



**PANGAEA**  
RESOURCES PTY Ltd.

# Petrophysical Report

## NT EP-167 – Manbulloo-S2

**Prepared For:** NT Department of Mines and Energy  
**Date:** 13-Aug-15  
**Revision No:** A

	<b>PETROPHYSICAL REPORT</b> <b>EP-167</b> <b>MANBULLOO-S2</b>	DOCUMENT:	1.0 WCR 1502
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## 1 INTRODUCTION AND OBJECTIVE

Manbulloo-S1 was the second of three stratigraphic core holes designed to assess the stratigraphy and hydrocarbon potential of the Western McArthur Basin.

Manbulloo-S1 reached a total depth (TD) of 1236.22 (mRT) at 13:30 on the 14<sup>th</sup> of August 2014. Open hole wireline data was acquired by Weatherford. Due to borehole condition, Gamma Ray (GR) was logging inside the drill pipe from TD to surface. The open hole tool was hung up at around 930 mRT, and wireline data was acquire from the Hang Up Depth (HUD) to the casing shoe.

Petrophysical analysis of wireline data was performed over the Barney Creek equivalent in the Manbulloo-S1. The main desired outputs are:

- Porosity
- Water Saturation

## 2 LOGGING DATA

Wireline data was acquired by Weatherford over the HQ (3.78 in.) open hole interval from hung up depth (~ 930.0 mRT) to 4-1/2 in. casing shoe (420.3 mRT). Table 1 presented available wireline data.

**Table 1. Wireline Logs**

Logging Run	Logging Suite
Run #1 (Inside the Drill Pipe)	Compact Gamma Ray/Temp (MCG)
Run #2 (Logged from Hang Up Depth)	Compact Gamma Ray/Temp (MCG)
	Compact Dual Neutron (MDN)
	Compact Photo Density (MPD)
	Compact Dual Laterlog (MDL)
	Compact Micro Resistivity (MMR)
	Compact Micro Imager (CMI) – for calipers only
Run #3 (Logged from Hang Up Depth)	Compact Sonic (MSS)
Run #3 (Logged from Hang Up Depth)	Velocity Check Shots (VCS)

CMI was run as the calipers tool only. The resistivity imager data was not acquired.

### 2.1 Log Quality Control

All tool calibrations were within tolerance.

All tool repeatability were within tolerance.

The following mud data was reported in the log header:

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**Table 2. Mud Properties in HQ (3.78 in.) Open Hole**

Mud Type:	KCL
Mud Weight:	1.04 g/c <sup>3</sup> (8.68 ppg)
Funnel Viscosity:	55 s
pH:	Not reported
Fluid Loss:	Not reported
Date/Time Circulation Stopped:	14-Aug-2014 19:00
Resistivity of Mud:	0.17 Ωm @ 25.0 °C
Resistivity of Mud Filtrate:	0.16 Ωm @ 25.0 °C
Resistivity of Mud Cake:	0.25 Ωm @ 25.0 °C

## 2.2 Borehole Temperature

**Table 3. Bottom Hole Temperature**

Time Reached TD	14-Aug-2014 13:30	Circulation Time	5.50 [hrs]	
Circulation Stopped	14-Aug-2014 19:00			
Services	Time @ TD	Time since Circ.	Temperature	Depth
		[hrs]	[°C]	[mRT]
Run # 1	14-Aug-2014 19:30	00.50	69.0	1236.00
Run # 2	15-Aug-2014 06:00	11.00	59.0	900.60
Run # 3	15-Aug-2014 14:00	19.00	65.0	930.70

The bottom hole static temperature (BHST) was not estimated because the bottom hole temperature was not measured at the same depth.

## 3 METHODOLOGY

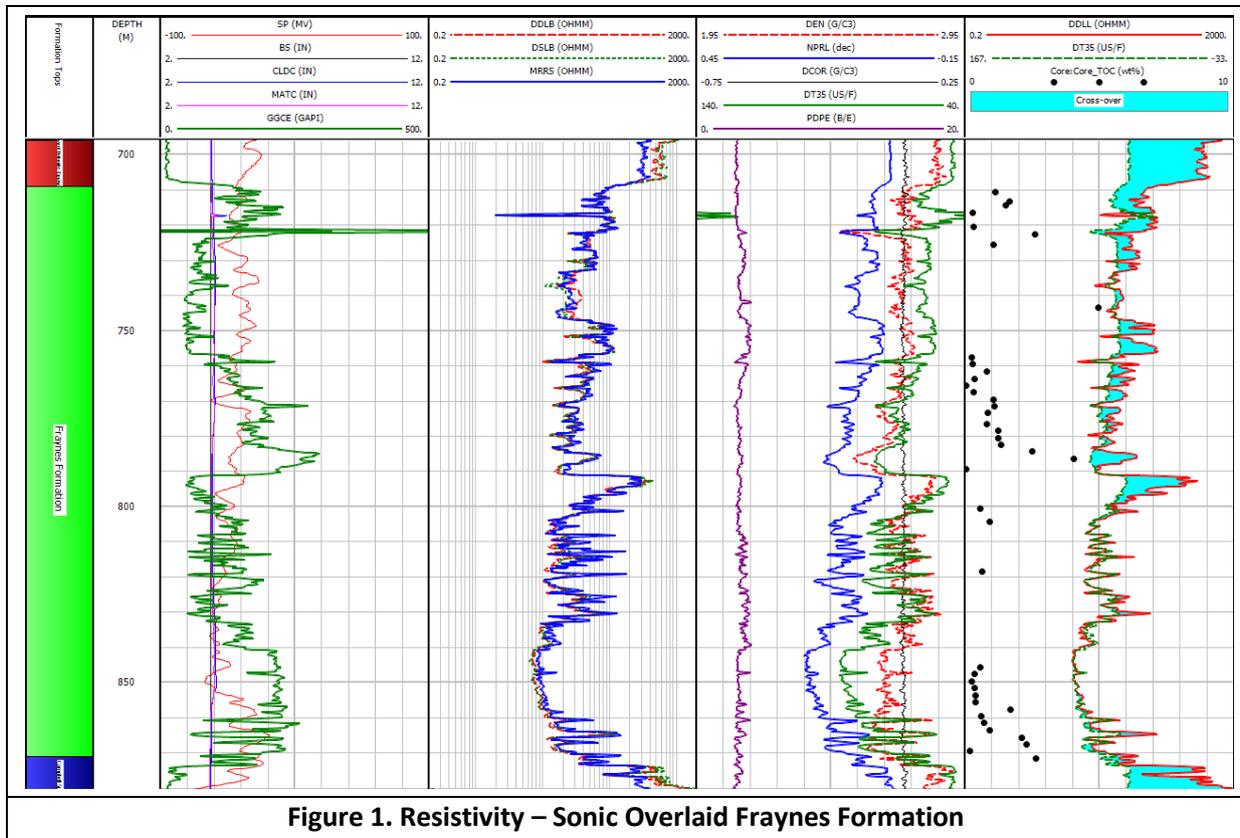
### 3.1 Total Organic Carbon

Figure 1 presented the complete Wireline data over the Fraynes Formation (Barney Creek Formation). Resistivity (DDLB) and Sonic (DT35) was plotted together on track # 6. DDLB and DT35 were overlain; Sonic – Resistivity cross-over indicated the presence of the Total Organic Carbon (TOC). Rock-Eval/TOC results agreed with the Wireline data.

TOC was estimated with the Schmoker method:

$$TOC = \frac{156.956}{\rho_b} - 58.271$$

Where  $\rho_b$  was the Bulk Density (DEN) in g/cc and TOC was reported in wt%.



### 3.2 Volume of Clay

Gamma Ray and Neutron – Density were used to estimate volume of clay. Data was calibrated with the XRD data. The Clay Volume was the smallest one from two methods.

### 3.3 Bulk Volume and Porosity

Base on XRD data and lithology description, multi-minerals models (probabilistic method) were used to solve for bulk volume and porosity.

### 3.4 Water Saturation

Water Saturation was computed using the Simandoux equation with default parameters ( $a = 1$ ,  $m = n = 2$ ).

Apparent Water Resistivity ( $R_{wa}$ ) was used to estimate the Formation Water Resistivity ( $R_w$ ).

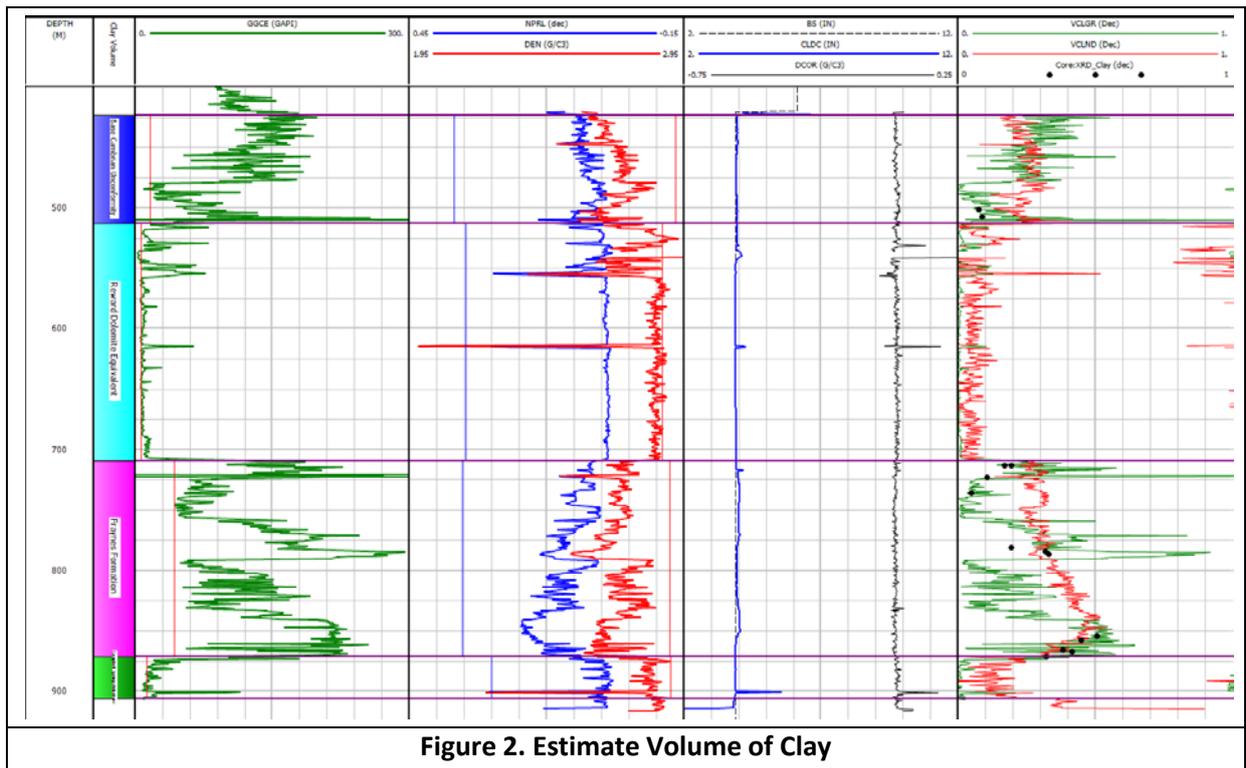
### 3.5 Cut-offs Summary

Table 4 presented the cut-offs value used to determine reservoir and pay thickness.



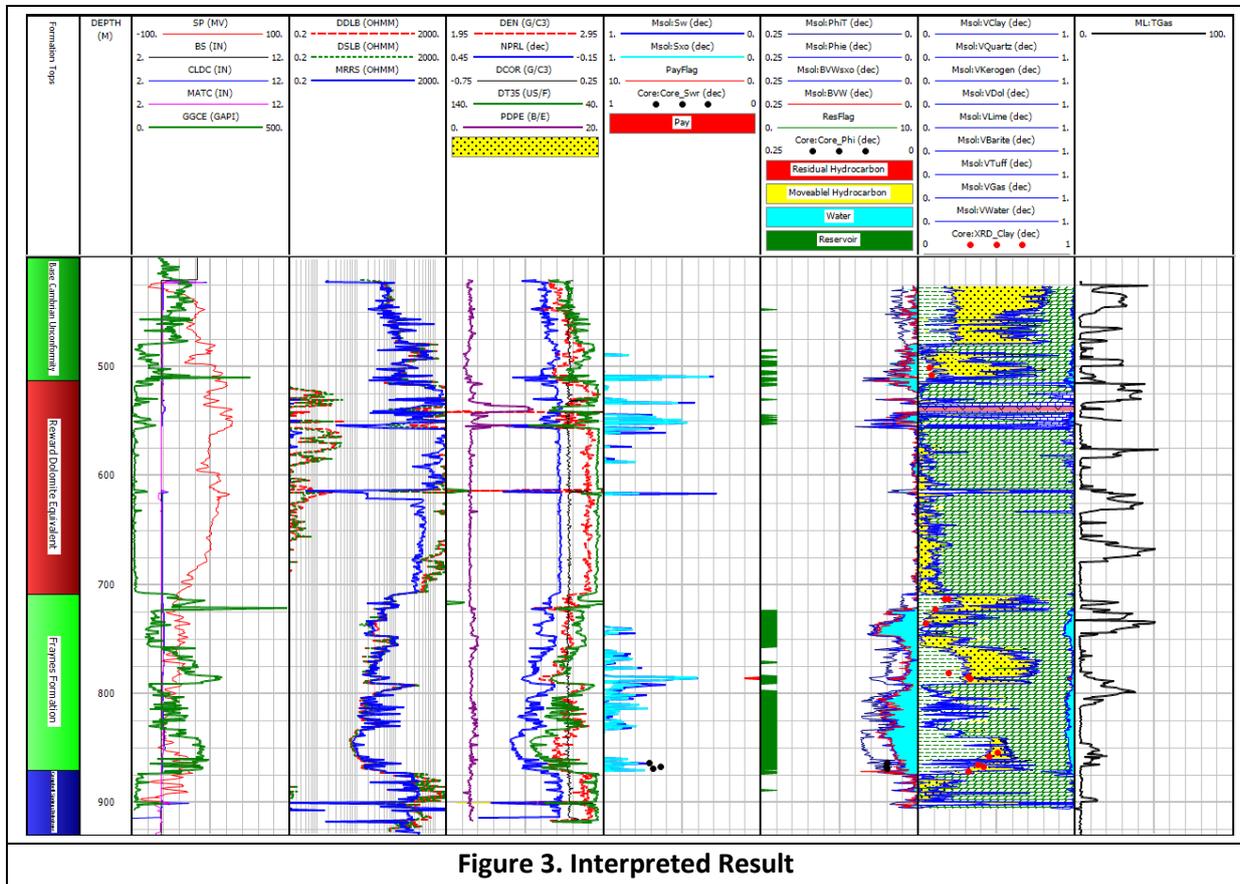
**Table 4. Cut-offs Used**

	Min. Thickness	PHIE	Sw	VClay
Reservoir	≥ 1.00	≥ 0.02		≤ 0.5
Pay	≥ 1.00	≥ 0.02	≤ 0.5	≤ 0.5



**Figure 2. Estimate Volume of Clay**

#### 4 INTERPRETED RESULT



Zone Name	Top	Bottom	Gross	Net	N/G	Av. Phi	Av. Sw	Av. VCl	Phi*H	PhiSo*H
<b>Reservoir</b>										
Fraynes Formation	709.00	871.00	162.00	113.65	0.702	0.044	0.945	0.200	4.96	0.270
<b>Pay</b>										
Fraynes Formation	709.00	871.00	162.00	1.60	0.01	0.048	0.413	0.266	0.08	0.05

**Table 5. Reservoir and Pay Summary**

#### 5 DISCUSSION

Wireline data and TOC lab results conform with each other and indicated that the penetrated formations have low TOC content.