4, 5, and 6 products (47.5% solids content, 1200 rpm, and 15 minutes) were performed.

This analysis included a mathematical modeling of the effect of the phosphate ore composition to predict the results on P<sub>2</sub>O<sub>5</sub> Recovery and Al<sub>2</sub>O<sub>3</sub> Rejection for Composite A (<2% Al<sub>2</sub>O<sub>3</sub>), and Composite B (<4% Al<sub>2</sub>O<sub>3</sub>, >9% Al<sub>2</sub>O<sub>3</sub>) at the selected best HPGR operating conditions that corresponded to Test 4, 40 bar Applied Pressure and 0.77 m/s Rolls Speed. The processed information is presented in the following Excel Files:

- KEMWorks-PN2069-HPGR Results-K12023SA12.

- KEMWorks-PN2069-HPGR Results-K12023SA13.
- KEMWorks-PN2069-HPGR Results-K12023SA14.
- KEMWorks-PN2069-HPGR Results-K12023SA15.
- KEMWorks-PN2069-HPGR Results-K12023SA16.
- KEMWorks-PN2069-HPGR Results-K12023SA17.
- KEMWorks-PN2069-HPGR Results-K12023SA18.
- KEMWorks-PN2069-HPGR Results-K12023SA19.
- KEMWorks-PN2069-HPGR-K12023 MPH AT86\_87.
- KEMWorks-PN2069-HPGR-K12023 MPH AT88\_89.
- KEMWorks-PN2069-HPGR-K12023 MPH AT90\_91.
- KEMWorks-PN2069-HPGR-K12023 MPH AT92\_93.

These tests results were aimed at determining the feasibility of using High Pressure Grinding Roll (HPGR) on the PFD for the beneficiation of a composite sample of the Main Zone (MPH), Arruwurra, Wonarah Phosphate Project. For these tests, MPH Phosphate Ore Composite C (>9% Al<sub>2</sub>O<sub>3</sub>) were submitted to HPGR testing program. Test 1, 2, and 3 deferred from Test 4, 5, and 6 on the Rolls Speed, 0.38 m/s and 0.77 m/s, respectively, but followed the same Applied Pressure sequence of 40, 50, and 70 bar, respectively. The following paragraphs presented the comments and observations in a bullet form for easy following.

## COMMENTS AND OBSERVATIONS

### General Comments

- As mentioned in previous reports (September 05 and November 11, 2013) for the Interim Tests Results, the use of HPGR may be possible due to these encouraging results. Thus, a SAG mill could be replaced, and savings in energy, CAPEX, and water may be obtained.
- Generally, the results showed that the selective grinding of Al<sub>2</sub>O<sub>3</sub> minerals took place during these tests, P<sub>2</sub>O<sub>5</sub> and SiO<sub>2</sub> being ground at a slower rate than Al<sub>2</sub>O<sub>3</sub>.
- Data showed that at all Applied Pressures (40 bar, 50, bar, and 70 bar), excessive grinding of P<sub>2</sub>O<sub>5</sub> occurred, increasing P<sub>2</sub>O<sub>5</sub> losses for Composite C. Thus, the lower the Applied Pressure the lower the P<sub>2</sub>O<sub>5</sub> losses obtained with higher Al<sub>2</sub>O<sub>3</sub> rejection than that reported for the Standard crushing + attrition system. Therefore, 40 bar of Applied Pressure was selected.
- It was also shown that grinding at higher Rolls Speed was beneficial at 40 bar of Applied Pressure since higher P<sub>2</sub>O<sub>5</sub> was recovered even though Al<sub>2</sub>O<sub>3</sub> rejection was lower at 0.77 m/s of Rolls Speed; slower Rolls Speed being beneficial for 50 bar and 70 bar of Applied Pressure with similar Al<sub>2</sub>O<sub>3</sub> rejection but higher P<sub>2</sub>O<sub>5</sub> recovery. However, differences in both Al<sub>2</sub>O<sub>3</sub> rejections and P<sub>2</sub>O<sub>5</sub> recoveries were not significant to be considered the defining factor for the selection of the best Rolls Speed to be used.
- At slower Rolls Speed (0.38 m/s) the P<sub>80</sub> of the ground product was significantly coarser than that of high Rolls Speed (0.77 m/s), 266 µm, 289 µm, and 243 µm for Tests 1, 2, and 3, respectively, versus 395 µm, 205 µm, and 152 µm for Test 4, 5, and 6, the exception

being Test 4, showing a coarse HPGR ground product (?). Probably, the coarser size fraction at 0.38 m/s Rolls Speed was a consequence of the plasticity of Composite C (energy lost in the material deformation).

- The capacity increased at higher Rolls Speed (0.77 m/s) for all the Applied Pressures tested. The selected HPGR operating conditions (Test 4) reported 1.97 times the throughput (t/h) obtained for the slow Rolls Speed, 0.38 m/s (Test 1). Test 5 (50 bar Applied Pressure and 0.77 m/s Rolls Speed) resulted in 1.96 times the throughput (t/h) obtained for the slow Rolls Speed, 0.38 m/s (Test 2); whereas, Test 6 (70 bar Applied Pressure and 0.77 m/s Rolls Speed) reported 1.94 times the throughput (t/h) obtained for the slow Rolls Speed, 0.38 m/s (Test 3). This parameter was a significant factor in the selection of the Rolls Speed to be used.
- The Specific Net Comminution Energy ( $E_{cs(net)}$ ) was slightly lower at high Rolls Speed (0.77 m/s) than that at low Rolls Speed (0.38 m/s), decreasing as the Applied Pressure increased. Thus, the  $E_{cs(net)}$  at 40 bar and 0.77 m/s Rolls Speed (Test 4) was 0.99 that of Test 1 at 0.38 m/s Rolls Speed;  $E_{cs(net)}$  at 50 bar and 0.77 m/s Rolls Speed (Test 5) was 0.93 that of Test 2 at 0.38 m/s Rolls Speed; and  $E_{cs(net)}$  70 bar and 0.77 m/s Rolls Speed (Test 6) was 0.94 that of Test 3 at 0.38 m/s Rolls Speed. This factor indicated that using higher Rolls Speed (0.77 m/s) was beneficial in reducing specific energy consumption.
- It must also bear in mind that Composite C was high in  $Al_2O_3$  and low in  $P_2O_5$ , which may increase the overall grindability of the material, resulting in high  $P_2O_5$  losses for all Applied Pressures (40 bar, 50 bar, and 70 bar). Moreover, HPGR is a more efficient comminution technology due to the application of the Bed Comminution Mechanism, which resulted in finer product than that obtained by conventional crushing. Under these conditions, it is necessary to model the effect of change in composition of the MPH Phosphate Ore and the use of more efficient HPGR to determine the potential  $Al_2O_3$  rejection and  $P_2O_5$  recovery for Composite A and B.
- Attrition of the HPGR products significantly reduced the particle size demonstrating the micro-cracking and residual stresses in the particles generated by the Bed Comminution Mechanism of the HPGR. As is shown in Excel File KEMWorks-PN2069-HPGR-K12023 MPH AT90\_91, Table 4. Summary of Results of HPGR – Composite C for MPH Phosphate Ore – Minemakers, the Standard (crushing + attrition) resulted in a  $P_{80}$  of 550  $\mu m$ ; whereas, HPGR + Attrition Tests 1, 2, 3, 4, 5, and 6 reported a  $P_{80}$  of 95  $\mu m$ , 95  $\mu m$ , 92  $\mu m$ , 95  $\mu m$ , 83  $\mu m$ , and 86  $\mu m$ ; respectively.
- In general, the analysis of the results was complicated by the different size fractions chosen for the HPGR Tests, and those size fractions used for the Attrition Scrubbing Tests 86 to 93. As a consequence, plotting of the results was a better way to analyze this information.
- The results of Duplicates for both HPGR Tests 3 and 6, and the Attrition Scrubbing Tests 87 and 89 were virtually identical to those of the Original samples studied. However, average data for the Original and Duplicate tests were used for the analysis. No Duplicates results were shown for HPGR Tests 1, 2, 4, and 5.
- For this evaluation, we must be aware that the data on Distribution and Grades takes into consideration the rejection of the +2360- $\mu m$  size fraction and the -38  $\mu m$  or -20- $\mu m$  size fraction for the HPGR and HPGR + attrition tests, respectively, for the calculations.

## Preliminary Analysis

To put in an appropriate context the data generated on these HPGR tests, Table 1 presented the Nominal,  $F_{80}$ , and  $P_{80}$  values of the Standard MPH Phosphate Ore prepared at different nominal sizes in comparison with those produced by preparing Composite C at nominal -9-mm feed size for Test 3 and 6. Table 2 presented this information for Tests 1 and 4; whereas, Table 3 presented the Nominal,  $F_{80}$ , and  $P_{80}$  Values for MPH Phosphate Samples for Tests 2 and 5.

TABLE 1. NOMINAL, $F_{80}$ , AND $P_{80}$ VALUES FOR MPH COMPOSITE SAMPLES									
TESTS 3 AND 6									
Composite MPH Ore Type	Nominal Feed Size mm	Ratio of Nominal Size	Particle $F_{80}$ $\mu\text{m}$	Ratio of $F_{80}$ Particle	Ratio of Nominal / $F_{80}$	Crushing HPGR $P_{80}$ , $\mu\text{m}$	Ratio of Reduction HPGR, $R_{80}$	Attrition $P_{80}$ $\mu\text{m}$	Ratio of Reduction Attrition, $R_{80}$
Standard	-12.7	--	8900.00	--	1.43	--	--	--	--
Standard	-2	6.35	1410.00	6.31	1.42	--	--	550.00	2.56
Composite C, 0.38 m/s	-9	1.41	3152.00	2.82	2.86	243.00	12.97	92.00	2.64
Composite C, 0.77 m/s	-9	1.41	3152.00	2.82	2.86	152.00	20.74	86.00	1.77

TABLE 2. NOMINAL, $F_{80}$ , AND $P_{80}$ VALUES FOR MPH COMPOSITE SAMPLES									
TESTS 1 AND 4									
Composite MPH Ore Type	Nominal Feed Size mm	Ratio of Nominal Size	Particle $F_{80}$ $\mu\text{m}$	Ratio of $F_{80}$ Particle	Ratio of Nominal / $F_{80}$	Crushing HPGR $P_{80}$ , $\mu\text{m}$	Ratio of Reduction HPGR, $R_{80}$	Attrition $P_{80}$ $\mu\text{m}$	Ratio of Reduction Attrition, $R_{80}$
Standard	-12.7	--	8900.00	--	1.43	--	--	--	--
Standard	-2	6.35	1410.00	6.31	1.42	--	--	550.00	2.56
Composite C, 0.38 m/s	-9	1.41	3152.00	2.82	2.86	266.00	11.85	95.00	2.80
Composite C, 0.77 m/s	-9	1.41	3152.00	2.82	2.86	395.00	7.98	95.00	4.16

TABLE 3. NOMINAL, $F_{80}$ , AND $P_{80}$ VALUES FOR MPH COMPOSITE SAMPLES									
TESTS 2 AND 5									
Composite MPH Ore Type	Nominal Feed Size mm	Ratio of Nominal Size	Particle $F_{80}$ $\mu\text{m}$	Ratio of $F_{80}$ Particle	Ratio of Nominal / $F_{80}$	Crushing HPGR $P_{80}$ , $\mu\text{m}$	Ratio of Reduction HPGR, $R_{80}$	Attrition $P_{80}$ $\mu\text{m}$	Ratio of Reduction Attrition, $R_{80}$
Standard	-12.7	--	8900.00	--	1.43	--	--	--	--
Standard	-2	6.35	1410.00	6.31	1.42	--	--	550.00	2.56
Composite C, 0.38 m/s	-9	1.41	3152.00	2.82	2.86	289.00	10.91	95.00	3.04
Composite C, 0.77 m/s	-9	1.41	3152.00	2.82	2.86	205.00	15.38	83.00	2.47

- These tables showed that the feed preparation procedure was quite consistent for the Standard Phosphate Ore Composites producing similar Ratio of  $F_{80}$  Particle than that obtained for the Nominal Size, and the same Ratio of Nominal/ $F_{80}$  Sizes of the Standard MPH Phosphate Ore Composite Samples than that of the Composites C Ratio of Nominal Size.
- The Ratio of Nominal Sizes of the Standard -12.7 mm to Composite C, -9 mm was only 1.41, but the Ratio of  $F_{80}$  produced for Composite C was 2.82, and that of Nominal/ $F_{80}$  for Composite C was 2.86. This data indicated that the preparation procedure of the MPH Phosphate Ore, Composite C produced material twice finer than that produced with the Standard MPH Composite samples, probably due to the presence of higher  $\text{Al}_2\text{O}_3$ .
- The presence of high  $\text{Al}_2\text{O}_3$  and low  $\text{P}_2\text{O}_5$  in Composite C reduced the strength of the phosphate ore, and increased its plasticity. This is reflected in the HPGR comminution with high reduction ratios. The data in Table 1 clearly showed a soft ore and the effect of



plasticity on HPGR comminution since Test 3 (at 0.38 m/s Rolls Speed) resulted in a much lower  $R_{80}$  (12.61) than that  $R_{80}$  (21.01) of Test 6 (0.77 m/s Rolls Speed) both at 70 bar of Applied Pressure. Table 3 showed a soft phosphate ore and the same plasticity effect using HPGR. Test 2 (at 0.38 m/s Rolls Speed) resulted in a much lower  $R_{80}$  (10.91) than that  $R_{80}$  (15.38) of Test 5 (0.77 m/s Rolls Speed) both at 50 bar of Applied Pressure. In the case of Table 2 for tests at 40 bar of Applied Pressure, the results for Test 1 are in agreement with those of Tests 2 and 3, showing an  $R_{80}$  of 11.85 at 0.38 m/s Rolls Speed. However, Test 4 showed  $R_{80}$  of only 7.98 at 0.77 m/s Rolls Speed, which is out of sequence with the  $R_{80}$  reported for Test 5 and 6 at 0.77 m/s Rolls Speed. This is related to the coarse feed to the attrition scrubbing (product of the HPGR crushing) of 395  $\mu\text{m}$  (?). However, the reduction of the strength of the phosphate ore is clearly shown since the attrition  $R_{80}$  produced was 4.16, the highest of all tests.

- The effect of micro-cracking and residual stresses produced during HPGR comminution in the attrition scrubbing was demonstrated by the increase in the overall  $R_{80}$  of all tests. Test 3 reported  $R_{80}$  of 2.65 and Test 6, 1.77 for an overall  $R_{80}$  of 34.26 and 36.65, respectively, with respect to the attrition of the Standard MPH Phosphate Ore Composite (2.56 and overall of 16.18). Test 2 showed  $R_{80}$  of 3.04 and Test 5, 2.47 for an overall  $R_{80}$  of 33.18 and 37.98, respectively; whereas, Test 1 reported  $R_{80}$  of 2.80 and Test 4,  $R_{80}$  of 4.16 for an overall  $R_{80}$  of 33.18 for both tests. Since attrition scrubbing should clean the surfaces and break agglomerates of particles of different mineralogical species from fines not actually ground, the higher  $R_{80}$  for attrition of Composite C samples could be attributed to the weakening of the grain border between different mineral species (micro-cracks).
- Consequently, the selection of the operating conditions of the HPGR will have to take into consideration the  $\text{Al}_2\text{O}_3$  and  $\text{P}_2\text{O}_5$  content of Composite C and both the capacity and Specific Net Comminution Energy ( $E_{cs(\text{net})}$ ) to achieve the highest  $\text{Al}_2\text{O}_3$  rejection and the highest  $\text{P}_2\text{O}_5$  recovery without excessive grinding of phosphate (Test 4). These will be used to extrapolate the effect of the operating parameters to MPH Composite A and B to avoid under or over-grinding of the material, and limiting grinding of  $\text{P}_2\text{O}_5$ . Under these conditions, it will be possible to predict the highest recovery of  $\text{P}_2\text{O}_5$  with the highest rejection of  $\text{Al}_2\text{O}_3$ ; thus, the lowest  $\text{Al}_2\text{O}_3$  grade in the Phosphate Concentrate. This is presented in Excel File KEMWorks-PN2069-HPGR-K12023 MPH AT90\_91 and explained below.

### **HPGR Test 3 and Attrition Scrubbing Tests 86 and 87**

- From the HPGR Test 3 and Duplicate Test plots of Particle Size Distribution (PSD)  $\text{Al}_2\text{O}_3$ ,  $\text{P}_2\text{O}_5$ , and  $\text{SiO}_2$  Distributions for MPH Phosphate Ore Composite C, the locus of the curves clearly showed that  $\text{Al}_2\text{O}_3$  bearing minerals were preferentially ground resulting in lower recovery in the 2360x38- $\mu\text{m}$  material, 13.42% (84.93% rejection in the -38- $\mu\text{m}$  size fraction); whereas,  $\text{P}_2\text{O}_5$  recovery on the 2360x38- $\mu\text{m}$  size fraction was 38.11% (55.88% losses in the -38- $\mu\text{m}$  material). The  $\text{SiO}_2$  recovery in the 2360x38- $\mu\text{m}$  size fraction being somewhere in between at 29.62% (64.63% rejection in the -38- $\mu\text{m}$  size fraction).  $\text{SiO}_2$  Distribution curve was almost identical to that of the Weight Distribution (yield), reporting 27.87% yield in the 2360x38- $\mu\text{m}$  size fraction. This

demonstrates that selective grinding of Al<sub>2</sub>O<sub>3</sub> bearing minerals takes place upon using HPGR due to the Bed Comminution Mechanism.

- HPGR Test 3 and Duplicate (70 bar and 0.38 m/s Rolls Speed) resulted in a drop in the Al<sub>2</sub>O<sub>3</sub> grade in the 2360x38- $\mu$ m product from a feed grade of 11.95% Al<sub>2</sub>O<sub>3</sub> to a product containing 5.75% Al<sub>2</sub>O<sub>3</sub>, a reduction of 2.08 times, which is the same as that for the Standard MPH Composite sample submitted to crushing and Attrition (4.10% Al<sub>2</sub>O<sub>3</sub> to 1.98% Al<sub>2</sub>O<sub>3</sub>).
- When the product of the HPGR Test 3 and Duplicate were submitted to our attrition process as reported in MPH Attrition Tests 86 and 87, respectively, the results were improved. These tests showed that the locus of the PSD, Al<sub>2</sub>O<sub>3</sub>, P<sub>2</sub>O<sub>5</sub>, and SiO<sub>2</sub> for MPH Phosphate Ore Composite C were in agreement with the concept of selective grinding with the Al<sub>2</sub>O<sub>3</sub> bearing minerals being preferentially ground with respect to P<sub>2</sub>O<sub>5</sub> and SiO<sub>2</sub> bearing minerals. The data showed that Al<sub>2</sub>O<sub>3</sub> recovery in the 2360x20- $\mu$ m size fraction decreased to 9.47% (89.67% of Al<sub>2</sub>O<sub>3</sub> rejected in the -20- $\mu$ m material), the P<sub>2</sub>O<sub>5</sub> recovery in the 2360x20- $\mu$ m product being 35.30% with P<sub>2</sub>O<sub>5</sub> losses of 61.26% in the -20- $\mu$ m size fraction. SiO<sub>2</sub> Distribution showed a recovery in the 2360x20- $\mu$ m material of 31.41% (63.84% rejection in the -20- $\mu$ m size fraction). As in the case of the HPGR Test 3 results, the locus of the Distributions curves for SiO<sub>2</sub> was somewhere in between that of the P<sub>2</sub>O<sub>5</sub> and Al<sub>2</sub>O<sub>3</sub>, and closer to the locus of the Weight Distribution curve (yield), showing 27.76% yield in the 2360x20- $\mu$ m size fraction with 68.42% in the -20- $\mu$ m.
- MPH Phosphate Attrition Tests 86 and 87 reported a further drop in the Al<sub>2</sub>O<sub>3</sub> grade to 4.09% Al<sub>2</sub>O<sub>3</sub> in the 2360x20- $\mu$ m product from an overall reduction of Al<sub>2</sub>O<sub>3</sub> of 2.93 times from 11.98% Al<sub>2</sub>O<sub>3</sub> in the feed to the system. These results corresponded to a better reduction in Al<sub>2</sub>O<sub>3</sub> grade than that obtained for the Standard MPH Phosphate Ore Composite sample after crushing and attrition (2.07 times).
- Even though over-grinding occurred due to the soft MPH Phosphate Ore Composite C and the high pressure applied (70 bar), the recovery of P<sub>2</sub>O<sub>5</sub> (35.30%) was significantly higher than that of the yield (27.76%) with 84.67% rejection of Al<sub>2</sub>O<sub>3</sub>. This also demonstrated that selective grinding took place, the right HPGR operating conditions (Applied Pressure and Rolls Speed) requiring to be determined.

#### **HPGR Test 6 and Attrition Scrubbing Tests 88 and 89**

- In the case of the HPGR Test 6 and Duplicate Test, the PSD, Al<sub>2</sub>O<sub>3</sub>, P<sub>2</sub>O<sub>5</sub>, and SiO<sub>2</sub> locus of the Distribution curves showed similar results than those presented for HPGR Test 3 and Duplicate. However, Al<sub>2</sub>O<sub>3</sub> bearing minerals were further ground resulting in a recovery of 12.15% in the 2360x38- $\mu$ m size fraction (86.66% of Al<sub>2</sub>O<sub>3</sub> rejection in the -38- $\mu$ m material). On the other hand, P<sub>2</sub>O<sub>5</sub> recovery also decreased but in a smaller proportion to 35.57% in the 2360x38- $\mu$ m product with P<sub>2</sub>O<sub>5</sub> losses of 60.33% in the -38- $\mu$ m material. Again, SiO<sub>2</sub> locus of the Distribution curve was in between, and similar to that of the Weight Distribution (yield). SiO<sub>2</sub> recovery in the 2360x38- $\mu$ m size fraction was 28.49% with rejection of SiO<sub>2</sub> of 67.12% in the -38- $\mu$ m material, the Weight Distribution (yield being 26.65% for 2380x38- $\mu$ m product and 69.67% for -38- $\mu$ m size fraction).

- By using 70 bar and 0.77 m/s Rolls Speed in the HPGR Test 6, the Al<sub>2</sub>O<sub>3</sub> grade drop to 5.51% Al<sub>2</sub>O<sub>3</sub> in the 2360x38- $\mu$ m product from a feed of 12.08% Al<sub>2</sub>O<sub>3</sub>; thus, a reduction of 2.32 times. This is higher than the reduction in Al<sub>2</sub>O<sub>3</sub> grade obtained by the Standard System (2.07 times).
- The Attrition process was applied to the HPGR Test 6 and its Duplicate as shown in the results of Attrition Tests 88 and 89, respectively. Here, the locus of the curves for the PSD, Al<sub>2</sub>O<sub>3</sub>, P<sub>2</sub>O<sub>5</sub>, and SiO<sub>2</sub> Distributions showed that selective grinding of Al<sub>2</sub>O<sub>3</sub> bearing minerals resulted in a recovery of 9.40% of Al<sub>2</sub>O<sub>3</sub> for the 2360x20- $\mu$ m product with a rejection of 89.96% of Al<sub>2</sub>O<sub>3</sub> in the -20- $\mu$ m size fraction. P<sub>2</sub>O<sub>5</sub> recovery in the 2360x20- $\mu$ m product was decreased to 34.59% with an increase in losses to 62.74% in the -20- $\mu$ m size fraction. SiO<sub>2</sub> recovery in the 2360x20- $\mu$ m product was 31.41% with higher rejection in the -20- $\mu$ m material of 64.83% than that obtained for Tests 86 and 87, indicating additional grinding of this material, but with similar Weight Distribution (yield) of 27.63% in the 2360x20- $\mu$ m product, and 69.42% in the -20- $\mu$ m size fraction.
- The Al<sub>2</sub>O<sub>3</sub> grade for the HPGR Attrition Tests 88 and 89 resulted in 4.11% Al<sub>2</sub>O<sub>3</sub> grade for the 2360x20- $\mu$ m size fraction, and a reduction of Al<sub>2</sub>O<sub>3</sub> grade of 2.93 times. Thus, a marginal improvement over those reductions in Al<sub>2</sub>O<sub>3</sub> obtained for HPGR + Attrition Test 86 and 87, but superior than that for the Standard MPH Phosphate Ore Composite samples.
- Further over-grinding of Composite C sample using 0.77 m/s Rolls Speed at 70 bar of Applied Pressure resulted in a lower P<sub>2</sub>O<sub>5</sub> recovery (34.59%) than that obtained for 0.38 m/s Rolls Speed (35.30%) on the 2360x20- $\mu$ m size fraction. On the other hand, a marginal increase in Al<sub>2</sub>O<sub>3</sub> in the -20- $\mu$ m was observed from 89.67% to 89.96% for 0.38 m/s and 0.77 m/s Rolls Speed, respectively with almost the same yields, 27.76% for 0.38 m/s Rolls Speed, and 27.63% for 0.77 m/s Rolls Speed.

### **HPGR Tests 1, 2, and Attrition Scrubbing Tests 90, and 91**

- Again, from the HPGR Test 1 and Test 2 plots of Particle Size Distribution (PSD) Al<sub>2</sub>O<sub>3</sub>, P<sub>2</sub>O<sub>5</sub>, and SiO<sub>2</sub> Distributions for MPH Phosphate Ore Composite C, the locus of the curves clearly showed that Al<sub>2</sub>O<sub>3</sub> bearing minerals were preferentially ground resulting in lower recovery in the 2360x38- $\mu$ m material for Test 1 (40 bar and 0.38 m/s Rolls Speed), 13.93% (84.61% rejection in the -38- $\mu$ m size fraction); whereas, P<sub>2</sub>O<sub>5</sub> recovery on the 2360x38- $\mu$ m size fraction was 39.74% (55.04% losses in the -38- $\mu$ m material). The SiO<sub>2</sub> recovery for Test 1 in the 2360x38- $\mu$ m size fraction was somewhere in between at 29.65% (63.93% rejection in the -38- $\mu$ m size fraction). SiO<sub>2</sub> Distribution curve was almost identical to that of the Weight Distribution (yield), reporting 28.27% yield in the 2360x38- $\mu$ m size fraction and 66.65% in the -38- $\mu$ m size fraction. This demonstrates that selective grinding of Al<sub>2</sub>O<sub>3</sub> takes place upon using HPGR due to the Bed Comminution Mechanism.
- HPGR Test 1 (40 bar and 0.38 m/s Rolls Speed) resulted in a drop in the Al<sub>2</sub>O<sub>3</sub> grade in the 2360x38- $\mu$ m product from a feed grade of 11.89% Al<sub>2</sub>O<sub>3</sub> to a product containing 6.09% Al<sub>2</sub>O<sub>3</sub>, a reduction of 1.95 times, which is lower than that for the Standard MPH Composite sample submitted to crushing and attrition (4.10% Al<sub>2</sub>O<sub>3</sub> to 1.98% Al<sub>2</sub>O<sub>3</sub>) a reduction of 2.07.

- When the product of the HPGR Test 1 was submitted to our attrition process as reported in MPH Attrition Test 90 the results were improved. These test showed that the locus of the PSD, Al<sub>2</sub>O<sub>3</sub>, P<sub>2</sub>O<sub>5</sub>, and SiO<sub>2</sub> for MPH Phosphate Ore Composite C were in agreement with the concept of selective grinding with the Al<sub>2</sub>O<sub>3</sub> bearing minerals being preferentially ground with respect to P<sub>2</sub>O<sub>5</sub> and SiO<sub>2</sub> bearing minerals. The data showed that Al<sub>2</sub>O<sub>3</sub> recovery in the 2360x20- $\mu$ m size fraction decreased to 10.51% (88.65% of Al<sub>2</sub>O<sub>3</sub> rejected in the -20- $\mu$ m material), the P<sub>2</sub>O<sub>5</sub> recovery in the 2360x20- $\mu$ m product being 37.59% with P<sub>2</sub>O<sub>5</sub> losses of 58.38% in the -20- $\mu$ m size fraction. SiO<sub>2</sub> Distribution showed a recovery in the 2360x20- $\mu$ m material of 31.86% (63.05% rejection in the -20- $\mu$ m size fraction). As in the case of the HPGR Test 1 results, the locus of the Distributions curves for SiO<sub>2</sub> was somewhere in between that of the P<sub>2</sub>O<sub>5</sub> and Al<sub>2</sub>O<sub>3</sub>, and closer to the locus of the Weight Distribution curve (yield), showing 28.45% yield in the 2360x20- $\mu$ m size fraction and 67.45% in the -20- $\mu$ m size fraction.
- MPH Phosphate Attrition Test 90 reported a further drop in the Al<sub>2</sub>O<sub>3</sub> grade to 4.39% Al<sub>2</sub>O<sub>3</sub> in the 2360x20- $\mu$ m product from an overall reduction of Al<sub>2</sub>O<sub>3</sub> of 2.71 times from 11.89% Al<sub>2</sub>O<sub>3</sub> in the feed to the system. These results corresponded to a better reduction in Al<sub>2</sub>O<sub>3</sub> grade than that obtained for the Standard MPH Phosphate Ore Composite sample after crushing and attrition (2.07 times).
- Even though over-grinding occurred due to the soft MPH Phosphate Ore Composite C for the pressure applied (40 bar), the recovery of P<sub>2</sub>O<sub>5</sub> (37.59%) was significantly higher than that of the yield (28.45%) with 88.65% rejection of Al<sub>2</sub>O<sub>3</sub>. This also demonstrated that selective grinding took place, the right HPGR operating conditions (Applied Pressure and Rolls Speed) requiring to be determined.
- In the case of the HPGR Test 2 (50 bar and 0.38 m/s), the PSD, Al<sub>2</sub>O<sub>3</sub>, P<sub>2</sub>O<sub>5</sub>, and SiO<sub>2</sub> locus of the Distribution curves showed similar results than those presented for HPGR Test 1. Al<sub>2</sub>O<sub>3</sub> bearing minerals were ground resulting in a recovery of 14.71% in the 2360x38- $\mu$ m size fraction (83.92% of Al<sub>2</sub>O<sub>3</sub> rejection in the -38- $\mu$ m material). On the other hand, P<sub>2</sub>O<sub>5</sub> recovery was 40.44% in the 2360x38- $\mu$ m product with P<sub>2</sub>O<sub>5</sub> losses of 54.79% in the -38- $\mu$ m material. Again, SiO<sub>2</sub> locus of the Distribution curve was in between, and similar to that of the Weight Distribution (yield). SiO<sub>2</sub> recovery in the 2360x38- $\mu$ m size fraction was 30.39% with rejection of SiO<sub>2</sub> of 63.87% in the -38- $\mu$ m material, the Weight Distribution reporting 29.04% in the 2380x38- $\mu$ m size fraction with 66.18% in the -38- $\mu$ m size fraction.
- Using 0.38 m/s Rolls Speed in the HPGR Test 2, the Al<sub>2</sub>O<sub>3</sub> grade drop to 6.37% Al<sub>2</sub>O<sub>3</sub> in the 2360x38- $\mu$ m product from a feed of 11.93% Al<sub>2</sub>O<sub>3</sub>; thus, a reduction of 1.87 times. This is lower than the reduction in Al<sub>2</sub>O<sub>3</sub> grade obtained by the Standard System (2.07 times).
- The Attrition process was applied to the HPGR Test 2 as shown in the results of Attrition Test 91. Here, the locus of the curves for the PSD, Al<sub>2</sub>O<sub>3</sub>, P<sub>2</sub>O<sub>5</sub>, and SiO<sub>2</sub> Distributions showed that selective grinding of Al<sub>2</sub>O<sub>3</sub> bearing minerals resulted in a recovery of 10.52% of Al<sub>2</sub>O<sub>3</sub> for the 2360x20- $\mu$ m product with a rejection of 88.48% of Al<sub>2</sub>O<sub>3</sub> in the -20- $\mu$ m size fraction. P<sub>2</sub>O<sub>5</sub> recovery in the 2360x20- $\mu$ m product was decreased to 36.57% with an increase in losses to 59.68% in the -20- $\mu$ m size fraction. SiO<sub>2</sub> recovery in the 2360x20- $\mu$ m product was 31.69% with higher SiO<sub>2</sub> rejection in the -20- $\mu$ m material of 63.09% than that obtained for Tests 90, indicating additional

grinding of this material, but with similar Weight Distribution (yield) of 28.28% in the 2360x20- $\mu\text{m}$  product, and 67.51% in the -20- $\mu\text{m}$  size fraction.

- The  $\text{Al}_2\text{O}_3$  grade for the HPGR Attrition Test 91 resulted in 4.44%  $\text{Al}_2\text{O}_3$  grade for the 2360x20- $\mu\text{m}$  size fraction, and a reduction of  $\text{Al}_2\text{O}_3$  grade of 2.69 times. Thus, a marginal difference over that reduction in  $\text{Al}_2\text{O}_3$  obtained for HPGR + Attrition Test 90, but superior than that for the Standard MPH Phosphate Ore Composite samples.

### **HPGR Tests 4, 5, and Attrition Scrubbing Tests 92, and 93**

- From the HPGR Test 4 and Test 5 plots of Particle Size Distribution (PSD)  $\text{Al}_2\text{O}_3$ ,  $\text{P}_2\text{O}_5$ , and  $\text{SiO}_2$  Distributions for MPH Phosphate Ore Composite C, the locus of the curves clearly showed that  $\text{Al}_2\text{O}_3$  bearing minerals were preferentially ground resulting in lower recovery in the 2360x38- $\mu\text{m}$  material for Test 4 (40 bar and 0.77 m/s Rolls Speed), 17.43% (80.81% rejection in the -38- $\mu\text{m}$  size fraction); whereas,  $\text{P}_2\text{O}_5$  recovery on the 2360x38- $\mu\text{m}$  size fraction was 42.45% (53.04% losses in the -38- $\mu\text{m}$  material). The  $\text{SiO}_2$  recovery for Test 4 in the 2360x38- $\mu\text{m}$  size fraction was somewhere in between at 32.82% (61.24% rejection in the -38- $\mu\text{m}$  size fraction).  $\text{SiO}_2$  Distribution curve was almost identical to that of the Weight Distribution (yield), reporting 31.45% yield in the 2360x38- $\mu\text{m}$  size fraction and 63.66% in the -38- $\mu\text{m}$  size fraction. This demonstrates that selective grinding of  $\text{Al}_2\text{O}_3$  bearing minerals takes place upon using HPGR due to the Bed Comminution Mechanism.
- HPGR Test 4 (40 bar and 0.77 m/s Rolls Speed) resulted in a drop in the  $\text{Al}_2\text{O}_3$  grade in the 2360x38- $\mu\text{m}$  product from a feed grade of 11.87%  $\text{Al}_2\text{O}_3$  to a product containing 6.90%  $\text{Al}_2\text{O}_3$ , a reduction of 1.72 times, which is lower than that for the Standard MPH Composite sample submitted to crushing and attrition (4.10%  $\text{Al}_2\text{O}_3$  to 1.98%  $\text{Al}_2\text{O}_3$ ) a reduction of 2.07.
- When the product of the HPGR Test 4 was submitted to our attrition process as reported in MPH Attrition Test 92 the results were improved. These test showed that the locus of the PSD,  $\text{Al}_2\text{O}_3$ ,  $\text{P}_2\text{O}_5$ , and  $\text{SiO}_2$  for MPH Phosphate Ore Composite C were in agreement with the concept of selective grinding with the  $\text{Al}_2\text{O}_3$  bearing minerals being preferentially ground with respect to  $\text{P}_2\text{O}_5$  and  $\text{SiO}_2$  bearing minerals. The data showed that  $\text{Al}_2\text{O}_3$  recovery in the 2360x20- $\mu\text{m}$  size fraction decreased to 10.45% (88.66% of  $\text{Al}_2\text{O}_3$  rejected in the -20- $\mu\text{m}$  material), the  $\text{P}_2\text{O}_5$  recovery in the 2360x20- $\mu\text{m}$  product being 36.83% with  $\text{P}_2\text{O}_5$  losses of 59.25% in the -20- $\mu\text{m}$  size fraction.  $\text{SiO}_2$  Distribution showed a recovery in the 2360x20- $\mu\text{m}$  material of 32.10% (62.83% rejection in the -20- $\mu\text{m}$  size fraction). As in the case of the HPGR Test 1 results, the locus of the Distributions curves for  $\text{SiO}_2$  was somewhere in between that of the  $\text{P}_2\text{O}_5$  and  $\text{Al}_2\text{O}_3$ , and closer to the locus of the Weight Distribution curve (yield), showing 28.36% yield in the 2360x20- $\mu\text{m}$  size fraction and 67.67% in the -38- $\mu\text{m}$  size fraction.
- MPH Phosphate Attrition Test 90 reported a further drop in the  $\text{Al}_2\text{O}_3$  grade to 4.38%  $\text{Al}_2\text{O}_3$  in the 2360x20- $\mu\text{m}$  product from an overall reduction of  $\text{Al}_2\text{O}_3$  of 2.71 times from 11.87%  $\text{Al}_2\text{O}_3$  in the feed to the system. These results corresponded to a better reduction in  $\text{Al}_2\text{O}_3$  grade than that obtained for the Standard MPH Phosphate Ore Composite sample after crushing and attrition (2.07 times).

- Even though over-grinding occurred due to the soft MPH Phosphate Ore Composite C for the pressure applied (40 bar), the recovery of  $P_2O_5$  (36.83%) was significantly higher than that of the yield (28.36%) with 88.66% rejection of  $Al_2O_3$ . This also demonstrated that selective grinding took place. The right HPGR operating conditions of Applied Pressure and Rolls Speed were considered to be those of this test due to the less excessive grinding, higher capacity, and lower specific net Comminution Energy  $E_{cs(net)}$ .
- In the case of the HPGR Test 5 (50 bar and 0.77 m/s), the PSD,  $Al_2O_3$ ,  $P_2O_5$ , and  $SiO_2$  locus of the Distribution curves showed similar results than those presented for HPGR Test 2.  $Al_2O_3$  minerals were ground resulting in a recovery of 13.88% in the 2360x38- $\mu m$  size fraction (84.68% of  $Al_2O_3$  rejection in the -38- $\mu m$  material). On the other hand,  $P_2O_5$  recovery was 37.60% in the 2360x38- $\mu m$  product with  $P_2O_5$  losses of 58.15% in the -38- $\mu m$  material. Again,  $SiO_2$  locus of the Distribution curve was in between, and similar to that of the Weight Distribution (yield).  $SiO_2$  recovery in the 2360x38- $\mu m$  size fraction was 29.83% with rejection of  $SiO_2$  of 65.38% in the -38- $\mu m$  material, the Weight Distribution (yield) being 28.06% for 2380x38- $\mu m$  product and 6791% for the -38- $\mu m$  size fraction.
- Using 0.77 m/s Rolls Speed in the HPGR Test 5, the  $Al_2O_3$  grade drop to 6.05%  $Al_2O_3$  in the 2360x38- $\mu m$  product from a feed of 11.97%  $Al_2O_3$ ; thus, a reduction of 1.98 times. This is lower than the reduction in  $Al_2O_3$  grade obtained by the Standard System (2.07 times).
- The Attrition process was applied to the HPGR Test 5 as shown in the results of Attrition Test 93. Here, the locus of the curves for the PSD,  $Al_2O_3$ ,  $P_2O_5$ , and  $SiO_2$  Distributions showed that selective grinding of  $Al_2O_3$  bearing minerals resulted in a recovery of 9.55% of  $Al_2O_3$  for the 2360x20- $\mu m$  product with a rejection of 89.91% of  $Al_2O_3$  in the -20- $\mu m$  size fraction.  $P_2O_5$  recovery in the 2360x20- $\mu m$  product was decreased to 34.70% with an increase in losses to 63.08% in the -20- $\mu m$  size fraction.  $SiO_2$  recovery in the 2360x20- $\mu m$  product was 31.72% with higher rejection in the -20- $\mu m$  material of 64.85% than that obtained for Tests 91, indicating additional grinding of this material, but with similar Weight Distribution (yield) of 27.75% in the 2360x20- $\mu m$  product, and 69.59% in the -20- $\mu m$  size fraction.
- The  $Al_2O_3$  grade for the HPGR Attrition Test 93 resulted in 4.12%  $Al_2O_3$  grade for the 2360x20- $\mu m$  size fraction, and a reduction of  $Al_2O_3$  grade of 2.91 times. Thus, a slight difference with that reduction in  $Al_2O_3$  obtained for HPGR + Attrition Test 92, and superior than that for the Standard MPH Phosphate Ore Composite samples.
- Further over-grinding of Composite C sample using 0.77 m/s Rolls Speed at 70 bar of Applied Pressure resulted in a lower  $P_2O_5$  recovery (34.59%) than that obtained 50 bar and 0.77 m/s Rolls Speed (34.70%) on the 2360x20- $\mu m$  size fraction. On the other hand, a marginal increase in  $Al_2O_3$  in the -20- $\mu m$  was observed from 89.91% to 89.96% for 50 bar and 70 bar at 0.77 m/s Rolls Speed, respectively with almost the same yields, 27.75% for 50 bar, and 27.63% for 70 bar.