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SANTOS LIMITED

**E. MERENIE WELL NO. 37
P3-230/250 TSO FRAC TREATMENT**

PR95-65

14 FEBRUARY 1996

DEPT OF MINES & ENERGY



P00110

**E. MEREEENIE WELL NO. 37
P3-230/250 TSO FRACTURE TREATMENT**

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14 February 1996

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SUMMARY

On 31 July 1995, a tip-screenout (TSO) fracture treatment was performed on Santos' East Mereenie Well No. 37 through "P3-190" and "P3-23/250" sand perforations at 5020-5083 ft. While a pre-frac PBU test was attempted, this failed. Reservoir properties were estimated to be an average permeability of 10 md, a skin of +20, and a reservoir pressure of 1770 psi (no depletion). The wellbore deviation through the pay was 28°.

Prior to the treatment, pre-frac tests were conducted to evaluate closure stress, fluid efficiency, and fracture geometry for final design formulation. The results indicated a closure pressure of 3280 psi and a fluid efficiency of 0.43 from pressure decline analysis. This gave an efficiency during injection, using the Mereenie correlation of decline to injection efficiency, of 0.20. A reasonably good model history match of the minifrac was obtained using (1) a stress of 4500 psi in the shalier region between the P3-230/250 and P3-120/130 alternative pay zone, (2) a modulus of 6.5×10^6 psi in the pay and $7.5 - 8 \times 10^6$ psi in the barriers, and (3) a leak-off coefficient of 0.005 ft/sq.rt. minute in the 190/230/250. This "calibrated" model was used to design the final treatment.

With the desire to limit fracture growth to below the P3-120/130, the final treatment design required 2000 gals of pad and an additional 3900 gals of gel carrying 14,800 lbs of 20/40 Carbo-Lite proppant at 0.5-8 ppg and at a rate of 15 bpm. The model-predicted TSO occurred at the beginning of the 3 ppg stage and net BHTP went from 1080 to 2700 psi with a corresponding average fracture width increase from 0.06 to 0.18 inches. Other fracture dimensions were a propped half-length of 116 ft, a maximum height of 123 ft (at base of 120/130), an average conductivity of 1874 md-ft, and an average in-situ concentration of 1.0 lbs/sq.ft.

The treatment was pumped fairly close to design, placing 106% (15,750 lbs) of the designed proppant amount in the fracture with 99% (5815 gals) of the design gel volume. The TSO did occur as predicted with a net BHTP gain of 1300 psi as compared to the design prediction of 1600 psi. To model history match this behavior required (1) relaxing the lower boundary stress from 5000 to 4500 psi and (2) reducing the leak-off coefficient from 0.005 to 0.0044 ft/sq.rt minute. Resultant dimensions were a propped

half-length of 118 ft, maximum height of 141 ft, an average conductivity of 1608 md-ft, and an average in-situ concentration of 0.9 lbs/sq.ft. Based on this analysis, the treatment came fairly close to design goals.

DISCUSSION

Introduction:

This report details the design, execution, and analysis of the tip-screenout (TSO) fracturing treatment performed in Santos' East Mereenie Well No. 37 on 31 July 1995. The treatment was pumped through Pacoota P3-190 and P3-230/250 perforations at 5020-5083 ft (MD), 4689-4745 ft (TVD), as shown in Fig. 1. Reservoir parameters were estimated to be an average permeability of 10 md, a reservoir pressure of 1770 psi (no depletion), and a BHT of 143°F. While a pressure buildup test was attempted, this failed. Skin, though, was expected to be high as observed on the EM35 and EM36 wells, i.e. approximately +20. Prior to the attempted PBU test, the well came on line at a clean oil rate of around 130 bopd before declining to a rate of 65 bopd after only 3 weeks (Fig. 2). The average porosity from log analysis was on the order of 9.5% and the estimated GOR was only 100 scf/stb. The wellbore deviation through the pay was 28°.

The fracture treatment, performed by Halliburton, was preceded with pre-fracture injection/decline tests to evaluate closure pressure, fluid efficiency, and fracture geometry for final design formulation. Bottomhole pressure was obtained with SRO wireline gauges during testing and with electronic memory gauges set in the tailpipe during the treatment. The following discusses the details of this testing and treatment.

Preliminary Fracture Treatment Design:

The objective of the EM #37 treatment was to obtain as much propped penetration as possible (≤ 100 ft) with an in-situ proppant concentration of at least 1.0 lb/sq.ft. without fracturing into the P3-120/130 alternative pay zone at 4643 ft-TVD (46 ft above top P3-190 perf). At the indicated BHT, 30 ppt borate XL gel (Boragel H3595) was recommended and 20/40 mesh Carbo-Lite was used to insure good conductivity. The design injection rate was 15 bpm with plans to pump down 2-7/8 inch tubing. Other design parameters included a modulus of 5.5×10^6 psi in the pay and $6.5-7.5 \times 10^6$ psi in the boundary layers (based on Mereenie correlation of modulus to porosity and EM35 and EM36 P3-230/250 treatment analysis), a toughness of 3000 psi/sq.rt. inch in all

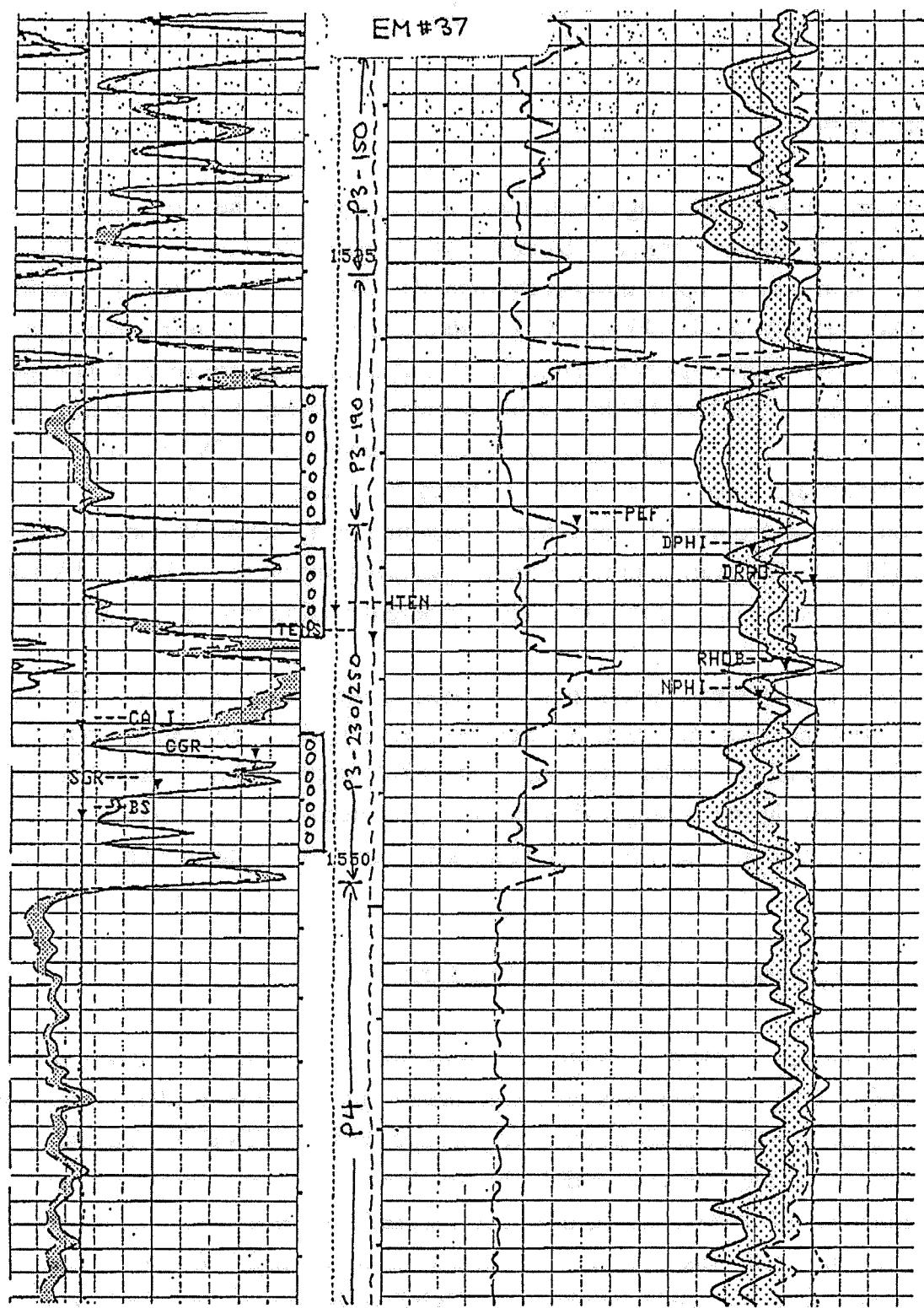


FIG. 1 - Log section thru pay interval and boundary layers, E. Mereenie 37.

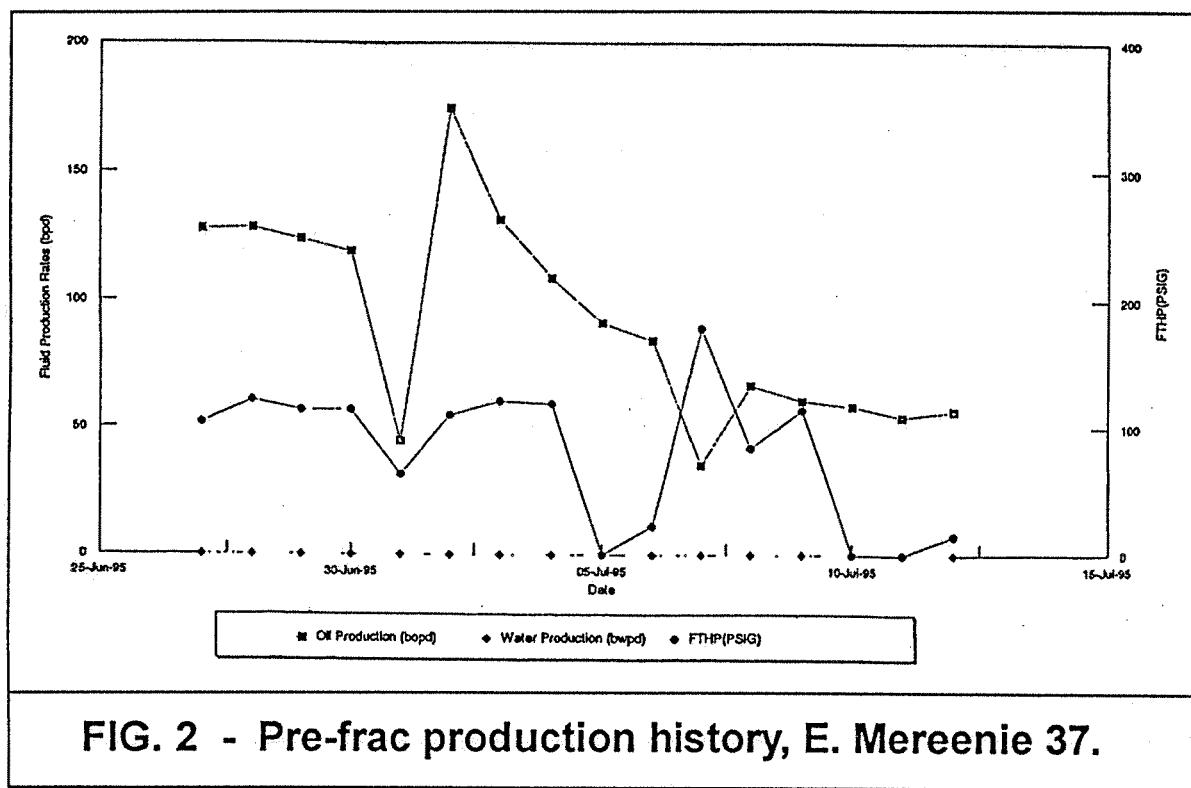


FIG. 2 - Pre-frac production history, E. Mereenie 37.

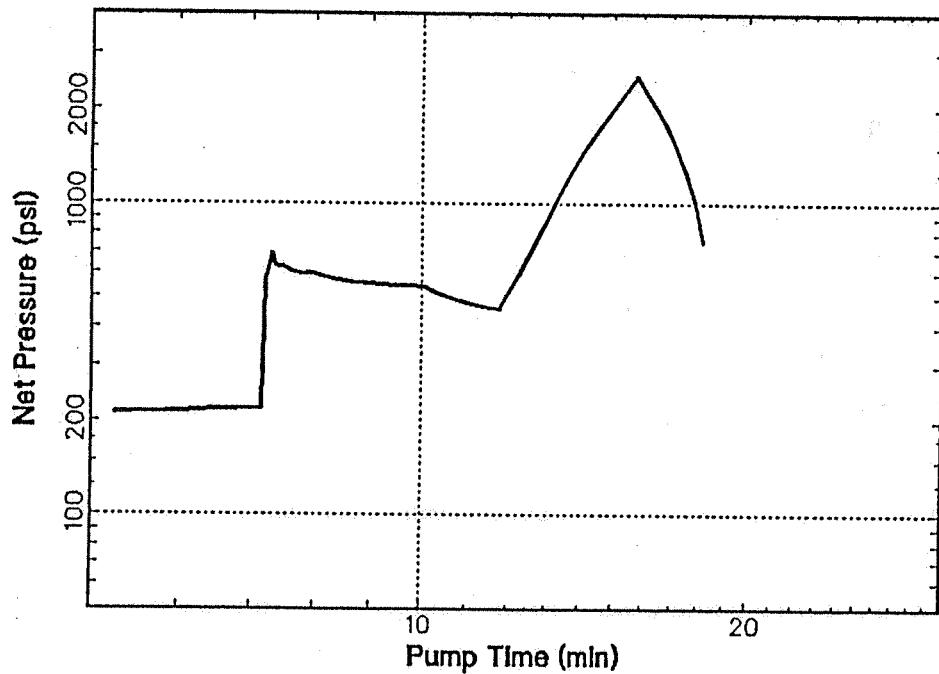
layers, and a leak-off coefficient of 0.012 ft/sq.rt. minute. From the established Mereenie correlation of reservoir to closure pressure, closure pressure was estimated to be on the order of 3400 psi in the pay and based on past treatment pressure response, boundary stresses were expected to be on the order of 3850-4000 psi.

Table 1 shows the preliminary design schedule. The pad size was limited to 2250 gals to prevent growth into the P3-120/130 and the resultant slurry stages included 2800 gals of gel carrying 8550 lbs of proppant at concentrations of 0.5-6 ppg. With multiple zones perforated, i.e. P3-190 and 230/250, and distinct shale layers between these, the preliminary design looked at three possible fracture initiation schemes to evaluate height growth - (1) across the entire perforated interval, (2) in only the P3-190, and (3) in only the P3-230/250. For the first scheme, the model-predicted a TSO in the 1.0 ppg stage, with net BHTP going from 460 to 2530 psi over the remainder of the treatment (Fig. 3). Model-predicted dimensions were a propped half-length of 43 ft, a maximum height at the wellbore of 100 ft (top at 4649 ft or only 6 ft below the 120/130), an average conductivity of 2332 md-ft, and an average in-situ concentration of 1.2 lbs/sq.ft. These are shown in Figs. 4-6, with the model I/O included in Appendix Table A-1.

**TABLE 1 - Preliminary treatment design schedule,
E. Mereenie 37.**

| <u>Fluid Type</u> | <u>Slur. Vol.</u> (gal) | <u>Fluid Vol.</u> (gal) | <u>Prop Conc.</u> (ppg) | <u>Prop Amt.</u> (lbs) | <u>Avg. Q</u> (bpm) | <u>Pump t</u> (min) |
|-------------------|----------------------------|----------------------------|----------------------------|---------------------------|------------------------|------------------------|
| Boragel H3595 | 2250 | 2250 | 0.00 | 0 | 15.00 | 3.57 |
| Boragel H3595 | 511 | 500 | 0.50 | 250 | 15.00 | 0.81 |
| Boragel H3595 | 418 | 400 | 1.00 | 400 | 15.00 | 0.66 |
| Boragel H3595 | 435 | 400 | 2.00 | 800 | 15.00 | 0.69 |
| Boragel H3595 | 340 | 300 | 3.00 | 900 | 15.00 | 0.54 |
| Boragel H3595 | 353 | 300 | 4.00 | 1200 | 15.00 | 0.56 |
| Boragel H3595 | 488 | 400 | 5.00 | 2000 | 15.00 | 0.77 |
| Boragel H3595 | <u>632</u> | <u>500</u> | <u>6.00</u> | <u>3000</u> | <u>15.00</u> | <u>1.00</u> |
| | 5427 | 5050 | | 8550 | | 8.60 |

Note: Proppant 20/40 Carbo-Lite.



**FIG. 3 - Preliminary treatment design predicted net
BHTP, E. Mereenie 37.**

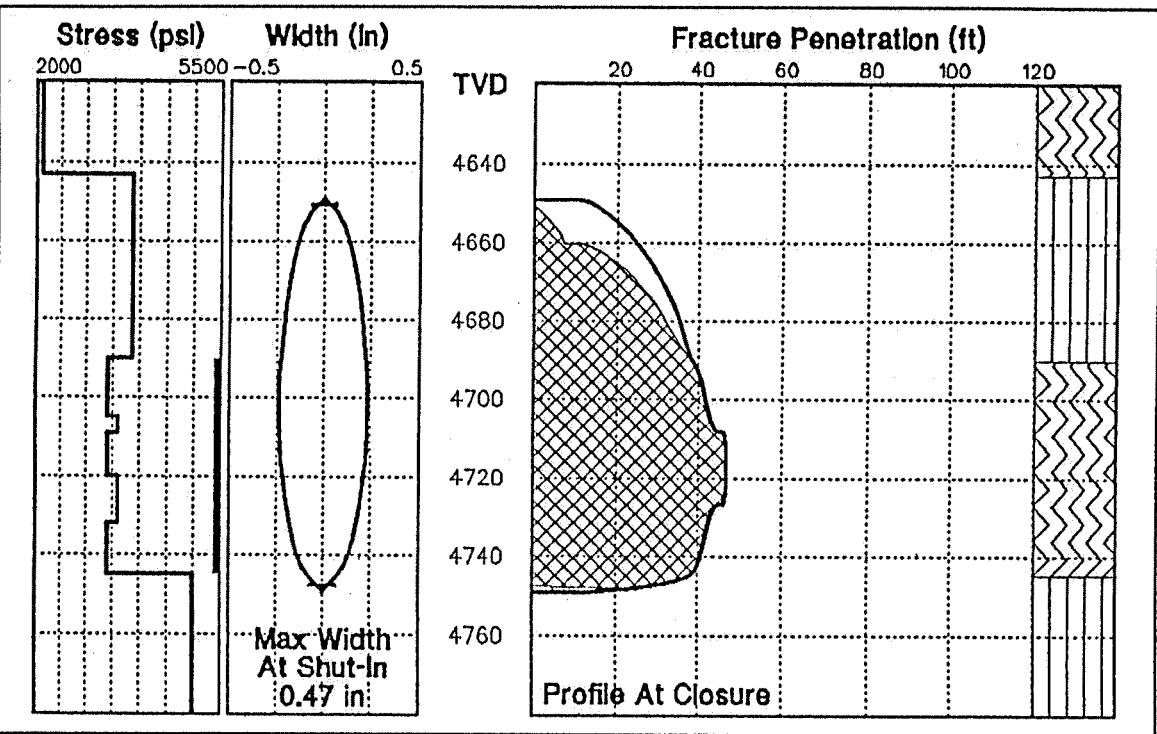


FIG. 4 - Preliminary treatment design predicted frac Geometry, E. Mereenie 37.

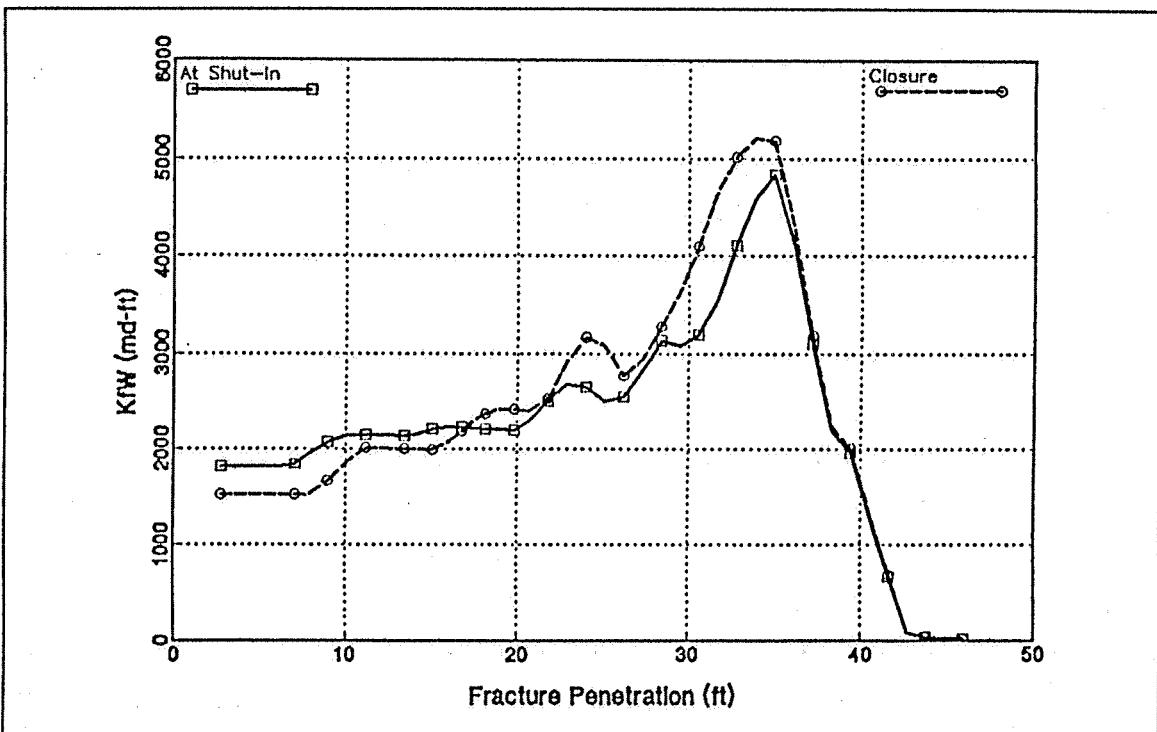


FIG. 5 - Preliminary treatment design predicted conductivity, E. Mereenie 37.

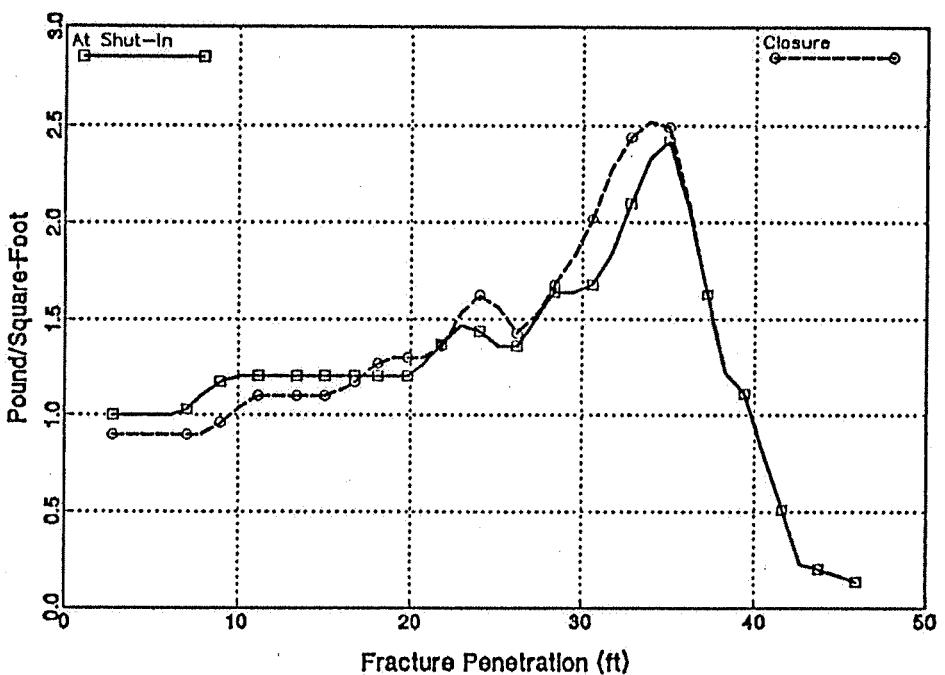


FIG. 6 - Preliminary treatment design predicted in-situ conc., E. Mereenie 37.

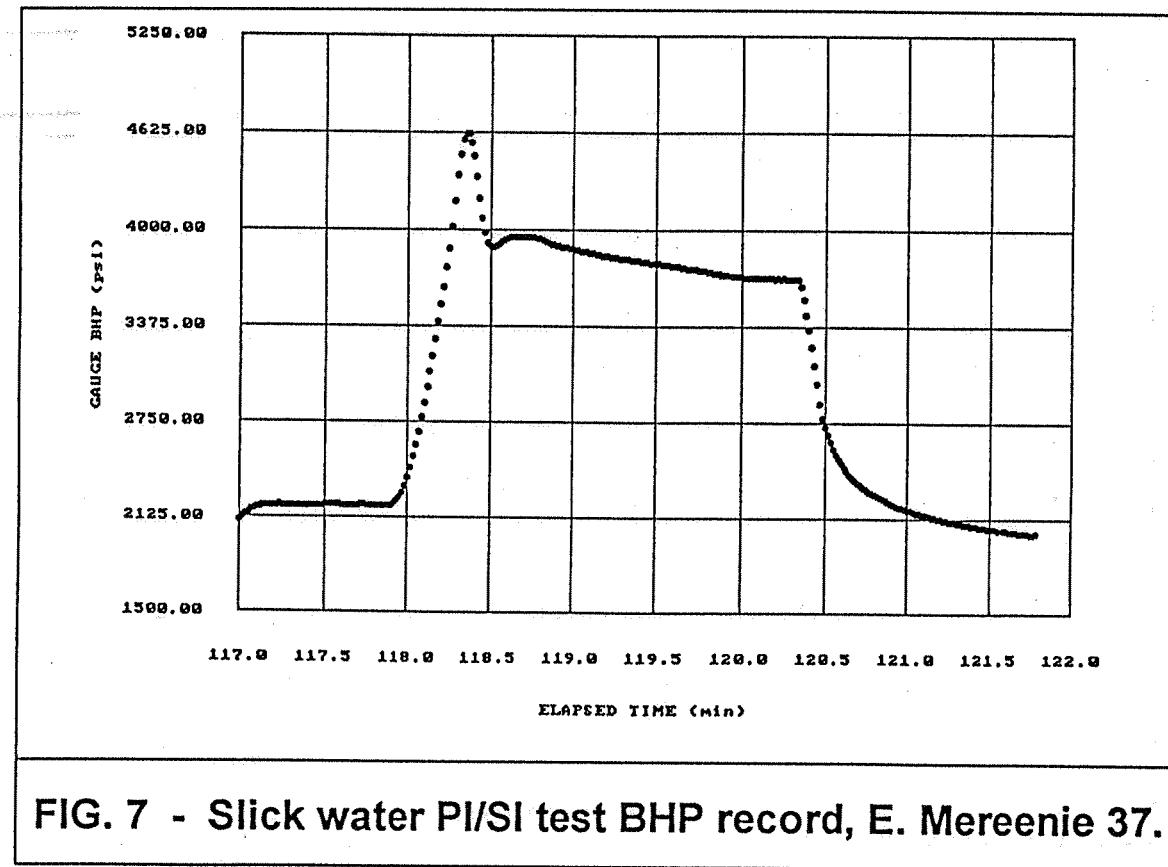
For the second scenario, with the modeled fracture initiating in only the P3-190, the TSO also occurred in the 1.0 ppg stage and net BHTP went from 430 to 2680 psi. Predicted dimensions in this case were a propped half-length of 48 ft, a maximum height of 100 ft (top at 4654 ft or 11 ft from the 120/130), an average conductivity of 3340 md-ft, and an average in-situ concentration of 1.8 lbs/sq.ft. (model I/O in Appendix Table A-2). In the final scheme, with the fracture initiating in only the P3-230/250, the TSO occurred in the 3 ppg stage, with net BHTP going from 430 to 1820 psi. Predicted dimensions were a propped half-length of 50 ft, a maximum height of 111 ft (top at 4649 ft or again only 6 ft from the 120/130), an average conductivity of 1810 md-ft, and an average in-situ concentration of 1.0 lbs/sq.ft. (model I/O in Appendix Table A-3).

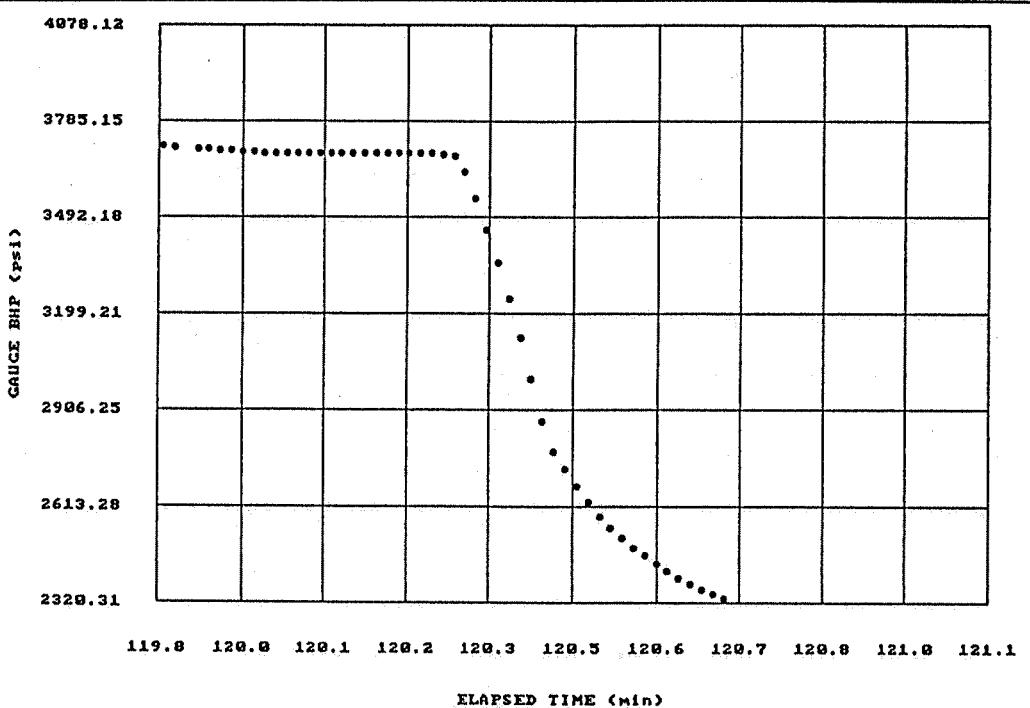
Based on these simulations, the preliminary treatment schedule was expected to give fracture dimensions sufficient to by-pass the near-wellbore damage region, provide good conductivity through this region, and limit vertical fracture growth to below the P3-120/130 alternative pay zone.

Pre-Frac Test Analysis:

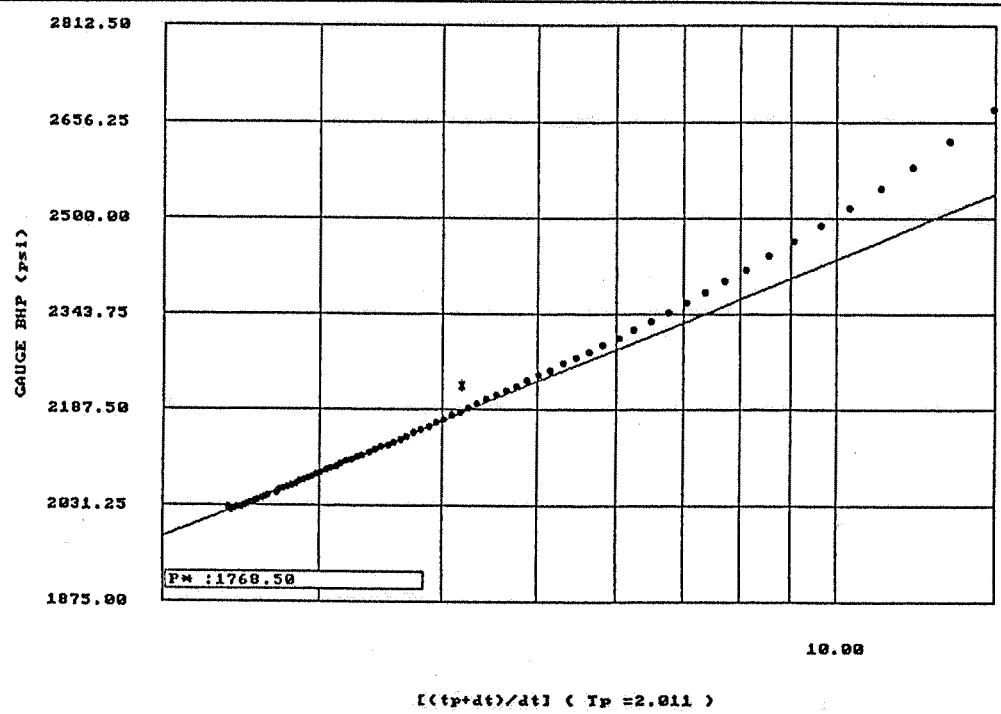
Pre-fracture testing consisted of (1) a 10 bbl slick water pump-in/shut-in (PI/SI) test at 5 bpm, (2) a slick water step-rate test (SRT)/SI at rates of 0.5-8 bpm, and (3) a 1500 gal, 30 ppt borate XL gel (Boragel H3595) minifrac at 15 bpm. The first two tests were designed to evaluate closure pressure and the minifrac was used to determine fluid efficiency and fracture geometry.

Fig. 7 shows the gauge BHP for the first PI/SI test. After an initial breakdown of 4625 psi, pressure dropped to about 3950 psi and then further declined to 3688 psi just prior to shut-down. At shut-down it was difficult to pick an ISIP as shown in Fig. 8. From the Horner plot of the pressure decline, Fig. 9, the pressure extrapolated to 1769 psi or very close to the expected reservoir pressure (no depletion). The square-root of SI time plot, Fig. 10, indicated a closure pressure at 3238 psi.





**FIG. 8 - Slick water PI/SI test BHP ISIP evaluation,
E. Mereenie 37.**



**FIG. 9 - Slick water PI/SI test BHP horner plot,
E. Mereenie 37.**

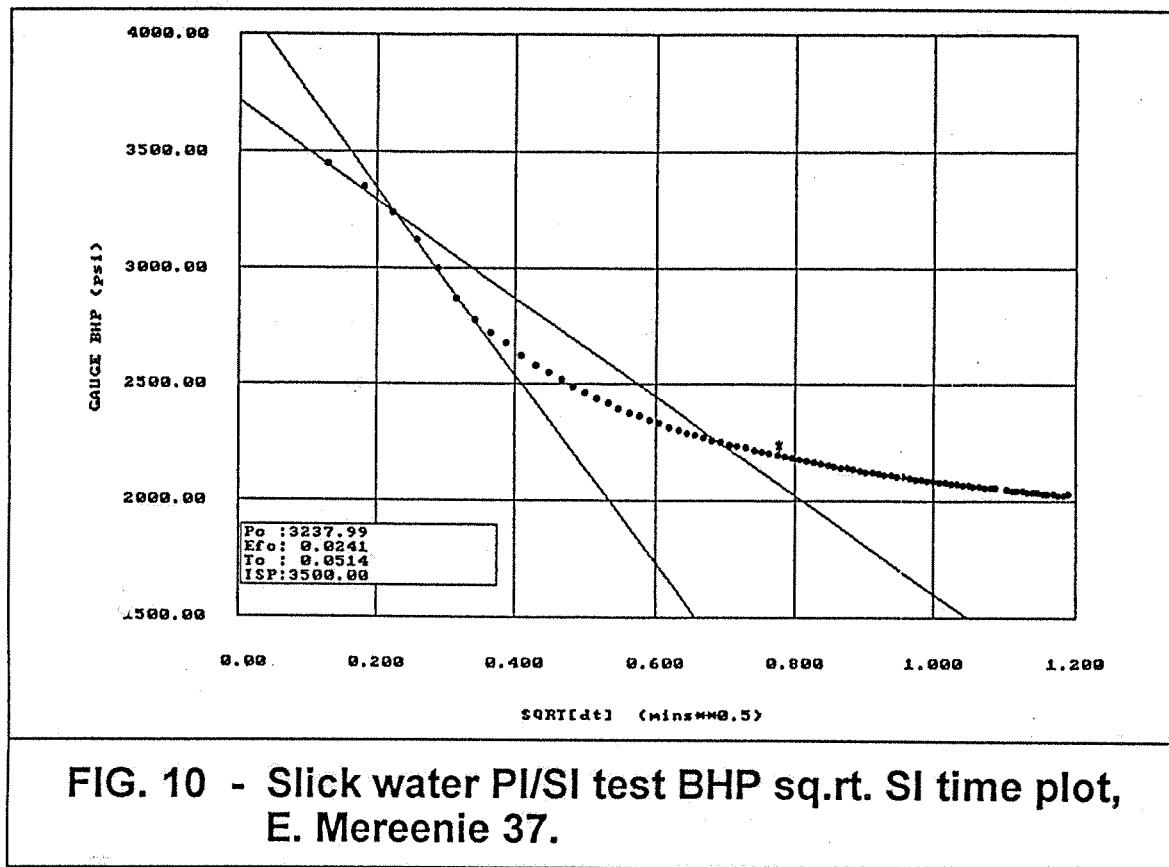
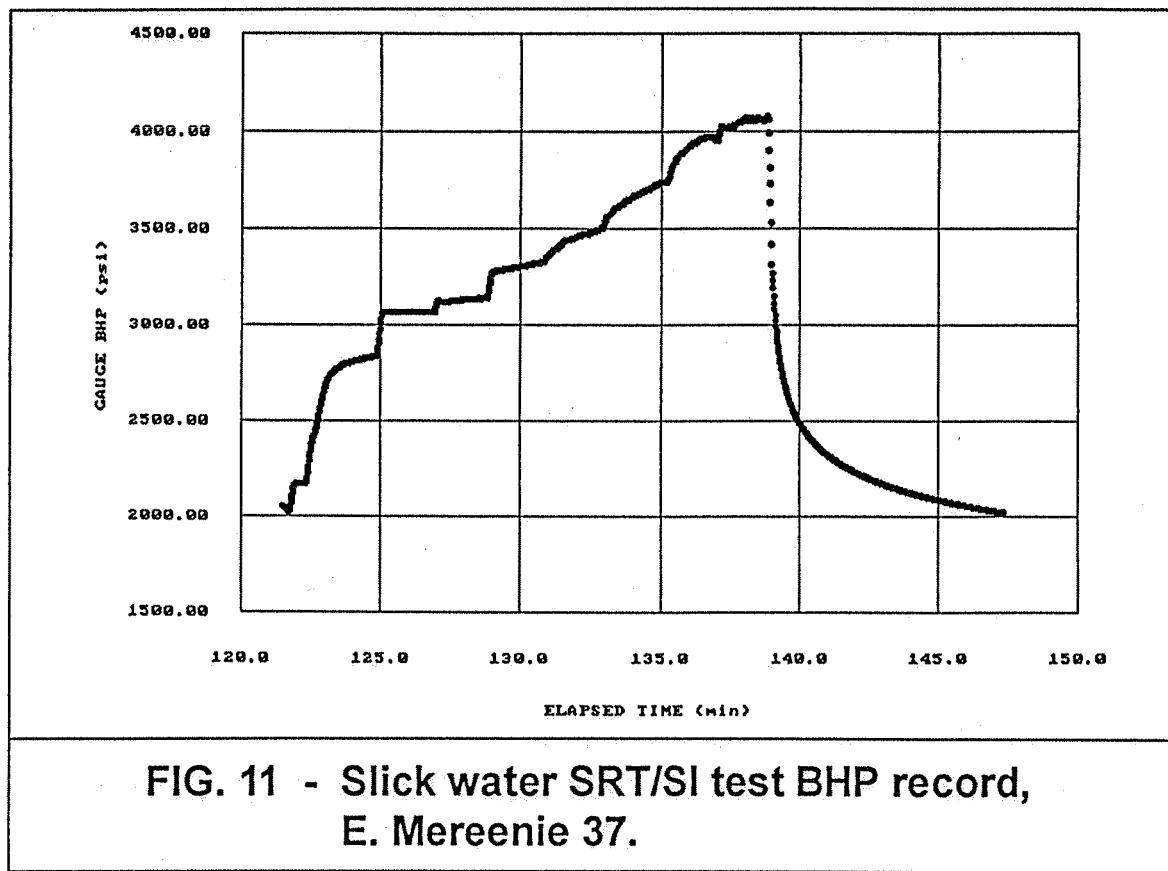
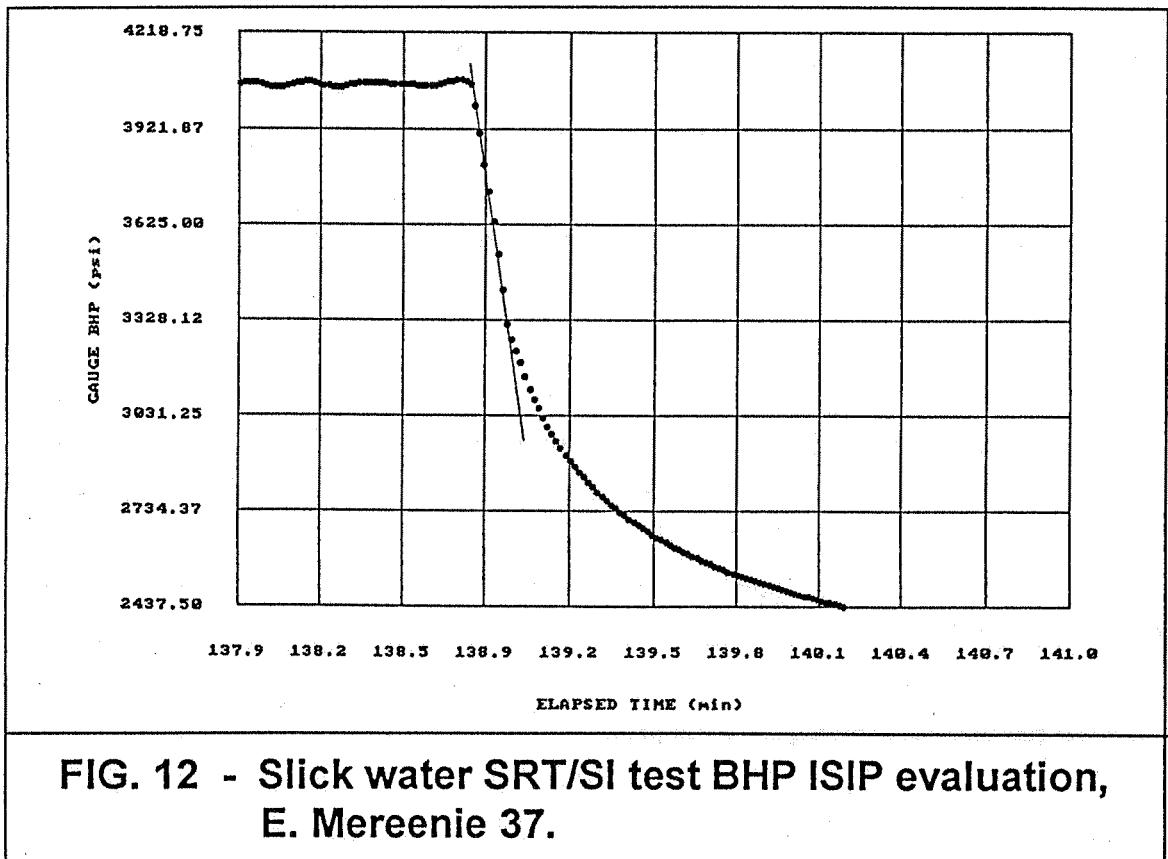


Fig. 11 shows the gauge BHP record for the SRT/SI. BHP never flattened out as expected, making it difficult to determine fracture extension pressure. Based on the ISIP, Fig. 12, fracture extension pressure was somewhere around 3330 psi, which was consistent with the closure pressure pick from the preceding test. From the square-root of SI time plot, Fig. 13, closure was picked at 3261 psi or again reasonably close to the results of the prior test.

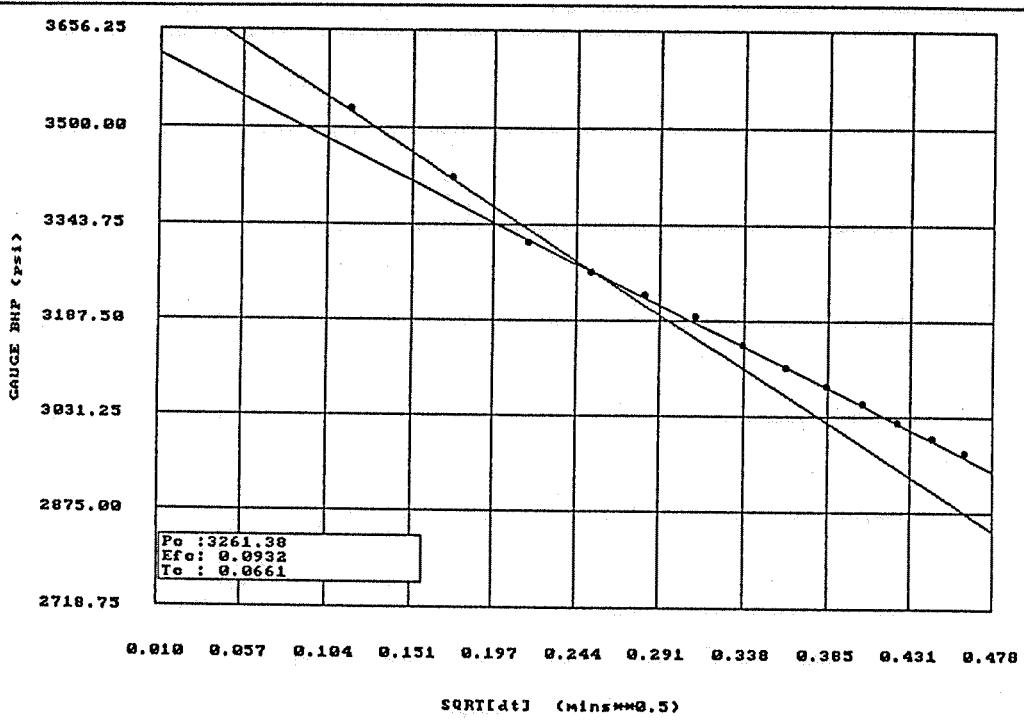
Fig. 14 shows the gauge BHP record for the minifrac. To minimize the effect of the residual wellbore fluid ahead of the crosslinked gel on determining fluid efficiency, the leading edge of the gel was pumped to near bottom at 5 bpm to bullhead the slick water into the fracture. This was followed by a 4 minute shut-in to allow this fluid to leak-off to the formation and the fracture to close prior to injecting the XL gel. At the end of the minifrac, displaced with slick water to the top perforation, the BHTP was 4782 psi. At shut-down, the ISIP appeared to be at 4213 psi, Fig. 15, indicating a downhole "excess" pressure of 569 psi or fairly large.



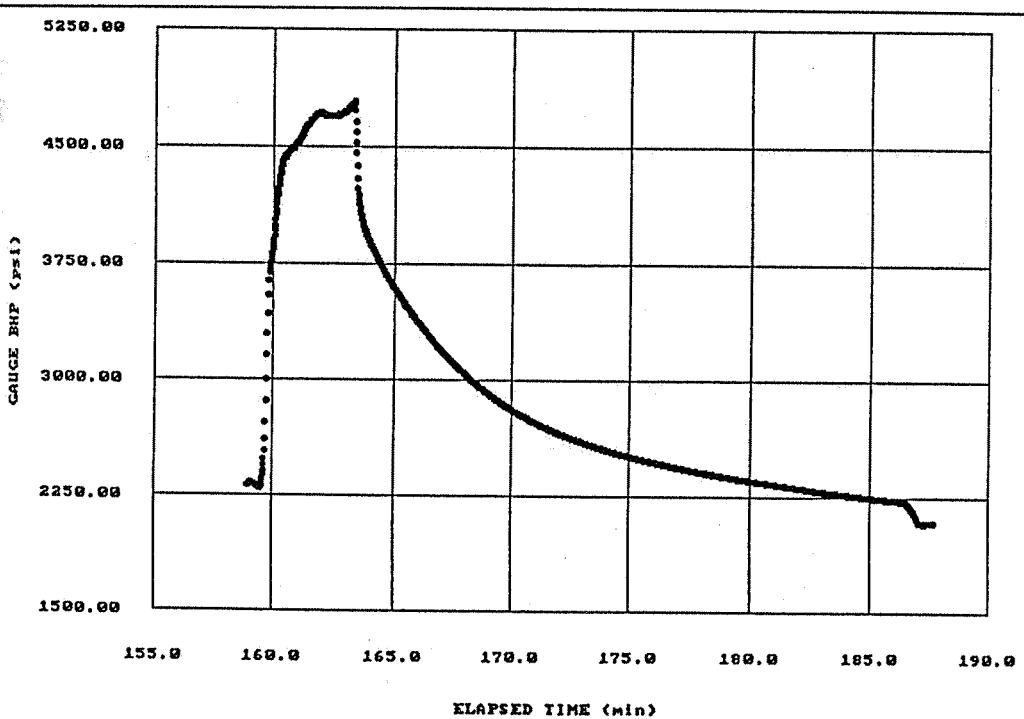
**FIG. 11 - Slick water SRT/SI test BHP record,
E. Mereenie 37.**



**FIG. 12 - Slick water SRT/SI test BHP ISIP evaluation,
E. Mereenie 37.**



**FIG. 13 - Slick water SRT/SI test BHP sq.rt. SI time plot,
E. Mereenie 37.**



**FIG. 14 - Boragel minifrac/SI test BHP record,
E. Mereenie 37.**

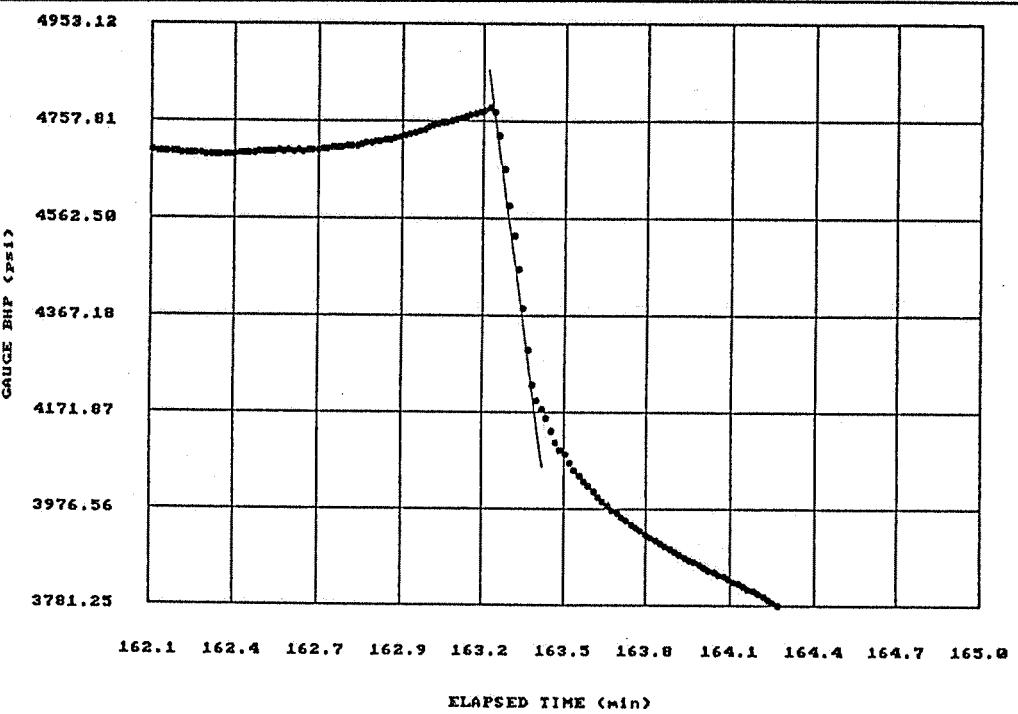
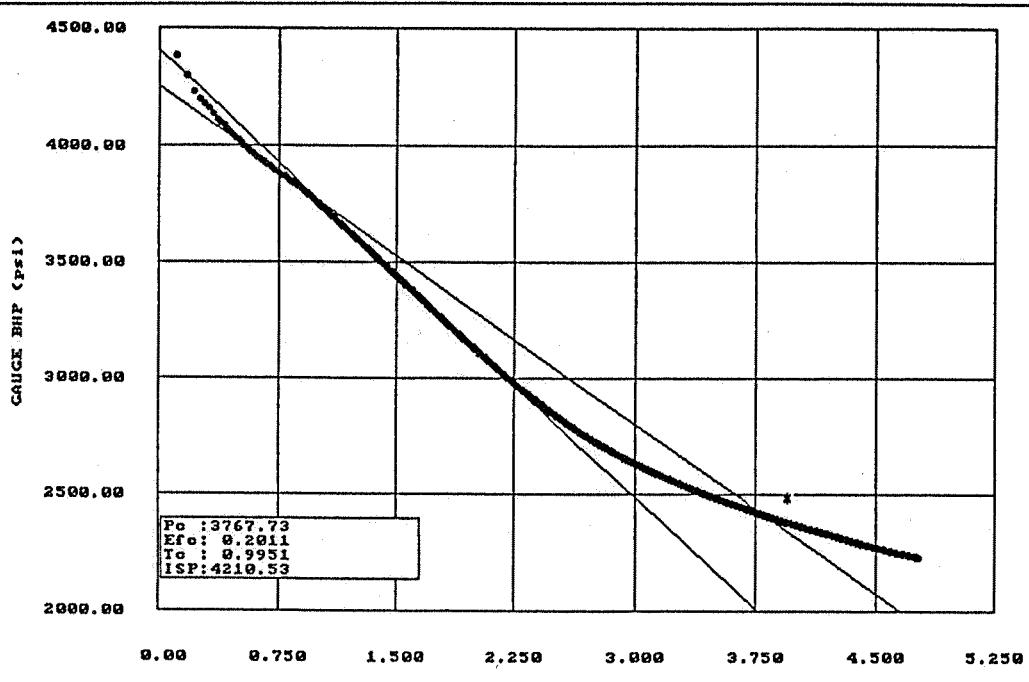


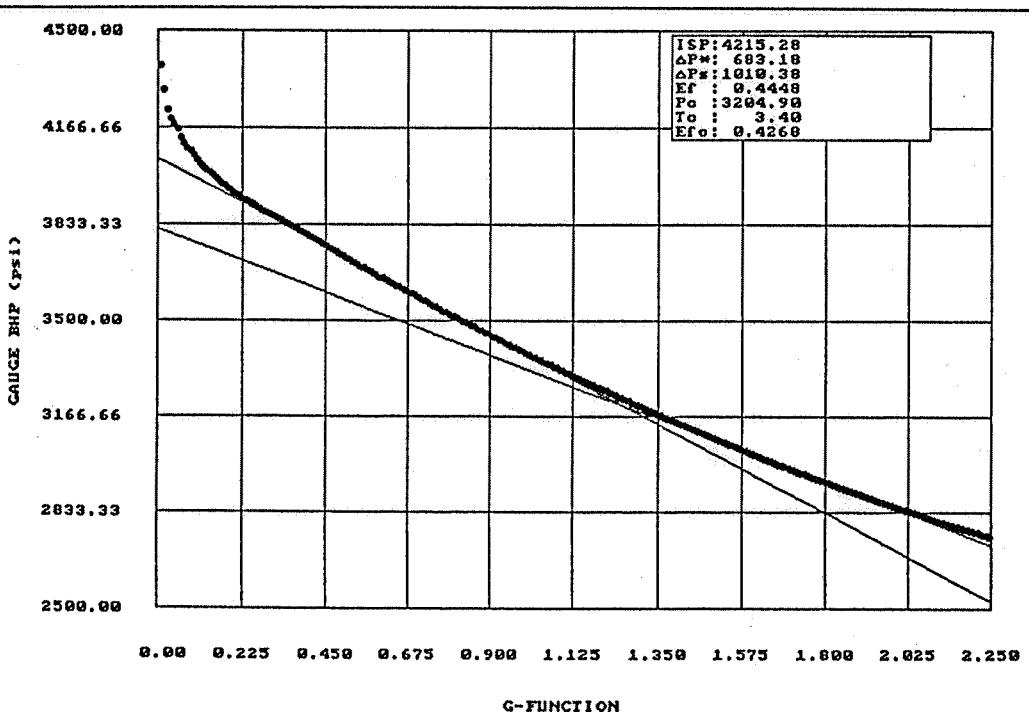
FIG. 15 - Boragel minifrac/SI test BHP ISIP evaluation, E. Mereenie 37.

From the minifrac pressure decline analysis, closure picked at 3768 psi on the square-root of SI time plot, Fig. 16, which corresponded to a fluid efficiency of 0.20 and a net BHTP (BHTP-closure P) of 445 psi. This closure, however, was above the ISIP on the SRT (expected fracture extension pressure) and thought to be more indicative of a shalier layer and not the primary pay zone. There was no indication of the lower closure pick from the previous tests at around 3200 psi. From the G-function plot, Fig. 17, however, closure could be picked at 3205 psi with a corresponding fluid efficiency of 0.43 and a net BHTP of about 1000 psi. From the Nolte type-curve match, Fig. 18, the indicated fluid efficiency was also 0.44.

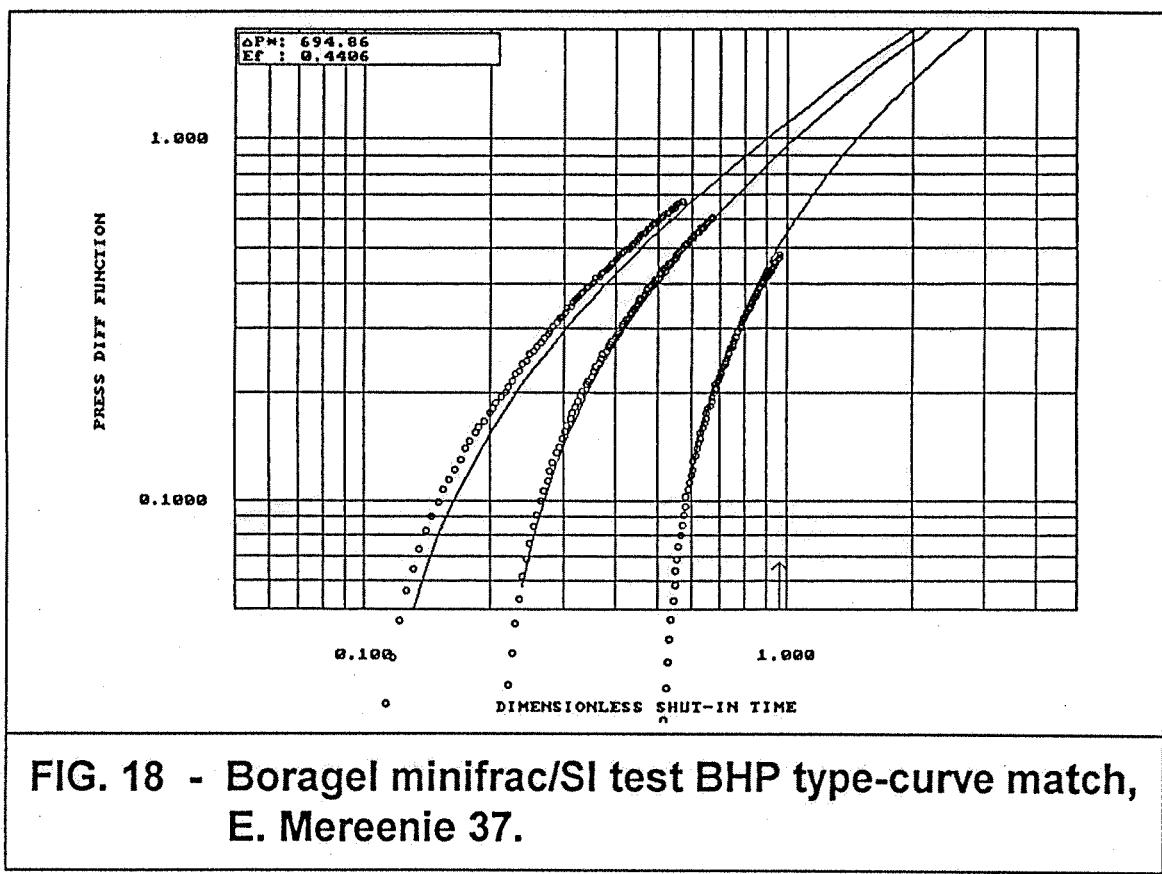
Based on the combined analysis of the three tests, closure pressure was thought to be at 3280 psi (depth corrected from gauge to mid-perf), fluid efficiency from pressure decline analysis was 0.43, and net BHTP for the XL gel at 15 bpm was on the order of 1000 psi. From the established Mereenie correlation of efficiency during injection to that determined from the decline, the injection efficiency was 0.20.



**FIG. 16 - Boragel minifrac/SI test BHP sq.rt. SI time plot,
E. Mereenie 37.**



**FIG. 17 - Boragel minifrac/SI test BHP g-function plot,
E. Mereenie 37.**



To further the minifrac analysis and generate a "calibrated" model for final design evaluation, the minifrac injection profile was history matched. Shown in Fig. 19, the match required to simulate the increasing, relatively high net BHTP and resultant fluid efficiency at the end of injection of 0.20 required (1) a closure stress of 4000 psi in the shalier region between the P3-230/250 and P3-190, and boundary stresses of 4500 psi, (2) an increase in the preliminary design pay zone modulus from 5.5 to 6.5×10^6 psi and from 6.5 to $7.5-8 \times 10^6$ psi in the boundaries, and (3) a decrease in the preliminary design leak-off coefficient from 0.012 to 0.005 ft/sq.rt. minute. The model-predicted fracture dimensions were a created half-length of 79 ft and a maximum height at the wellbore of 82 ft (better confinement than expected). This is shown in Fig. 20 with the model I/O included in Appendix Table A-4.

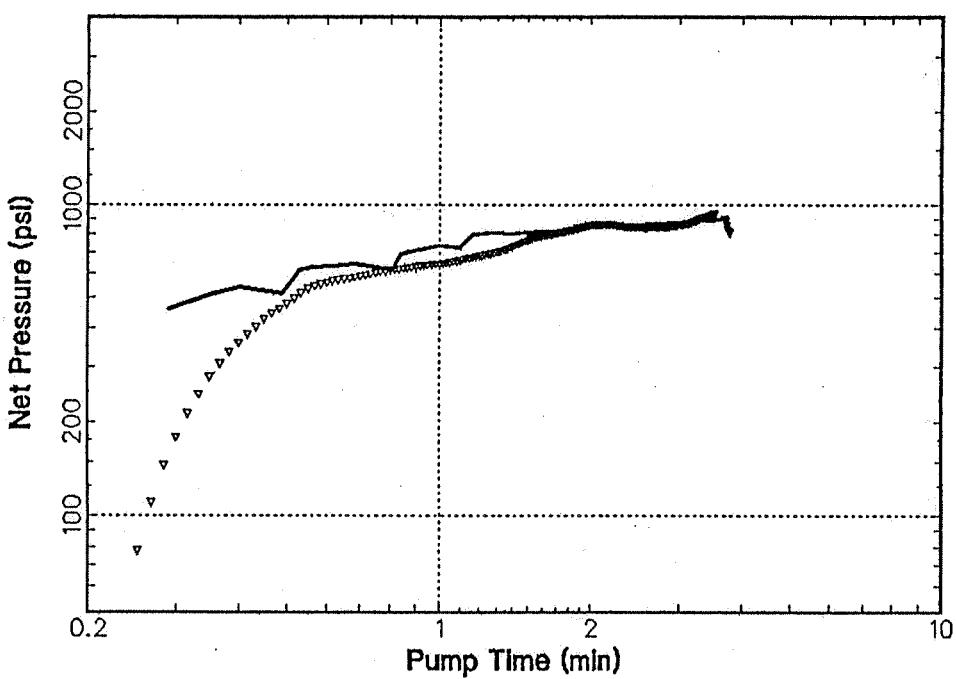


FIG. 19 - Boragel minifrac net BHTP model history match, E. Mereenie 37.

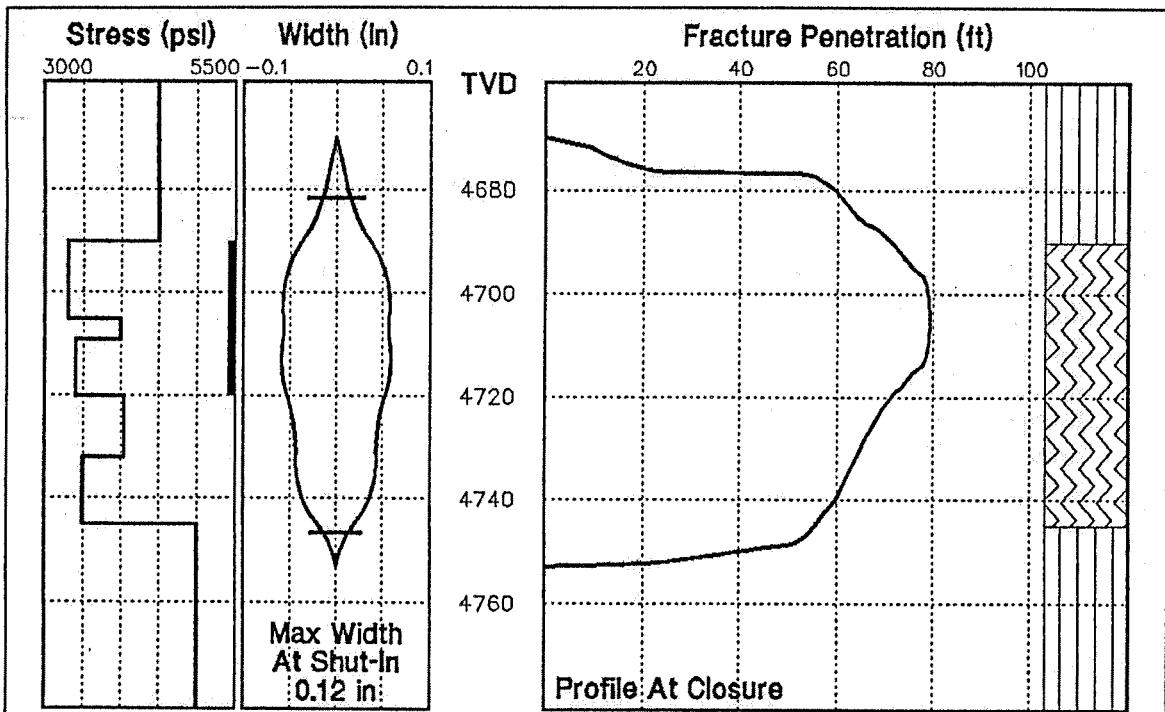


FIG. 20 - Boragel minifrac net BHTP model history match predicted frac geometry, E. Mereenie 37.

Final Treatment Design:

Using the "calibrated" design model, the final design pad stage was limited to 2000 gals to prevent upward growth into the P3-120/130 sands (Table 2). With this pad and the design injection rate of 15 bpm, the model-predicted TSO started at the beginning of the 3 ppg stage. The slurry stages consisted of 3900 gals of gel carrying 14,800 lbs of 20/40 Carbo-Lite at 0.5-8 ppg. With this pad and the design injection rate of 15 bpm, the model-predicted TSO started at the beginning of the 3 ppg stage (Fig. 21) and net BHTP increased from 1080 to 2700 psi with a corresponding average fracture width increase from 0.06 to 0.18 inches. At the wellbore, the final predicted average and maximum widths were 0.25 and 0.45 inches. Other modeled dimensions were a propped half-length of 116 ft, a maximum height at the wellbore of 123 ft (frac top at 4642 ft or at base of 120/130), an average conductivity of 1874 md-ft, and an average in-situ concentration of 1.0 lbs/sq.ft. These are shown in Figs. 22-24 with the model I/O included in Appendix Table A-5.

**TABLE 2 - Final treatment design schedule,
E. Mereenie 37.**

| <u>Fluid Type</u> | <u>Slur. Vol.</u> (gal) | <u>Fluid Vol.</u> (gal) | <u>Prop Conc.</u> (ppg) | <u>Prop Amt.</u> (lbs) | <u>Avg. Q</u> (bpm) | <u>Pump t</u> (min) |
|-------------------|----------------------------|----------------------------|----------------------------|---------------------------|------------------------|------------------------|
| Boragel H3595 | 2000 | 2000 | 0.00 | 0 | 15.00 | 3.17 |
| Boragel H3595 | 613 | 600 | 0.50 | 300 | 15.00 | 0.81 |
| Boragel H3595 | 522 | 500 | 1.00 | 500 | 15.00 | 0.66 |
| Boragel H3595 | 435 | 400 | 2.00 | 800 | 15.00 | 0.69 |
| Boragel H3595 | 453 | 400 | 3.00 | 1200 | 15.00 | 0.54 |
| Boragel H3595 | 470 | 400 | 4.00 | 1600 | 15.00 | 0.56 |
| Boragel H3595 | 488 | 400 | 5.00 | 2000 | 15.00 | 0.77 |
| Boragel H3595 | 506 | 400 | 6.00 | 2400 | 15.00 | 0.80 |
| Boragel H3595 | 523 | 400 | 7.00 | 2800 | 15.00 | 0.83 |
| Boragel H3595 | 541 | 400 | 8.00 | 3200 | 15.00 | 0.86 |
| | 6551 | 5900 | | 14800 | | 10.39 |

Note: (1) Proppant 20/40 Carbo-Lite.

(2) SP (raw) breaker ramped from 0.5-5 ppt in 1-8 ppg stages. Opti-flo II
(encapsulated) breaker ramped from 5-2 ppt throughout treatment.

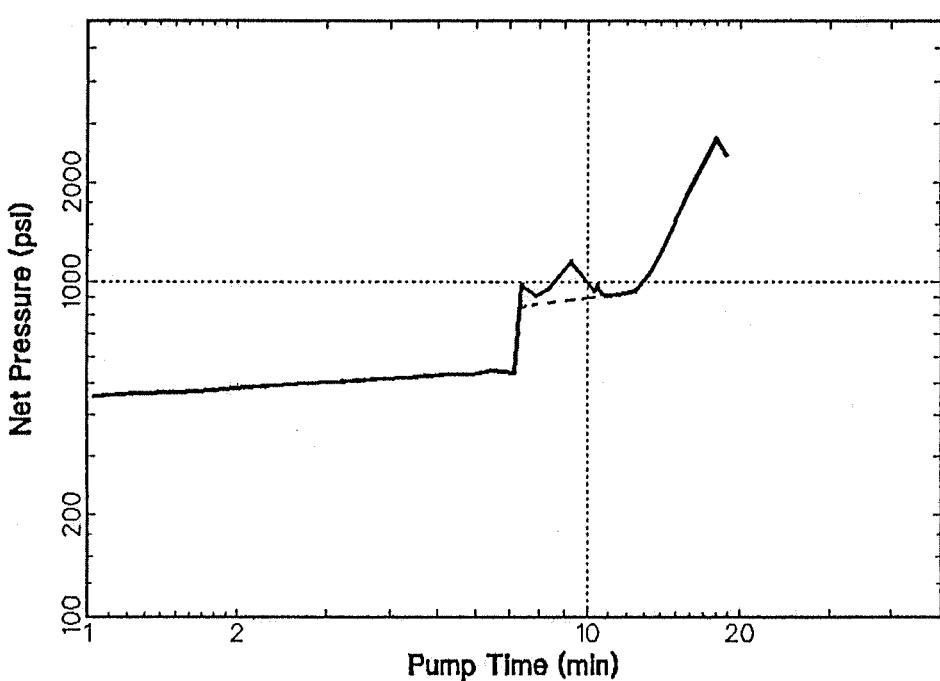


FIG. 21 - Final treatment design predicted net BHTP, E. Mereenie 37.

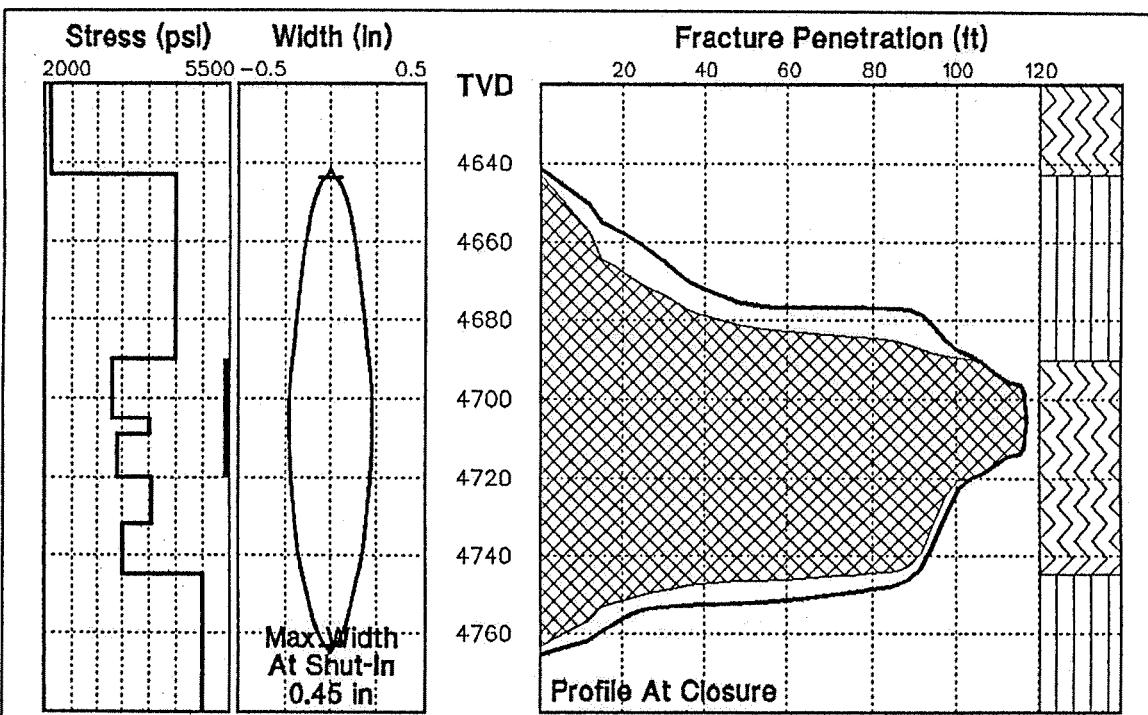
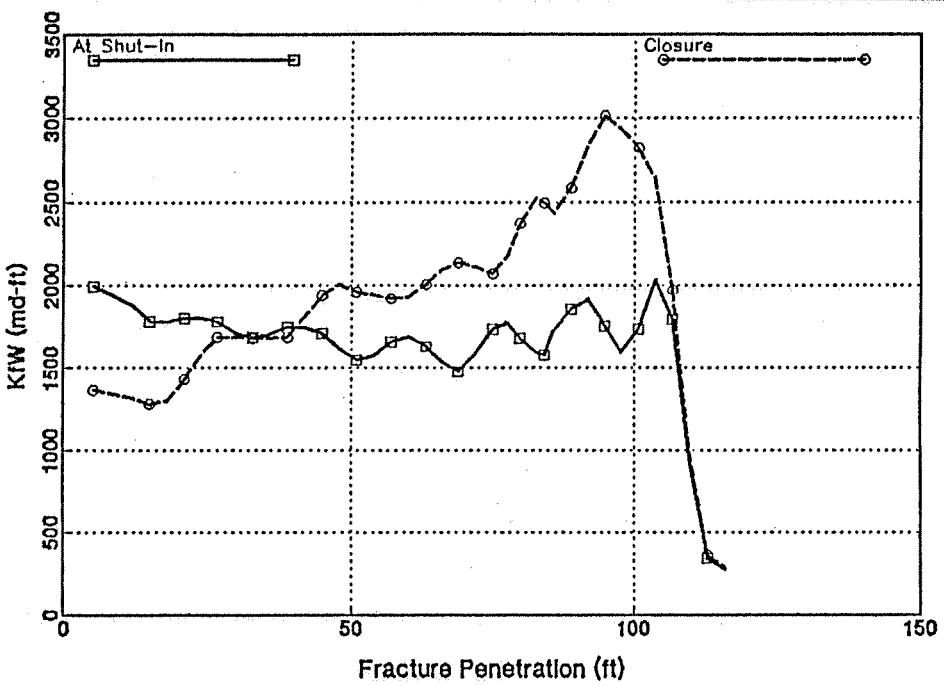
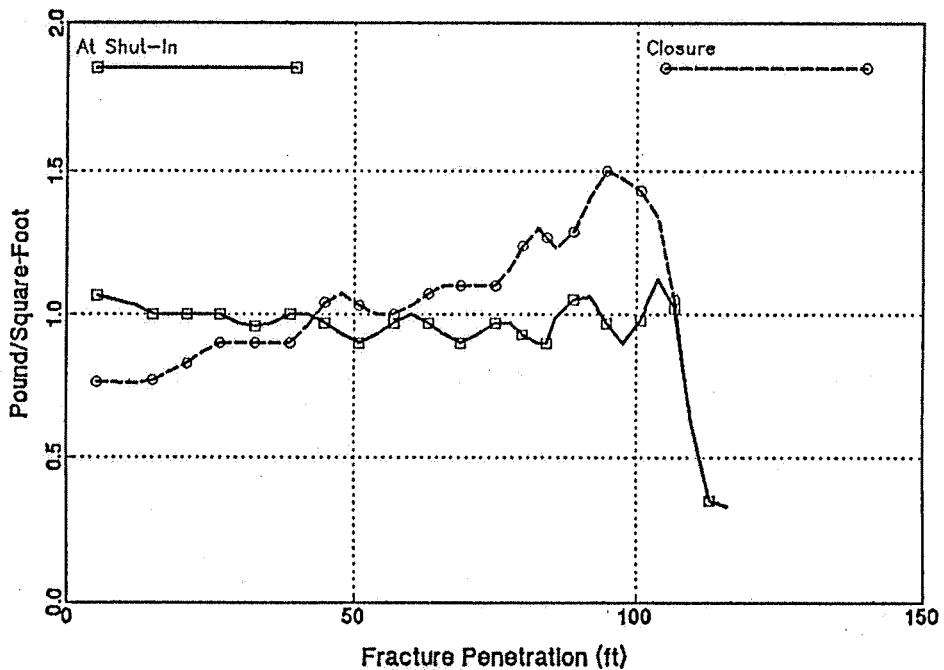


FIG. 22 - Final treatment design predicted frac geometry, E. Mereenie 37.



**FIG. 23 - Final treatment design predicted conductivity,
E. Mereenie 37.**



**FIG. 24 - Final treatment design predicted in-situ conc.,
E. Mereenie 37.**

Treatment Execution:

Samples of the gel were tested on-site prior to the treatment and found to possess the proper characteristics with respect to base gel viscosity, pH, and crosslink time/consistency. While this was not the smallest treatment performed to date in Mereenie, its relatively small size and short pump time required precise execution. To minimize the effect of the bullheaded residual wellbore fluid ahead of the pad, the pad was pumped to the bottom of the tubing at 5 bpm. The rate was then increased to 15 bpm for the remainder of the treatment.

The treatment was pumped without any mechanical or blending mishaps. Fig. 25 shows the surface treating parameters. From this it was difficult to detect whether or not a TSO had occurred. Table 3 shows the surface schedule from Halliburton's computer printout. This indicated a total of 14,586 lbs of proppant pumped with 7436 gals of gel and flush. Based on the amount of proppant loaded/pumped (18,000 lbs) and accounting for 500 lbs spillage, though, this was 20% low. With this correction made in Table 4, the 17,500 lbs of proppant was pumped with 7308 gals of gel and flush. This

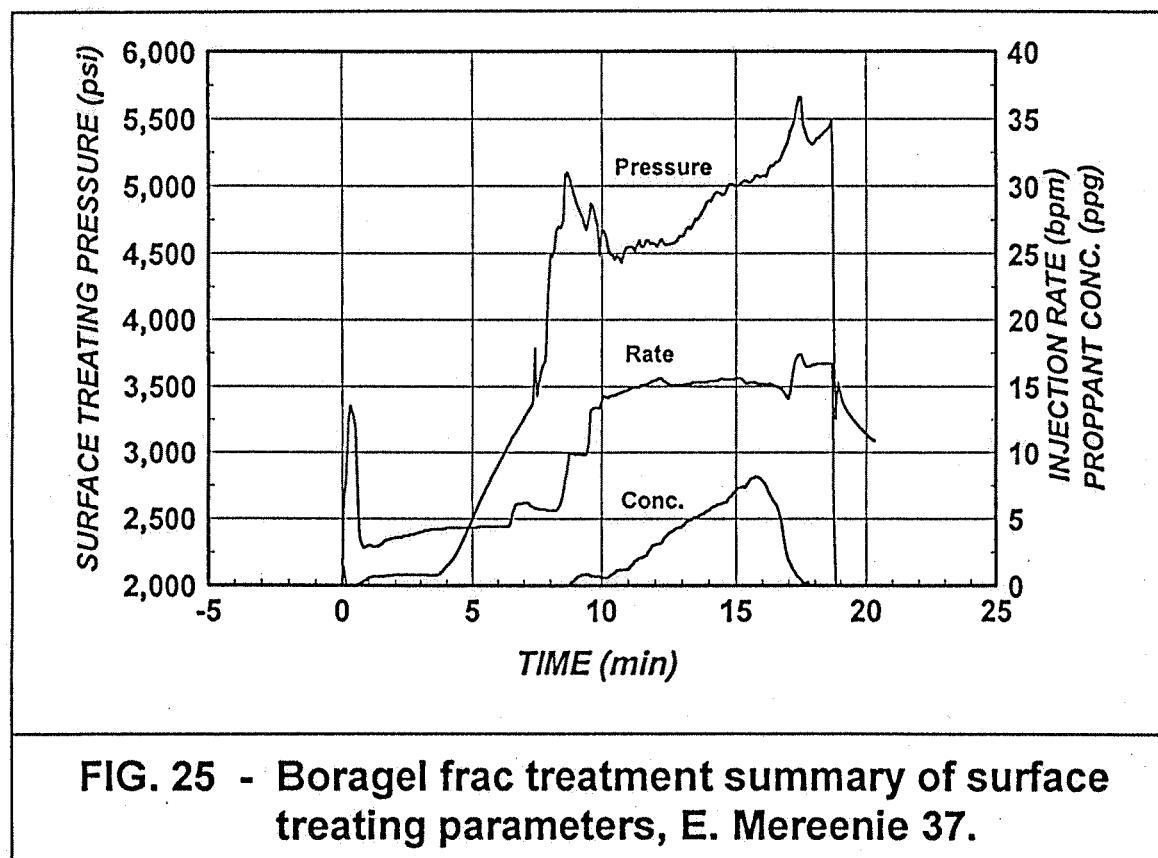


TABLE 3 - Halliburton computed surface pump schedule, E. Mereenie 37.

| <u>Fluid Type</u> | <u>Slur. Vol.</u> (gal) | <u>Fluid Vol.</u> (gal) | <u>Prop Conc.</u> (ppg) | <u>Prop Amt.</u> (lbs) | <u>Avg. Q</u> (bpm) | <u>Pump t</u> (min) |
|-------------------|----------------------------|----------------------------|----------------------------|---------------------------|------------------------|------------------------|
| Boragel H3595 | 1664 | 1664 | 0.00 | 0 | 4.80 | 8.25 |
| Boragel H3595 | 192 | 192 | 0.00 | 0 | 8.31 | 0.55 |
| Boragel H3595 | 284 | 278 | 0.53 | 146 | 9.90 | 0.68 |
| Boragel H3595 | 568 | 554 | 0.57 | 315 | 13.75 | 0.98 |
| Boragel H3595 | 481 | 460 | 1.06 | 486 | 14.62 | 0.78 |
| Boragel H3595 | 489 | 450 | 1.98 | 892 | 15.19 | 0.77 |
| Boragel H3595 | 471 | 416 | 3.01 | 1253 | 15.29 | 0.73 |
| Boragel H3595 | 692 | 588 | 4.04 | 2372 | 15.21 | 1.08 |
| Boragel H3595 | 627 | 514 | 5.01 | 2573 | 15.44 | 0.97 |
| Boragel H3595 | 455 | 359 | 6.07 | 2181 | 15.48 | 0.70 |
| Boragel H3595 | 352 | 272 | 6.70 | 1821 | 15.24 | 0.55 |
| Boragel H3595 | 180 | 142 | 6.00 | 855 | 15.13 | 0.28 |
| Boragel H3595 | 53 | 43 | 5.36 | 230 | 15.15 | 0.08 |
| Flush | 126 | 103 | 5.02 | 518 | 15.00 | 0.20 |
| Flush | 94 | 79 | 4.17 | 331 | 14.92 | 0.15 |
| Flush | 71 | 63 | 2.90 | 183 | 14.49 | 0.12 |
| Flush | 60 | 55 | 1.86 | 103 | 14.29 | 0.10 |
| Flush | 269 | 258 | 0.98 | 252 | 16.01 | 0.40 |
| Flush | 273 | 270 | 0.28 | 75 | 16.96 | 0.38 |
| Flush | <u>676</u> | <u>676</u> | 0.00 | <u>0</u> | 16.10 | <u>1.00</u> |
| | 8077 | 7436 | | 14586 | | 18.75 |

Note: (1) Proppant 20/40 Carbo-Lite.

(2) Loaded 18,000 lbs and allowing for 500 lbs spillage, this is 20% more than computer indicated (densiometer error).

schedule was used to determine the downhole treatment schedule shown in Table 5. From this, a total of 15,746 lbs of proppant (106% of design) was placed in the fracture with 5815 gals of gel (99% design). When compared to the design proppant schedule, the actual schedule came very close as shown in Fig. 26.

**TABLE 4 - "Corrected" surface pump schedule,
E. Mereenie 37.**

| <u>Fluid Type</u> | <u>Slur. Vol.</u> (gal) | <u>Fluid Vol.</u> (gal) | <u>Prop Conc.</u> (ppg) | <u>Prop Amt.</u> (lbs) | <u>Avg. Q</u> (bpm) | <u>Pump t</u> (min) |
|-------------------|----------------------------|----------------------------|----------------------------|---------------------------|------------------------|------------------------|
| Boragel H3595 | 1664 | 1664 | 0.00 | 0 | 4.80 | 8.25 |
| Boragel H3595 | 192 | 192 | 0.00 | 0 | 8.31 | 0.55 |
| Boragel H3595 | 284 | 276 | 0.63 | 175 | 9.90 | 0.68 |
| Boragel H3595 | 568 | 551 | 0.69 | 378 | 13.75 | 0.98 |
| Boragel H3595 | 481 | 455 | 1.28 | 583 | 14.62 | 0.78 |
| Boragel H3595 | 489 | 442 | 2.42 | 1070 | 15.19 | 0.77 |
| Boragel H3595 | 471 | 405 | 3.71 | 1503 | 15.29 | 0.73 |
| Boragel H3595 | 692 | 567 | 5.02 | 2846 | 15.21 | 1.08 |
| Boragel H3595 | 627 | 491 | 6.29 | 3087 | 15.44 | 0.97 |
| Boragel H3595 | 455 | 340 | 7.70 | 2617 | 15.48 | 0.70 |
| Boragel H3595 | 352 | 256 | 8.54 | 2185 | 15.24 | 0.55 |
| Boragel H3595 | 180 | 135 | 7.61 | 1026 | 15.13 | 0.28 |
| Boragel H3595 | 53 | 41 | 6.75 | 276 | 15.15 | 0.08 |
| Flush | 126 | 99 | 6.29 | 621 | 15.00 | 0.20 |
| Flush | 94 | 77 | 5.19 | 397 | 14.92 | 0.15 |
| Flush | 71 | 61 | 3.59 | 220 | 14.49 | 0.12 |
| Flush | 60 | 55 | 2.27 | 124 | 14.29 | 0.10 |
| Flush | 269 | 256 | 1.18 | 302 | 16.01 | 0.40 |
| Flush | 273 | 269 | 0.33 | 90 | 16.96 | 0.38 |
| Flush | <u>676</u> | <u>676</u> | 0.00 | <u>0</u> | 16.10 | <u>1.00</u> |
| | 8077 | 7308 | | 17500 | | 18.75 |

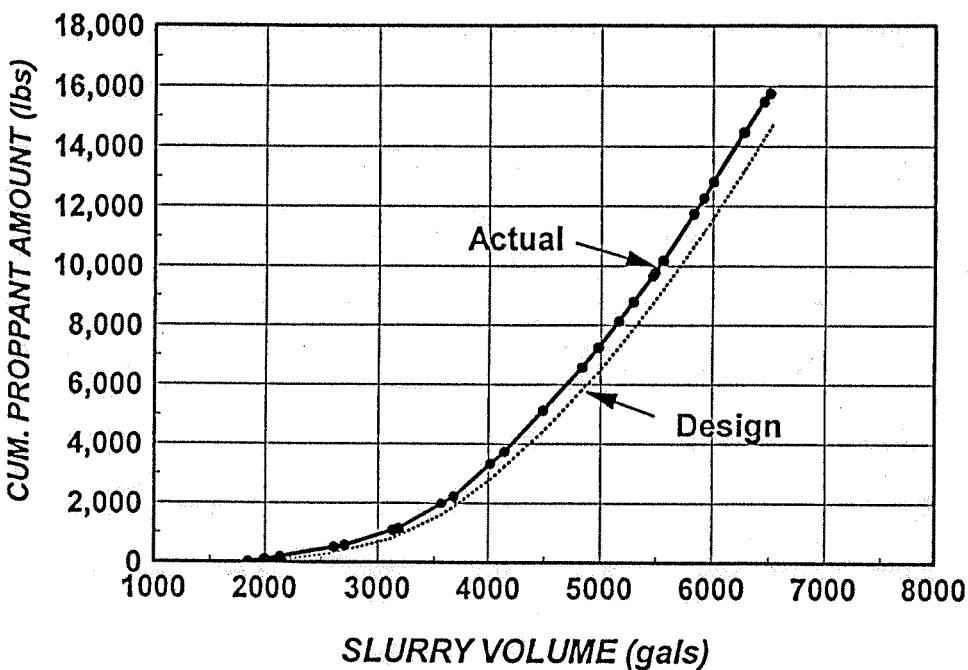
Note: (1) Proppant 20/40 Carbo-Lite.
(2) Flush volume from blender to top perf = 1571 gals.

**TABLE 5 - Treatment downhole pump schedule,
E. Mereenie 37.**

| <u>Fluid Type</u> | <u>Slur. Vol.</u> (gal) | <u>Fluid Vol.</u> (gal) | <u>Prop Conc.</u> (ppg) | <u>Prop Amt.</u> (lbs) | <u>Avg. Q</u> (bpm) | <u>Pump t</u> (min) |
|-------------------|----------------------------|----------------------------|----------------------------|---------------------------|------------------------|------------------------|
| WB/Line Fluid | 1569 | 1569 | 0.00 | 0 | 4.80 | 7.78 |
| Boragel H3595 | 95 | 95 | 0.00 | 0 | 4.80 | 0.47 |
| Boragel H3595 | 192 | 192 | 0.00 | 0 | 8.31 | 0.55 |
| Boragel H3595 | 284 | 284 | 0.00 | 0 | 9.90 | 0.68 |
| Boragel H3595 | 568 | 568 | 0.00 | 0 | 13.75 | 0.98 |
| Boragel H3595 | 481 | 481 | 0.00 | 0 | 14.62 | 0.78 |
| Boragel H3595 | 236 | 236 | 0.00 | 0 | 15.19 | 0.37 |
| Boragel H3595 | 284 | 276 | 0.63 | 175 | 15.20 | 0.44 |
| Boragel H3595 | 568 | 551 | 0.69 | 378 | 15.27 | 0.89 |
| Boragel H3595 | 481 | 455 | 1.28 | 583 | 15.21 | 0.75 |
| Boragel H3595 | 489 | 442 | 2.42 | 1070 | 15.40 | 0.76 |
| Boragel H3595 | 471 | 405 | 3.71 | 1503 | 15.46 | 0.73 |
| Boragel H3595 | 692 | 567 | 5.02 | 2846 | 15.29 | 1.08 |
| Boragel H3595 | 318 | 249 | 6.29 | 1566 | 15.02 | 0.50 |
| Boragel H3595 | 131 | 103 | 6.29 | 645 | 14.40 | 0.22 |
| Boragel H3595 | 178 | 139 | 6.29 | 876 | 16.01 | 0.26 |
| Boragel H3595 | 91 | 68 | 7.70 | 523 | 16.01 | 0.14 |
| Boragel H3595 | 273 | 204 | 7.70 | 1570 | 16.96 | 0.38 |
| Boragel H3595 | 91 | 68 | 7.70 | 524 | 16.10 | 0.13 |
| Boragel H3595 | 352 | 256 | 8.54 | 2185 | 16.10 | 0.52 |
| Boragel H3595 | 180 | 135 | 7.61 | 1026 | 16.10 | 0.27 |
| Boragel H3595 | <u>76</u> | <u>41</u> | <u>6.75</u> | <u>276</u> | <u>16.10</u> | <u>0.08</u> |
| | 8077 | 7384 | | 15746 | | 18.76 |

Note: (1) Proppant 20/40 Carbo-Lite.

(2) Actual prop amt. placed = 106.4% of design. Act. gel vol. placed = 98.6% of design. Avg. conc. (slurry) = 3.98 ppg (design - 3.79 ppg).



**FIG. 26 - Comparison of actual to design prop schedule,
E. Mereenie 37.**

Post-Frac Evaluation:

Fig. 27 shows the gauge BHTP record plotted with the corresponding rate and downhole proppant concentration. From this it was apparent that the TSO started somewhere around 13 minutes, with a pressure gain of 1300 psi as compared to the design prediction of 1600 psi. To history match this pressure behavior, net BHTP was calculated using the closure pressure of 3280 psi and the downhole "excess" pressure of 570 psi from the minifrac for the higher rate, crosslinked gel portion of the treatment.

Fig. 28 shows the best model match obtained for both the low rate wellbore fluid injection and the main treatment. To obtain this match required only minor changes to the final design model, these including (1) relaxing the lower boundary stress from 5000 to 4500 psi and (2) reducing the leak-off coefficient from 0.005 to 0.0044 ft/sq.rt. minute and increasing spurt from 0.2 to 0.45 gals/100 sq.ft. With the actual downhole treatment schedule, this model predicted fracture dimensions of a propped half-length of 118 ft

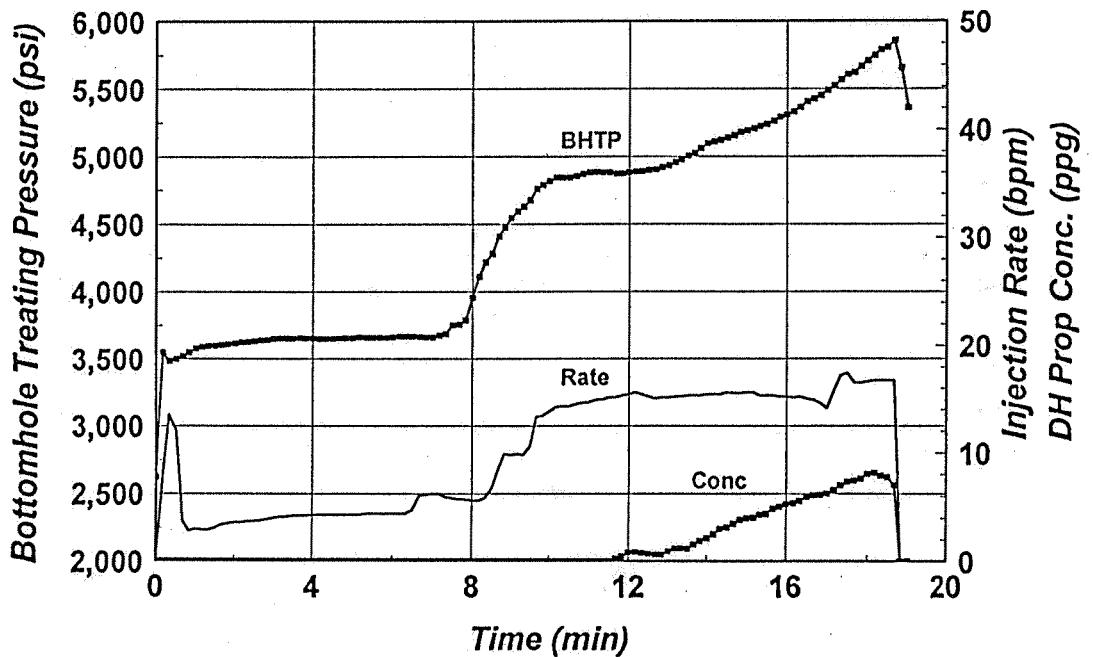


FIG. 27 - Boragel treatment summary of BH treating parameters, E. Mereenie 37.

(design - 116 ft), a maximum height of 141 ft (design - 123 ft), an average conductivity of 1608 md-ft (design - 1874 md-ft), and an average in-situ concentration of 0.9 lbs/sq.ft. (design - 1.0 lbs/sq.ft.). These are shown in Figs. 29-31 with the model I/O included in Appendix Table A-6. The predicted top of the fracture was at 4647 ft-TVD or 4 ft from the bottom of the 120/130. The resultant average and maximum widths at the wellbore at the end of the treatment were 0.23 and 0.44 inches, respectively.

With this first history match being somewhat "rough" in the early part of the high rate portion of the treatment, a second history match was attempted without the initial low rate stage (assuming this had minimal impact on fracture dimensions). To obtain the match shown in Fig. 32 required two changes to the previous model, i.e. a further reduction in leak-off to 0.0034 ft/sq.rt. minute and a reduction in spurt from 0.45 to 0.25 gals/100 sq.ft. This was not that surprising, given that the wellbore fluid would have a much higher leak-off than the crosslinked gel. The resultant dimensions were a propped half-length of 118 ft (same as before), a maximum height of 135 ft (6 ft less than before),

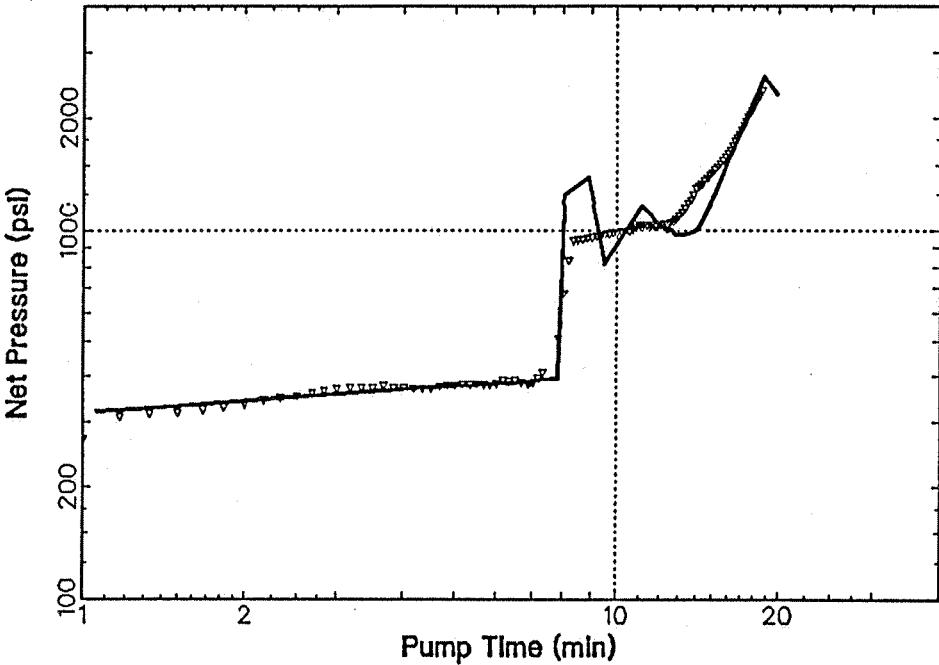


FIG. 28 - Boragel treatment post-frac net BHTP history match #1, E. Mereenie 37.

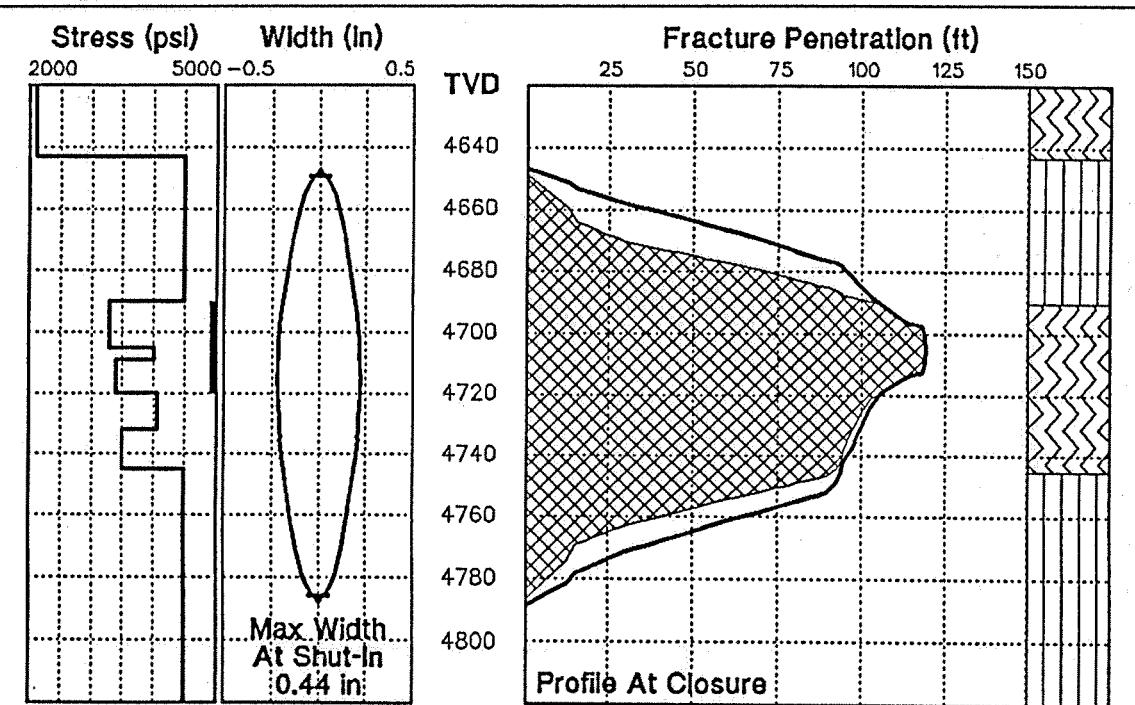


FIG. 29 - Boragel treatment history match #1 predicted frac geometry, E. Mereenie 37.

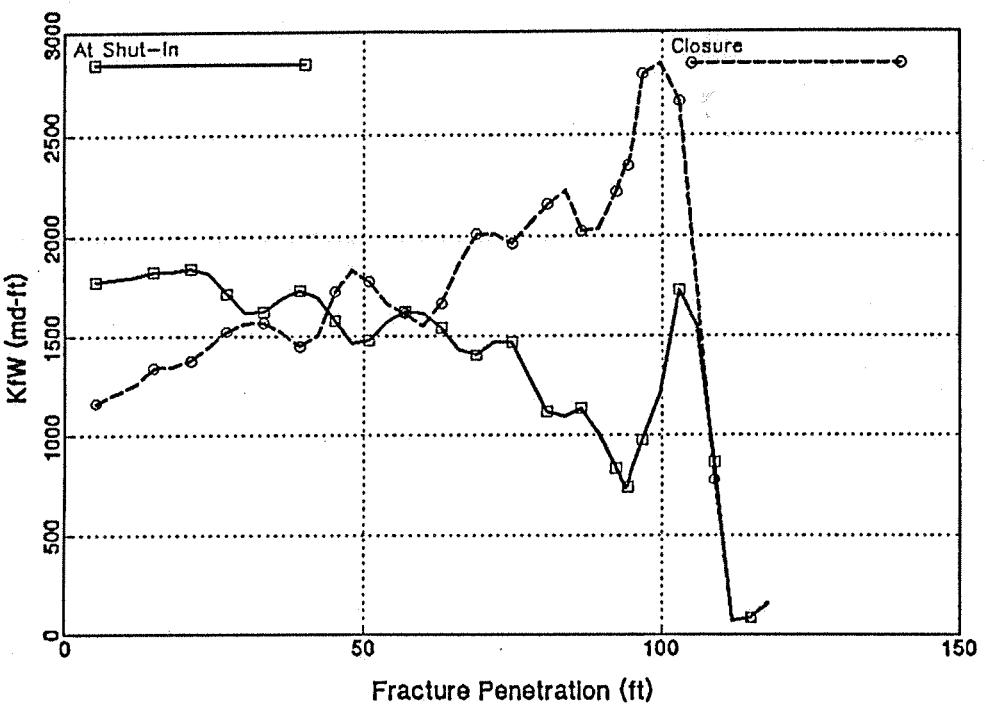


FIG. 30 - Boragel treatment history match #1 predicted conductivity, E. Mereenie 37.

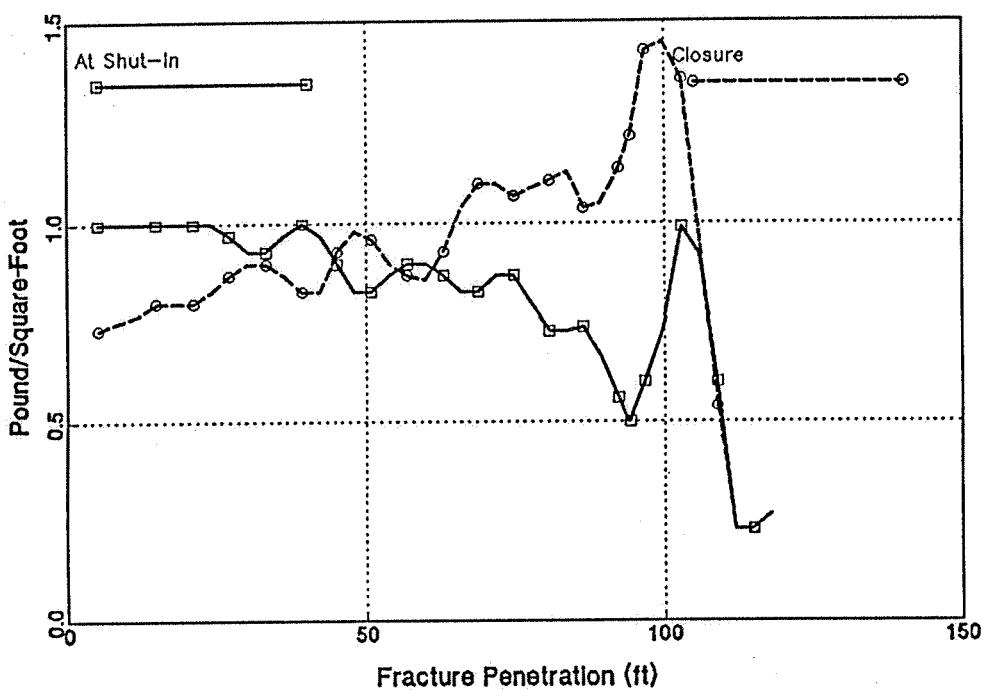
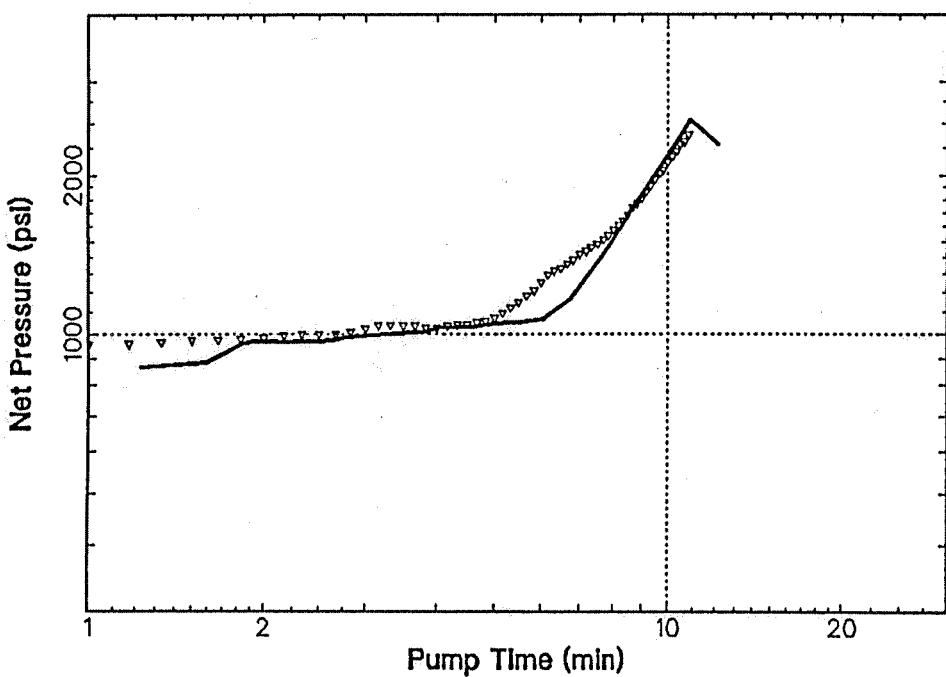


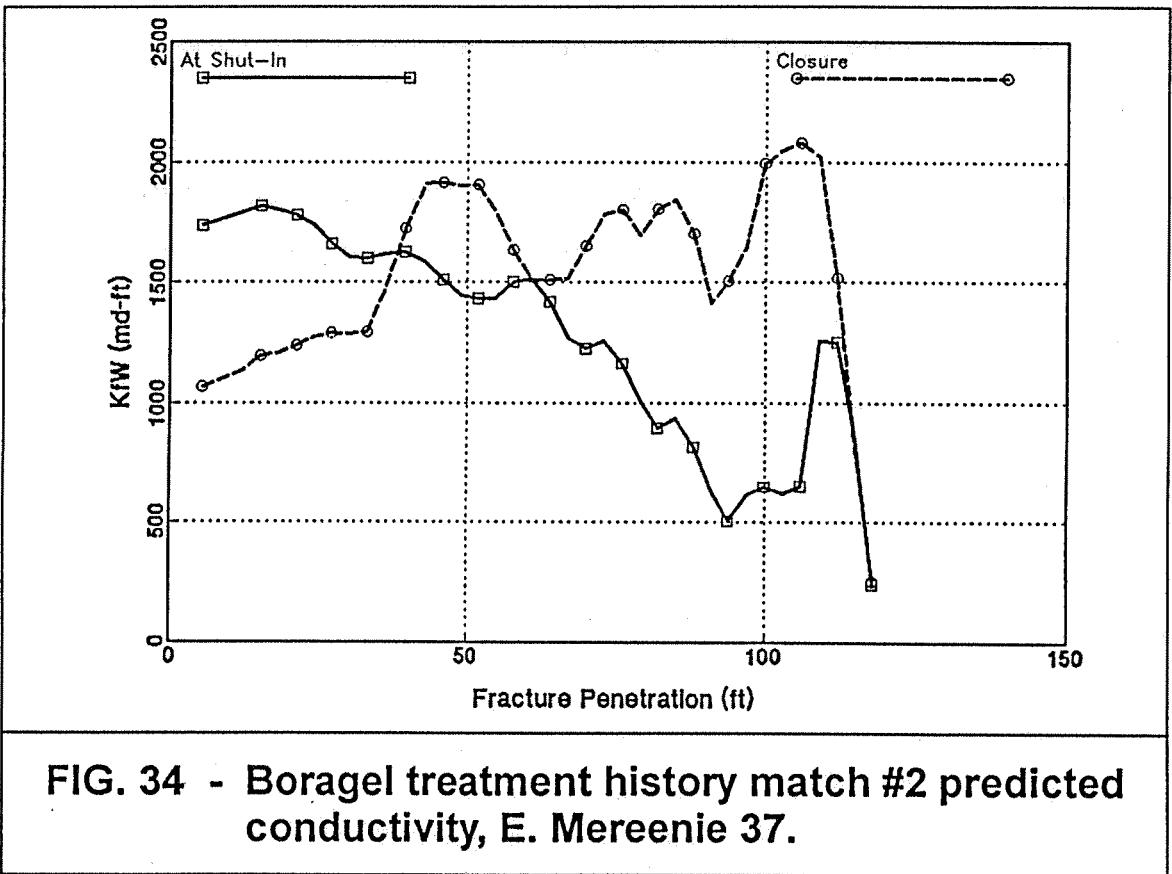
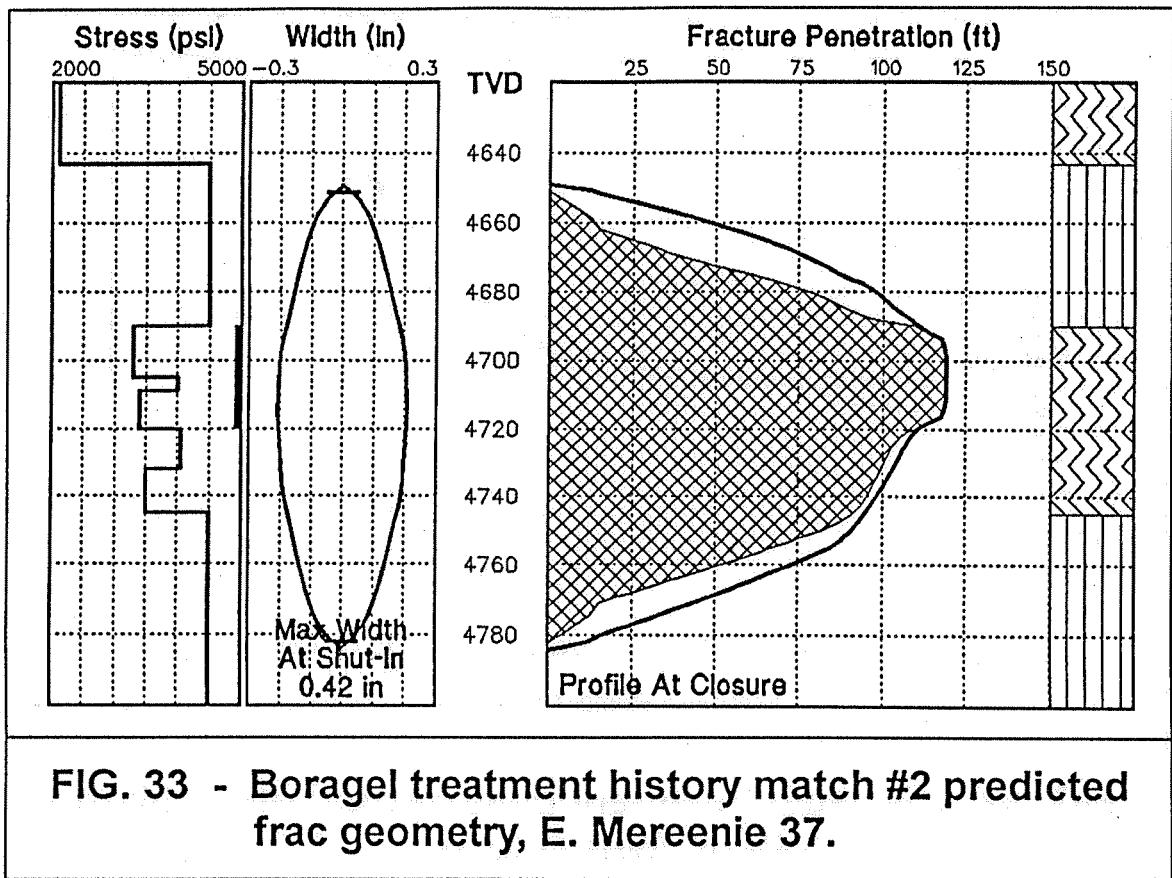
FIG. 31 - Boragel treatment history match #1 predicted in-situ conc., E. Mereenie 37.



**FIG. 32 - Boragel treatment post-frac net BHTP history
match #2, E. Mereenie 37.**

an average conductivity of 1519 md-ft, and an average in-situ concentration of 0.9 lbs/sq.ft. These are shown in Figs. 33-35 with the model I/O in Appendix Table A-7.

In summary, the fracture appears to extend 118 ft from the wellbore with an average conductivity of 1500-1600 md-ft. It does not appear that the fracture grew into the P3-120/130.



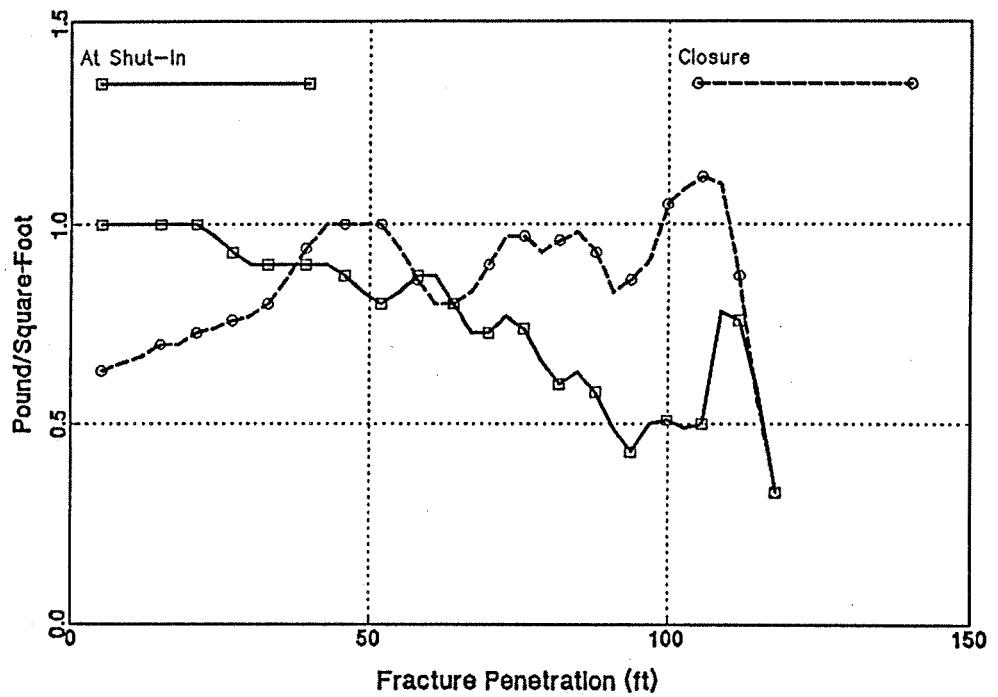


FIG. 35 - Boragel treatment history match #2 predicted in-situ conc., E. Mereenie 37.

CONCLUSIONS / RECOMMENDATIONS

From pre-frac test analysis, closure pressure was 3280 psi (0.695 psi/ft), fluid efficiency from pressure decline analysis was 0.43, and net BHTP was on the order of 1000 psi with the XL gel at 15 bpm. Using the Mereenie correlation of fluid efficiency from pressure decline to injection efficiency, the efficiency was reduced to only 0.20 for final design formulation. A fairly high downhole "excess" pressure of 570 psi was measured on the minifrac. This was thought to be due to the wellbore deviation and poor alignment of the wellbore with the preferred fracture azimuth. This did not cause any problems in pumping the treatment.

The treatment, kept small in size to stay out of the alternative P3-120/130 pay zone, was pumped fairly close to design, placing 106% of the designed proppant amount in the fracture with 99% of the design gel volume. The TSO did occur as planned, with a net BHTP gain of 1300 psi as compared to the design prediction of 1600 psi. When compared to the design model, the post-frac history match required relaxing the lower boundary stress from 5000 to 4500 psi and reducing the leak-off coefficient from 0.005 to 0.0044 ft/sq.rt. minute. Model-predicted dimensions were a propped half-length of 118 ft (design - 116 ft), a maximum height of 141 ft (design - 123 ft), an average conductivity of 1608 md-ft (design - 1874 md-ft), and an average in-situ concentration of 0.9 lbs/sq.ft. (design - 1.0 lbs/sq.ft.). The modeled fracture top was at 4647 ft-TVD or 4 ft below the P3-120/130. Based on this analysis, the treatment came fairly close to design predictions.

APPENDIX A

Fracture Model Simulations

INIT. OVER ENTIRE PERFS.

| | | | |
|--|--|--|--|
| StimPlan 2.50 (TM). NSI Technologies, Tulsa, OK | | | |
| Licensed To: Internal Use - NSI Technologies | | | |
| WELL ID: | | | |
| SANTOS -E.MERENNIE #37 (230/250) PRELIM. FRAC DESIGN | | | |
| DEPTH: Well Depth (ft) ... 4690 | | | |
| PRESSURE: Reservoir Pressure (psi) ... 1770 | | | |
| Closure Pressure (psi) ... 3400 | | | |
| TEMPERATURE: Bottom Hole Temperature (deg_F) ... 143 | | | |

Frac Summary * SANTOS -E.MERENNIE #37 (230/250) PRELIM. FRAC DESIGN
 Filename: EM37PP1.FRK ; Jul 28, 95

| | | | |
|--|--|--|--|
| WELL ID: | | | |
| SANTOS -E.MERENNIE #37 (230/250) PRELIM. FRAC DESIGN | | | |
| DEPTH: Well Depth (ft) ... 4690 | | | |
| PRESSURE: Reservoir Pressure (psi) ... 1770 | | | |
| Closure Pressure (psi) ... 3400 | | | |
| TEMPERATURE: Bottom Hole Temperature (deg_F) ... 143 | | | |

| SL VOL | FL VOL | Conc | Pumping Schedule ** | Rate | Fluid | Prop | Cum Prop | Pump Time | Time (min) |
|--------------------|--------|-------|---------------------|-------|-------|------|----------|-----------|------------|
| (mGal) | (mGal) | (PPG) | (BPM) | (BPM) | Type | Type | Type | (MLbs) | |
| 1.50 | 1.50 | 0.0 | 5.00 | 1 | 1 | 0.0 | 0.0 | 7.1 | |
| 2.25 | 2.25 | 0.0 | 15.00 | 2 | 1 | 0.0 | 0.3 | 3.6 | |
| 0.51 | 0.50 | 0.5 | 15.00 | 2 | 1 | 0.3 | 0.8 | | |
| 0.42 | 0.40 | 1.0 | 15.00 | 2 | 1 | 0.7 | 0.7 | | |
| 0.44 | 0.40 | 2.0 | 15.00 | 2 | 1 | 1.4 | 0.7 | | |
| 0.34 | 0.30 | 3.0 | 15.00 | 2 | 1 | 2.4 | 0.5 | | |
| 0.35 | 0.30 | 4.0 | 15.00 | 2 | 1 | 3.6 | 0.6 | | |
| 0.49 | 0.40 | 5.0 | 15.00 | 2 | 1 | 5.6 | 0.8 | | |
| 0.63 | 0.50 | 6.0 | 15.00 | 2 | 1 | 8.6 | 1.0 | | |
| Total Slurry ... | 6.9 | | Total Fluid ... | 6.6 | | | | | |
| Total Proppant ... | 8.6 | | Avg. Conc ... | 1.3 | | | | | |
| Total Pump Time | 15.8 | min | | | | | | | |

| | |
|--|----------------------------|
| Proppant ID No. 1 | 20- 40 CARBO-LITE |
| Specific Gravity | 2.72 |
| 'Damage Factor' | |
| Proppant Stress (Mpsi) KfW @ 2 #/sq ft (md-ft) | 0 10500 9200 7600 3200 500 |

| | |
|------------------------|-----------------|
| Fluid ID No. 1 | 10#_SLICK_WATER |
| Specific Gravity | 1.04 |
| vis (cp @ 170 1/sec) | 0.2Hr |
| non-Newtonian 'n' | 5 |
| K(lb.sec/ft^2)x1000 | 5 |
| Measured Depth (ft) | 4950.0 |

| | |
|---------|-------------------|
| Q (BPM) | dP/dL (psi/100ft) |
| 5.0 | 30.0 |
| 10.0 | 32.0 |
| 15.0 | 40.0 |
| 20.0 | 60.0 |

| | | | | | | | | | |
|---|--|--|--|--|--|--|--|--|--------------------------------|
| Calculated Results | | | | | | | | | |
| from 3-D Simulator | | | | | | | | | STIMPLAN (TM) , NSI , Tulsa,OK |
| Licensed To: Internal Use - NSI Technologies | | | | | | | | | |
| 1/2 LENGTH: 'Hydraulic' length (ft) | | | | | | | | | |
| PRESSURE: Max Net Pressure (psi) | | | | | | | | | |
| Surface Pres-End of Pad (psi) | | | | | | | | | |
| Surface Pres-Start of Flush (psi) | | | | | | | | | |
| Maximum Hydraulic Horsepower | | | | | | | | | |
| TIME: Max Exposure to Form. Temp. (min) | | | | | | | | | |
| Time to Close (min) | | | | | | | | | |
| RATE: Fluid Loss Rate during pad (BPM) | | | | | | | | | |
| EFFICIENCY: at end of pumping schedule | | | | | | | | | |
| PROPPANT: Average In Situ Conc. (#/sq ft) | | | | | | | | | |
| HEIGHT: Max Fracture Height (ft) | | | | | | | | | |
| WIDTH: Avg width at end of pumping (in) | | | | | | | | | |

TABLE A-1

Fluid ID No. 2

BORGEL_H3595

Specific Gravity

@Wellbore @FormTemp
0.325 275 225 175 10 2
0.41 0.42 0.90 0.95 0.95 0.05
0.41 0.42 0.90 0.95 0.95 0.05
0.34 70.51 0.34 0.05

V_{is} (cp @ 170 1/sec)

non-Newtonian n' ... 0.38 0.40 0.41 0.42 0.90 0.95
K(lb.sec/ft²)x1000 160.82 122.80 95.44 70.51 0.34 0.05

Time History * NSI STIMPLAN 3-D Fracture Simulation

SANTOS -E.MEREEENIE #37 (230/250) PRELIM. FRAC DESIGN

| Time (min) | Pen (ft) | Pres (psi) | Rate (BPM) | Prop (PPG) | SI Vol (MGal) | Efficiency (%) | Loss (ft) | Avg W-Avg (in) |
|--|----------|------------|------------|------------|---------------|----------------|-----------|----------------|
| 0.9 | 7 | 165 | 5.00 | 0.0 | 0.2 | 0.03 | 4.7 | 55 0.01 |
| 1.3 | 7 | 164 | 5.00 | 0.0 | 0.3 | 0.03 | 4.8 | 56 0.01 |
| 1.6 | 8 | 172 | 5.00 | 0.0 | 0.3 | 0.03 | 5.0 | 56 0.01 |
| 2.0 | 10 | 179 | 5.00 | 0.0 | 0.4 | 0.02 | 5.0 | 56 0.01 |
| 2.3 | 11 | 186 | 5.00 | 0.0 | 0.5 | 0.02 | 5.0 | 56 0.01 |
| 2.8 | 12 | 194 | 5.00 | 0.0 | 0.6 | 0.02 | 5.0 | 56 0.01 |
| 3.1 | 13 | 200 | 5.00 | 0.0 | 0.7 | 0.01 | 5.0 | 56 0.01 |
| 3.6 | 14 | 203 | 5.00 | 0.0 | 0.8 | 0.01 | 5.0 | 56 0.01 |
| 4.0 | 14 | 204 | 5.00 | 0.0 | 0.8 | 0.01 | 5.0 | 56 0.01 |
| 4.4 | 16 | 207 | 5.00 | 0.0 | 0.9 | 0.01 | 4.9 | 57 0.01 |
| 4.9 | 16 | 208 | 5.00 | 0.0 | 1.0 | 0.01 | 4.9 | 57 0.01 |
| 5.3 | 17 | 212 | 5.00 | 0.0 | 1.1 | 0.01 | 4.9 | 57 0.01 |
| 5.7 | 18 | 213 | 5.00 | 0.0 | 1.2 | 0.01 | 5.0 | 57 0.01 |
| 6.1 | 18 | 215 | 5.00 | 0.0 | 1.3 | 0.01 | 5.0 | 57 0.01 |
| 6.5 | 19 | 218 | 5.00 | 0.0 | 1.4 | 0.01 | 4.9 | 57 0.01 |
| 7.2 | 20 | 219 | 5.00 | 0.0 | 1.5 | 0.01 | 5.0 | 57 0.01 |
| 7.2 | 21 | 571 | 15.00 | 0.0 | 1.5 | 0.02 | 9.8 | 57 0.01 |
| 7.2 | 22 | 598 | 15.00 | 0.0 | 1.5 | 0.02 | 8.6 | 57 0.02 |
| 7.3 | 23 | 688 | 15.00 | 0.0 | 1.6 | 0.03 | 9.2 | 57 0.03 |
| 7.3 | 25 | 650 | 15.00 | 0.0 | 1.6 | 0.03 | 14.8 | 57 0.03 |
| 7.4 | 26 | 636 | 15.00 | 0.0 | 1.6 | 0.03 | 14.0 | 58 0.03 |
| 7.4 | 27 | 628 | 15.00 | 0.0 | 1.7 | 0.03 | 14.0 | 58 0.03 |
| 7.5 | 28 | 626 | 15.00 | 0.0 | 1.7 | 0.03 | 14.4 | 61 0.03 |
| 7.6 | 29 | 608 | 15.00 | 0.0 | 1.8 | 0.04 | 13.6 | 64 0.03 |
| 7.8 | 30 | 596 | 15.00 | 0.0 | 1.9 | 0.04 | 13.9 | 66 0.03 |
| 7.9 | 31 | 597 | 15.00 | 0.0 | 2.0 | 0.04 | 13.7 | 69 0.03 |
| 8.1 | 32 | 585 | 15.00 | 0.0 | 2.1 | 0.04 | 13.8 | 71 0.03 |
| 8.3 | 33 | 573 | 15.00 | 0.0 | 2.2 | 0.04 | 14.3 | 73 0.03 |
| 8.5 | 34 | 563 | 15.00 | 0.0 | 2.4 | 0.04 | 14.1 | 76 0.03 |
| 8.7 | 36 | 557 | 15.00 | 0.0 | 2.5 | 0.05 | 14.2 | 78 0.03 |
| 9.0 | 37 | 555 | 15.00 | 0.0 | 2.6 | 0.05 | 14.3 | 81 0.03 |
| 9.2 | 38 | 550 | 15.00 | 0.0 | 2.8 | 0.05 | 14.2 | 83 0.04 |
| 9.5 | 39 | 547 | 15.00 | 0.0 | 3.0 | 0.05 | 14.4 | 86 0.04 |
| 9.8 | 40 | 545 | 15.00 | 0.0 | 3.1 | 0.05 | 14.4 | 88 0.04 |
| 10.0 | 41 | 543 | 15.00 | 0.0 | 3.3 | 0.05 | 14.5 | 90 0.04 |
| 10.3 | 42 | 517 | 15.00 | 0.0 | 3.5 | 0.05 | 14.6 | 93 0.04 |
| 10.6 | 43 | 498 | 15.00 | 0.0 | 3.7 | 0.05 | 14.6 | 95 0.04 |
| 11.0 | 44 | 480 | 15.00 | 0.0 | 3.9 | 0.05 | 14.4 | 98 0.04 |
| 11.4 | 45 | 466 | 15.00 | 0.5 | 4.2 | 0.05 | 14.4 | 100 0.04 |
| Bridge Stage 3 at 11 min, at 24.4 (ft), Avg Dia/W 0.03/0.04 in | | | | | | | | |
| 11.8 | 47 | 458 | 15.00 | 0.5 | 4.4 | 0.05 | 14.5 | 100 0.04 |
| Bridge Stage 3 at 12 min, at 24.8 (ft), Avg Dia/W 0.03/0.04 in | | | | | | | | |
| ScreenOut in Stage 3 at Time = 11.8 min at 41 (ft) | | | | | | | | |
| 12.3 | 47 | 595 | 15.00 | 1.0 | 4.7 | 0.06 | 11.7 | 100 0.05 |
| Bridge Stage 3 at 12 min, at 36.0 (ft), Avg Dia/W 0.03/0.04 in | | | | | | | | |
| 12.8 | 47 | 789 | 15.00 | 2.0 | 5.0 | 0.07 | 10.7 | 100 0.07 |
| Bridge Stage 3 at 13 min, at 37.8 (ft), Avg Dia/W 0.03/0.05 in | | | | | | | | |
| 13.3 | 47 | 1020 | 15.00 | 2.0 | 5.4 | 0.09 | 10.0 | 100 0.09 |
| ScreenOut in Stage 4 at Time = 13.3 min at 38 (ft) | | | | | | | | |
| 13.8 | 47 | 1281 | 15.00 | 3.0 | 5.7 | 0.10 | 9.5 | 100 0.11 |
| ScreenOut in Stage 5 at Time = 14.3 min at 36 (ft) | | | | | | | | |
| 14.3 | 47 | 1563 | 15.00 | 4.0 | 6.0 | 0.12 | 9.0 | 100 0.14 |

| GEOMETRY SUMMARY * At End of Pumping Schedule | | | | | | | | | |
|--|-------|-------|--------|---------|-----------|-------|------|---------------------|------|
| SANTOS - E.MERENIE #37 (230/250) PRELIM. FRAC DESIGN | | | | | | | | | |
| Dstnce | Press | W-Avg | Q | Sh-Rate | Hght (ft) | Total | Bank | Prop | |
| (ft) | (psi) | (in) | (_BPM) | (1/sec) | | Up | Dn | Prop Fraction (PSF) | |
| 3 | 2529 | 0.27 | 7.5 | 36 | 100 | 41 | 4 | 88 | 0.01 |
| 6 | 2529 | 0.27 | 6.4 | 31 | 100 | 41 | 4 | 88 | 0.01 |
| 7 | 2529 | 0.27 | 6.2 | 30 | 100 | 41 | 4 | 88 | 0.01 |
| 8 | 2529 | 0.27 | 6.1 | 29 | 100 | 41 | 4 | 88 | 0.01 |
| 9 | 2529 | 0.27 | 5.9 | 28 | 100 | 41 | 4 | 88 | 0.01 |
| 10 | 2529 | 0.27 | 5.7 | 27 | 100 | 41 | 4 | 88 | 0.00 |
| 11 | 2529 | 0.27 | 5.5 | 26 | 100 | 41 | 4 | 88 | 0.00 |
| 12 | 2529 | 0.27 | 5.2 | 25 | 100 | 41 | 4 | 88 | 0.00 |
| 13 | 2529 | 0.27 | 5.0 | 24 | 99 | 40 | 4 | 87 | 0.00 |
| 14 | 2529 | 0.27 | 4.8 | 24 | 99 | 40 | 4 | 87 | 0.00 |
| 15 | 2529 | 0.27 | 4.7 | 23 | 98 | 39 | 4 | 86 | 0.00 |
| 16 | 2529 | 0.27 | 4.5 | 23 | 98 | 39 | 4 | 86 | 0.00 |
| 17 | 2529 | 0.26 | 4.4 | 22 | 97 | 38 | 4 | 85 | 0.00 |
| 18 | 2529 | 0.26 | 4.2 | 22 | 96 | 37 | 4 | 85 | 0.00 |
| 18 | 2529 | 0.26 | 4.1 | 21 | 96 | 37 | 4 | 84 | 0.00 |
| 19 | 2529 | 0.26 | 3.9 | 21 | 95 | 36 | 4 | 84 | 0.00 |
| 20 | 2529 | 0.26 | 3.7 | 20 | 94 | 35 | 4 | 83 | 0.00 |
| 21 | 2529 | 0.26 | 3.6 | 20 | 93 | 35 | 4 | 82 | 0.00 |
| 22 | 2529 | 0.26 | 3.4 | 19 | 92 | 33 | 3 | 81 | 0.00 |
| 23 | 2529 | 0.25 | 3.2 | 19 | 90 | 32 | 3 | 80 | 0.00 |
| 24 | 2529 | 0.25 | 2.9 | 18 | 89 | 31 | 3 | 79 | 0.00 |
| 25 | 2529 | 0.25 | 2.7 | 17 | 87 | 29 | 3 | 78 | 0.00 |
| 26 | 2529 | 0.25 | 2.5 | 16 | 86 | 28 | 3 | 76 | 0.00 |
| 27 | 2528 | 0.25 | 2.3 | 15 | 84 | 26 | 3 | 75 | 0.00 |
| 28 | 2528 | 0.25 | 2.1 | 14 | 82 | 25 | 3 | 73 | 0.00 |
| 30 | 2528 | 0.25 | 1.9 | 14 | 80 | 23 | 2 | 71 | 0.00 |
| 31 | 2527 | 0.25 | 1.7 | 13 | 78 | 21 | 2 | 69 | 0.00 |
| 32 | 2527 | 0.25 | 1.5 | 12 | 75 | 19 | 2 | 67 | 0.00 |
| 33 | 2526 | 0.25 | 1.4 | 11 | 73 | 16 | 2 | 65 | 0.00 |
| 34 | 2525 | 0.24 | 1.2 | 10 | 70 | 14 | 1 | 63 | 0.39 |
| 35 | 2524 | 0.24 | 1.0 | 9 | 67 | 11 | 1 | 61 | 0.86 |
| 36 | 2188 | 0.23 | 0.8 | 10 | 64 | 8 | 1 | 59 | 1.00 |
| 37 | 1547 | 0.13 | 0.7 | 34 | 57 | 2 | 0 | 56 | 1.00 |
| 38 | 1544 | 0.15 | 0.7 | 30 | 55 | 0 | 0 | 55 | 1.00 |
| 39 | 968 | 0.10 | 0.6 | 68 | 53 | 0 | 0 | 53 | 1.00 |
| 41 | 703 | 0.11 | 0.4 | 96 | 48 | 0 | 0 | 48 | 1.00 |
| 42 | 287 | 0.03 | 0.4 | 1629 | 35 | 0 | 0 | 35 | 1.00 |
| 43 | 259 | 0.02 | 0.6 | 3058 | 23 | 0 | 0 | 23 | 1.00 |
| 44 | 223 | 0.02 | 0.5 | 6044 | 19 | 0 | 0 | 19 | 1.00 |
| 45 | 182 | 0.02 | 0.3 | 6937 | 18 | 0 | 0 | 18 | 1.00 |
| 46 | 142 | 0.01 | 0.2 | 9999 | 18 | 0 | 0 | 18 | 1.00 |
| | | | | | | | | | 0.08 |

| | | | | | | | | | | | | |
|---|---|---|---|----|-----|------|-----|-----|-----|-----|-----|------|
| 9 | 0 | 2 | 1 | 15 | 6.0 | 11.2 | 3.5 | 6.2 | 0.0 | 143 | 427 | 0.01 |
| 9 | 0 | 2 | 1 | 12 | 6.0 | 8.6 | 4.3 | 6.5 | 0.0 | 141 | 404 | 0.00 |
| 9 | 0 | 2 | 1 | 4 | 6.0 | 7.0 | 5.2 | 6.7 | 0.0 | 78 | 391 | 0.00 |

| FLUID SUMMARY * At End of Pumping Schedule SANTOS -E MERENNIE #37 (230/250) PRELIM. FRAC DESIGN | | | | | | | | | | | | | |
|--|------|-------|----------|----|---------|----------|-----------------------------|---------------|---------------|--------------|------|------|------|
| No | Gone | Stage | Fluid ID | ID | Prop ID | Pos (ft) | Concentration In Now Design | F1 Vol (MGal) | Ex Temp (min) | Visc (deg_F) | (CP) | Frac | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 0.2 | 0.3 | 143 | 3 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 0.3 | 0.3 | 143 | 3 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 0.3 | 0.3 | 143 | 3 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 0.4 | 0.4 | 143 | 3 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 0.5 | 0.4 | 143 | 3 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 0.6 | 0.0 | 143 | 3 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 0.7 | 0.0 | 143 | 4 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 0.8 | 0.0 | 143 | 3 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 0.8 | 0.0 | 143 | 4 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 0.9 | 0.0 | 143 | 3 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 1.0 | 0.0 | 143 | 4 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 1.1 | 0.0 | 143 | 3 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 1.2 | 0.0 | 143 | 3 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 1.3 | 0.0 | 143 | 4 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 1.4 | 0.0 | 143 | 3 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 1.5 | 0.0 | 143 | 3 | 0.00 | |
| 1 | 1 | 1 | 1 | 1 | 47 | 0.0 | 0.0 | 1.5 | 0.0 | 143 | 5 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 1.5 | 0.1 | 143 | 7 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 1.5 | 0.1 | 143 | 8 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 1.5 | 0.1 | 143 | 10 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 1.6 | 0.2 | 143 | 11 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 1.6 | 0.2 | 143 | 12 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 1.7 | 0.2 | 143 | 11 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 1.7 | 0.2 | 143 | 11 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 1.8 | 0.2 | 143 | 11 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 1.9 | 0.2 | 143 | 11 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 2.0 | 0.2 | 143 | 12 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 2.1 | 0.2 | 143 | 12 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 2.2 | 0.2 | 143 | 12 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 2.4 | 0.2 | 143 | 12 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 2.5 | 0.2 | 143 | 12 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 2.6 | 0.3 | 143 | 13 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 2.8 | 0.3 | 143 | 13 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 3.0 | 0.3 | 143 | 13 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 3.1 | 0.3 | 143 | 16 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 3.3 | 0.3 | 143 | 99 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 3.5 | 0.3 | 143 | 100 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 3.7 | 0.4 | 143 | 164 | 0.00 | |
| 2 | 1 | 2 | 1 | 2 | 47 | 0.0 | 0.0 | 3.8 | 0.8 | 143 | 320 | 0.00 | |
| 3 | 1 | 2 | 1 | 2 | 47 | 0.5 | 45.3 | 0.0 | 4.7 | 1.5 | 143 | 383 | 0.00 |
| 3 | 1 | 2 | 1 | 2 | 40 | 0.5 | 45.3 | 0.0 | 4.2 | 0.9 | 143 | 606 | 0.00 |
| 3 | 1 | 2 | 1 | 2 | 40 | 0.5 | 45.3 | 0.0 | 4.3 | 2.5 | 143 | 739 | 0.00 |
| 3 | 1 | 2 | 1 | 2 | 39 | 1.0 | 45.3 | 0.0 | 4.4 | 1.0 | 143 | 674 | 0.02 |
| 3 | 1 | 2 | 1 | 2 | 38 | 1.0 | 45.3 | 0.0 | 4.7 | 2.0 | 143 | 621 | 0.00 |
| 4 | 1 | 2 | 1 | 2 | 37 | 2.0 | 45.3 | 0.0 | 4.7 | 1.5 | 143 | 570 | 0.02 |
| 5 | 1 | 2 | 1 | 2 | 36 | 2.0 | 45.3 | 0.0 | 5.0 | 2.0 | 143 | 524 | 0.00 |
| 5 | 0 | 2 | 1 | 2 | 35 | 2.0 | 37.9 | 0.6 | 5.1 | 2.5 | 143 | 490 | 0.02 |
| 6 | 0 | 2 | 1 | 2 | 33 | 3.0 | 27.8 | 1.0 | 5.3 | 2.0 | 143 | 453 | 0.00 |
| 6 | 0 | 2 | 1 | 2 | 31 | 3.0 | 13.0 | 1.6 | 5.4 | 2.0 | 143 | 320 | 0.00 |
| 7 | 0 | 2 | 1 | 2 | 29 | 4.0 | 17.3 | 1.8 | 5.6 | 1.5 | 143 | 383 | 0.00 |
| 7 | 0 | 2 | 1 | 2 | 26 | 4.0 | 10.7 | 2.5 | 5.8 | 1.0 | 143 | 606 | 0.00 |
| 8 | 0 | 2 | 1 | 2 | 23 | 5.0 | 13.2 | 2.6 | 5.9 | 1.0 | 143 | 100 | 0.00 |
| 8 | 0 | 2 | 1 | 2 | 19 | 5.0 | 9.3 | 3.4 | 6.2 | 0.5 | 143 | 164 | 0.00 |

PROPPANT SUMMARY * At End of Pumping Schedule
TOS - E.MERENIE #37 (230/250) PRELIM. FRAC DESIGN

**PROPPANT SUMMARY * At Fracture Closure
SANTOS - E MERFENTE #37 (230/250) PRETUM FBAC DESIGN**

| Lb/Sq-Ft | Lost to Embedment | Kfw (md-ft) | Prop ID--> 1 | Concentration(Total lb/sq foot) | 0.200 |
|----------|-------------------|----------------|--------------|---------------------------------|-------|
| 2.8 | 1525 | | | 0.90 | |
| 6.2 | 1522 | | | 0.90 | |
| 7.1 | 1528 | | | 0.90 | |
| 7.9 | 1511 | | | 0.90 | |
| 9.0 | 1516 | | | 0.90 | |
| 10.1 | 2024 | | | 1.10 | |
| 11.2 | 2011 | | | 1.10 | |
| 12.3 | 2010 | | | 1.10 | |
| 13.4 | 2009 | | | 1.10 | |
| 14.2 | 1998 | | | 1.10 | |
| 15.0 | 1995 | | | 1.10 | |
| 15.9 | 1995 | | | 1.10 | |
| 16.7 | 2285 | | | 1.20 | |
| 17.5 | 2244 | | | 1.20 | |
| 18.1 | 2424 | | | 1.30 | |
| 18.9 | 2416 | | | 1.30 | |
| 19.8 | 2412 | | | 1.30 | |
| 20.7 | 2403 | | | 1.30 | |
| 21.8 | 2383 | | | 1.30 | |
| 22.9 | 2839 | | | 1.50 | |
| 24.0 | 3589 | | | 1.80 | |
| 25.1 | 2935 | | | 1.50 | |
| 26.2 | 2770 | | | 1.40 | |
| 27.3 | 2599 | | | 1.40 | |
| 28.4 | 3585 | | | 1.80 | |
| 29.5 | 3546 | | | 1.80 | |
| 30.6 | 3838 | | | 1.90 | |
| 31.7 | 4994 | | | 2.40 | |
| 32.8 | 5066 | | | 2.50 | |
| 33.9 | 4998 | | | 2.40 | |
| 35.0 | 5653 | | | 2.70 | |
| 36.1 | 4759 | | | 2.30 | |
| 37.2 | 2420 | | | 1.30 | |
| 38.3 | 2612 | | | 1.40 | |
| 39.4 | 1622 | | | 0.90 | |
| 40.5 | 1933 | | | 1.10 | |
| 41.6 | 209 | | | 0.30 | |
| 42.7 | 57 | | | 0.20 | |
| 43.8 | 0 | | | 0.20 | |
| 44.9 | 56 | | | 0.20 | |
| 46.0 | 0 | | | 0.10 | |

| PROPPANT SUMMARY * At End of Pumping Schedule | | | |
|--|--------------|--------------------------------------|-------|
| SANTOS -E. MERIDENIE #37 (230/250) PRELIM. FRAC DESIGN | | | |
| Lb/sq-ft Lost to Embedment | KfW (ft) | Prop Concentration(Total lb/sq foot) | 0.200 |
| Distance (ft) | Prop ID--> 1 | | |
| 2.8 | 1817 | 1.00 | |
| 6.2 | 1816 | 1.00 | |
| 7.1 | 1820 | 1.00 | |
| 7.9 | 1906 | 1.10 | |
| 9.0 | 2149 | 1.20 | |
| 10.1 | 2154 | 1.20 | |
| 11.2 | 2148 | 1.20 | |
| 12.3 | 2148 | 1.20 | |
| 13.4 | 2143 | 1.20 | |
| 14.2 | 2134 | 1.20 | |
| 15.0 | 2222 | 1.20 | |
| 15.9 | 2253 | 1.20 | |
| 16.7 | 2222 | 1.20 | |
| 17.5 | 2217 | 1.20 | |
| 18.1 | 2213 | 1.20 | |
| 18.9 | 2204 | 1.20 | |
| 19.8 | 2196 | 1.20 | |
| 20.7 | 2186 | 1.20 | |
| 21.8 | 2544 | 1.40 | |
| 22.9 | 2758 | 1.50 | |
| 24.0 | 2730 | 1.50 | |
| 25.1 | 2448 | 1.30 | |
| 26.2 | 2335 | 1.30 | |
| 27.3 | 2922 | 1.50 | |
| 28.4 | 3221 | 1.70 | |
| 29.5 | 3226 | 1.70 | |
| 30.6 | 2756 | 1.50 | |
| 31.7 | 3749 | 1.90 | |
| 32.8 | 4082 | 2.10 | |
| 33.9 | 4517 | 2.30 | |
| 35.0 | 5221 | 2.60 | |
| 36.1 | 4648 | 2.30 | |
| 37.2 | 2364 | 1.30 | |
| 38.3 | 2551 | 1.40 | |
| 39.4 | 1584 | 0.90 | |
| 40.5 | 1888 | 1.10 | |
| 41.6 | 2084 | 0.30 | |
| 42.7 | 55 | 0.20 | |
| 43.8 | 0 | 0.20 | |
| 44.9 | 55 | 0.20 | |
| 46.0 | 0 | 0.10 | |

Frac Summary * SANTOS -E-MERENIE #37 (230/250) PRELIM. FRAC DESIGN
 Filename: EM37PD2.FRK ; Jul 28, 95

| Design Data | | | | | |
|--|----------------------------------|-------------|------------|-------------------------|---------------------------|
| FLUID LOSS LAYERS: | Top (ft) | Bottom (ft) | Thick (ft) | Loss Coef. (ft/sqrtnin) | Spurt (Gal/100 ft^2) |
| | 4610.0 | 4643.0 | 33.0 | 0.01600 | 0.50 |
| | 4643.0 | 4690.0 | 47.0 | 0.00300 | 0.00 |
| | 4690.0 | 4745.0 | 55.0 | 0.01200 | 0.40 |
| FORMATION: | Modulus (e6_psi) | | 155.0 | 0.06010 | 0.00 |
| | Perforated Height (ft) | | | | 5.50 |
| TEMPERATURE: | Bottom Hole (deg_F) | | | | 15.0 |
| PRESSURE: | Reservoir Pressure (psi) | | | | 10.000 |
| DEPTH: | Well Depth (ft) | | | | 3400.0 |
| | | | | | 4690.0 |
| FORMATION LAYER DATA - Multi-Layer Height Growth | | | | | |
| ---Depth(ftm) | | | | | |
| Top | Bottom | Thick | Top | Botm | Gradient Modulus (psi/in) |
| 4610.0 | 4643.0 | 33.0 | 2100.0 | 0.000 | 5.50 |
| 4643.0 | 4675.0 | 32.0 | 3850.0 | 0.000 | 6.50 |
| 4675.0 | 4690.0 | 15.0 | 3850.0 | 0.000 | 6.50 |
| 4690.0 | 4705.0 | 15.0 | 3400.0 | 0.000 | 6.50 |
| 4705.0 | 4709.0 | 4.0 | 3600.0 | 0.000 | 6.00 |
| 4709.0 | 4720.0 | 11.0 | 3400.0 | 0.000 | 5.50 |
| 4720.0 | 4732.0 | 12.0 | 3600.0 | 0.000 | 6.00 |
| 4732.0 | 4745.0 | 13.0 | 3400.0 | 0.000 | 5.50 |
| 4745.0 | | | 5000.0 | 0.000 | 7.50 |
| | Fluid Pressure Gradient (psi/ft) | | | | 0.450 |
| | Initial Fracture Top (ft) | | | | 4690 |
| | Initial Fracture Bottom (ft) | | | | 4705 |
| 3-D SIMULATOR | Step Size (ft) | | | | 1.1 |
| PROGRAM CONTROL | Time Step (min) | | | | 0.5 |

| Calculated Results from 3-D Simulator | | | | | |
|---------------------------------------|--|--|--------|---|------|
| STIMPLAN (TM), NSI, Tulsa, OK | Licensed To: Internal Use - NSI Technologies | | | | |
| 1/2 LENGTH: | 'Hydraulic' length (ft) | | 47.8 | 5 | 1.04 |
| | Propped Length (ft) | | 47.6 | 5 | 0.90 |
| PRESSURE: | Max Net Pressure (psi) | | 2677.8 | 5 | 0.90 |
| | Surface Pres-End of Pad (psi) | | 3206.7 | 5 | 0.90 |
| | Surface Pres-Start of Flush (psi) | | 6137.7 | 5 | 0.90 |
| | Surface Pres-End of Job (psi) | | 5945.8 | 5 | 0.90 |
| TIME: | Maximum Hydraulic Horsepower | | 2302 | 5 | 0.90 |
| | Max Exposure to Form. Temp. (min) | | 2.1 | 5 | 0.90 |
| | Time to Close (min) | | 1.7 | 5 | 0.90 |
| RATE: | Fluid Loss Rate during pad (-BPM) | | 14.65 | 5 | 0.90 |
| EFFICIENCY: | at end of pumping schedule | | 0.16 | 5 | 0.90 |
| PROPPANT: | Average In Situ Conc. (#/sq ft) | | 1.8 | 5 | 0.90 |
| HEIGHT: | Average Conductivity (md-ft) | | 3343 | 5 | 0.90 |
| WIDTH: | Max Fracture Height (ft) | | 99.6 | 5 | 0.90 |
| | Avg width at end of pumping (in) | | 0.19 | 5 | 0.90 |

| StimPlan 2.50 (TM) - NSI Technologies, Tulsa, OK Licensed To: Internal Use - NSI Technologies | | | | | |
|--|---------------------------------|------------------|----------------------|-----------|-----------------|
| WELL ID: | | | | | |
| SANTOS -E-MERENIE #37 (230/250) PRELIM. FRAC DESIGN | DEPTH: | Well Depth (ft) | 4690 | 5 | 0.90 |
| PRESSURE: | Reservoir Pressure (psi) | | 1770 | 5 | 0.90 |
| TEMPERATURE: | Bottom Hole Temperature (deg_F) | | 3400 | 5 | 0.90 |
| ** Pumping Schedule ** | | | | | |
| SI Vol (MGal) | Fl Vol (MGal) | Conc (%PGC) | Rate (BPM) | Prop Type | Cum Prop (MLBS) |
| 1.50 | 1.50 | 0.0 | 5.00 | 1 | 0.0 |
| 2.25 | 2.25 | 0.0 | 15.00 | 2 | 0.0 |
| 0.51 | 0.50 | 0.5 | 15.00 | 2 | 0.3 |
| 0.42 | 0.40 | 1.0 | 15.00 | 2 | 0.7 |
| 0.44 | 0.40 | 2.0 | 15.00 | 2 | 1.4 |
| 0.34 | 0.30 | 3.0 | 15.00 | 2 | 2.4 |
| 0.35 | 0.30 | 4.0 | 15.00 | 2 | 3.6 |
| 0.49 | 0.40 | 5.0 | 15.00 | 2 | 5.6 |
| 0.63 | 0.50 | 6.0 | 15.00 | 2 | 8.6 |
| Total Slurry ... | | 6.9 | Total Fluid ... | | 1.0 |
| Total Proppant ... | | 8.6 | Avg. Conc ... | | 6.6 |
| Total Pump Time | | 15.8 min | min | | 1.3 |
| Proppant ID No. | 1 | 20-40 CARBO-LITE | | | |
| Specific Gravity | | 2.72 | | | |
| Damage Factor | | 0.60 | | | |
| Propellant Stress (Mpsi) | 0 | 2 | Avg. Conc ... | | 1.3 |
| KFW @ 2 #/sq ft (mid-ft) | 10500 | 9200 | Total Pump Time | | 15.8 |
| Fluid ID No. | 1 | 10# SLICK_WATER | | | |
| Specific Gravity | | 1.04 | | | |
| vis (cp @ 170 1/sec) | 5 | 5 | Specific Gravity | | |
| non-Newtonian n' | 0.90 | 0.90 | vis (cp @ 170 1/sec) | | |
| K(lb.sec/in^2)x1000 | 0.17 | 0.17 | non-Newtonian n' | | |
| Q (-BPM) | dP/dL (psi/100ft) | | K(lb.sec/in^2)x1000 | | |
| Measured Depth (ft) | ... 4950.0 | | Q (-BPM) | | |

TABLE A-2

| Fluid ID No. | BORAGEL_H3595 |
|----------------------|--|
| Specific Gravity | 1.04 |
| vis (cp @ 170 1/sec) | @Wellbore @FormTemp @1Hr 225 175 10 2 @8HR |
| non-Newtonian n' | 325 0.40 0.42 0.90 0.95 |
| K(lb.sec/ft^2)x1000 | 0.38 122.80 160.82 70.51 0.34 0.05 |

| Time History * NSI STIMPLAN 3-D Fracture Simulation SANTOS -E.MERENNIE #37 (230/250) PRELIM. FRAC DESIGN | | | | | | | | | |
|---|-----------------------|---------------------|-------------|-------------|----------------|----------------|------------------------|------------------|------|
| Time (min) | Pen (ft) | Pres (psi) | Rate (_BPM) | Prop (_PPG) | SL Vol (Mcgal) | Efficiency (%) | Loss (_BPM) | Right W-Avg (ft) | (in) |
| 4.3 | 21 | 215 | 5.00 | 0.0 | 0.9 | 0.01 | 4.8 | 4.5 | 0.01 |
| 4.8 | 21 | 205 | 5.00 | 0.0 | 1.0 | 0.02 | 4.8 | 4.5 | 0.01 |
| 5.1 | 22 | 219 | 5.00 | 0.0 | 1.1 | 0.02 | 5.0 | 4.5 | 0.01 |
| 5.4 | 23 | 228 | 5.00 | 0.0 | 1.1 | 0.02 | 5.1 | 4.5 | 0.01 |
| 5.7 | 23 | 237 | 5.00 | 0.0 | 1.2 | 0.01 | 5.1 | 4.5 | 0.01 |
| 6.0 | 24 | 241 | 5.00 | 0.0 | 1.3 | 0.01 | 5.1 | 4.5 | 0.01 |
| 6.3 | 24 | 247 | 5.00 | 0.0 | 1.3 | 0.01 | 5.0 | 4.5 | 0.01 |
| 6.7 | 25 | 249 | 5.00 | 0.0 | 1.4 | 0.01 | 5.0 | 4.5 | 0.01 |
| 7.2 | 26 | 253 | 5.00 | 0.0 | 1.5 | 0.01 | 5.1 | 4.5 | 0.01 |
| 7.2 | 27 | 713 | 15.00 | 0.0 | 1.5 | 0.03 | 6.7 | 4.9 | 0.01 |
| 7.3 | 28 | 759 | 15.00 | 0.0 | 1.6 | 0.03 | 12.6 | 6.1 | 0.01 |
| 7.6 | 29 | 620 | 15.00 | 0.0 | 1.8 | 0.04 | 13.8 | 6.3 | 0.02 |
| 7.7 | 30 | 580 | 15.00 | 0.0 | 1.8 | 0.03 | 15.0 | 6.6 | 0.02 |
| 7.8 | 31 | 540 | 15.00 | 0.0 | 1.9 | 0.03 | 14.9 | 6.8 | 0.02 |
| 8.1 | 32 | 505 | 15.00 | 0.0 | 2.1 | 0.03 | 14.8 | 7.1 | 0.02 |
| 8.3 | 33 | 488 | 15.00 | 0.0 | 2.2 | 0.03 | 14.3 | 7.3 | 0.02 |
| 8.4 | 34 | 481 | 15.00 | 0.0 | 2.3 | 0.03 | 14.1 | 7.5 | 0.02 |
| 8.6 | 35 | 475 | 15.00 | 0.0 | 2.4 | 0.04 | 14.2 | 7.8 | 0.02 |
| 8.8 | 37 | 469 | 15.00 | 0.0 | 2.6 | 0.04 | 14.1 | 8.0 | 0.02 |
| 9.1 | 38 | 467 | 15.00 | 0.0 | 2.7 | 0.04 | 14.4 | 8.3 | 0.02 |
| 9.3 | 39 | 464 | 15.00 | 0.0 | 2.9 | 0.04 | 14.4 | 8.5 | 0.02 |
| 9.6 | 40 | 467 | 15.00 | 0.0 | 3.0 | 0.04 | 14.4 | 8.8 | 0.02 |
| 9.8 | 41 | 464 | 15.00 | 0.0 | 3.2 | 0.04 | 14.5 | 9.0 | 0.02 |
| 10.1 | 42 | 465 | 15.00 | 0.0 | 3.3 | 0.04 | 14.5 | 9.2 | 0.02 |
| 10.3 | 43 | 466 | 15.00 | 0.0 | 3.5 | 0.04 | 14.5 | 9.5 | 0.02 |
| 10.6 | 44 | 450 | 15.00 | 0.0 | 3.7 | 0.04 | 14.7 | 9.6 | 0.03 |
| 10.9 | 45 | 438 | 15.00 | 0.0 | 3.9 | 0.04 | 14.8 | 9.8 | 0.03 |
| 11.2 | 46 | 434 | 15.00 | 0.5 | 4.1 | 0.04 | 14.6 | 9.9 | 0.03 |
| Bridge Stage 3 | at 11 min, | at 24.5 (ft), | | | | | Avg Dia/W 0.03/0.03 in | | |
| 11.6 | 48 | 435 | 15.00 | 0.5 | 4.3 | 0.04 | 14.6 | 10.0 | 0.03 |
| Bridge Stage 3 | at 12 min, | at 27.4 (ft), | | | | | Avg Dia/W 0.03/0.02 in | | |
| 12.1 | 48 | 510 | 15.00 | 1.0 | 4.6 | 0.04 | 13.1 | 10.0 | 0.03 |
| Bridge Stage 3 | at 12 min, | at 31.0 (ft), | | | | | Avg Dia/W 0.03/0.03 in | | |
| ScreenOut in Stage 3 | at Time = 3 at Time = | 12.1 min at 44 (ft) | | | | | | | |
| 12.6 | 48 | 734 | 15.00 | 1.0 | 4.9 | 0.06 | 11.4 | 10.0 | 0.06 |
| Bridge Stage 4 | at 13 min, | at 25.6 (ft), | | | | | Avg Dia/W 0.03/0.05 in | | |
| 13.1 | 48 | 951 | 15.00 | 2.0 | 5.2 | 0.08 | 10.6 | 10.0 | 0.07 |
| Bridge Stage 4 | at 13 min, | at 35.1 (ft), | | | | | Avg Dia/W 0.03/0.06 in | | |
| 13.6 | 48 | 1205 | 15.00 | 3.0 | 5.5 | 0.09 | 9.9 | 10.0 | 0.09 |
| ScreenOut in Stage 4 | at Time = 4 at Time = | 13.6 min at 40 (ft) | | | | | | | |
| 14.1 | 48 | 1498 | 15.00 | 4.0 | 5.8 | 0.10 | 9.4 | 10.0 | 0.11 |
| 14.6 | 48 | 1814 | 15.00 | 5.0 | 6.2 | 0.12 | 9.0 | 10.0 | 0.13 |
| ScreenOut in Stage 5 | at Time = 5 at Time = | 14.6 min at 37 (ft) | | | | | | | |
| 15.1 | 48 | 2161 | 15.00 | 5.0 | 6.5 | 0.14 | 8.6 | 10.0 | 0.15 |
| 15.8 | 48 | 2678 | 15.00 | 6.0 | 6.9 | 0.16 | 8.2 | 10.0 | 0.18 |
| ScreenOut in Stage 6 | at Time = | 15.8 min at 35 (ft) | | | | | | | |
| 16.0 | 48 | 2410 | 0.00 | 0.0 | 6.9 | 0.14 | 8.1 | 10.0 | 0.18 |
| 16.4 | 48 | 2142 | 0.00 | 0.0 | 6.9 | 0.13 | 7.8 | 10.0 | 0.17 |
| 16.7 | 48 | 1874 | 0.00 | 0.0 | 6.9 | 0.12 | 7.7 | 10.0 | 0.16 |
| 17.1 | 48 | 1607 | 0.00 | 0.0 | 6.9 | 0.11 | 7.5 | 10.0 | 0.15 |
| 17.4 | 48 | 1339 | 0.00 | 0.0 | 6.9 | 0.10 | 7.4 | 10.0 | 0.14 |

| FLUID SUMMARY * At End of Pumping Schedule | | | | | | | | | | | |
|---|------|----------|---------|-----|---------------|--------|---------|-----------|-----------|-----------|------|
| SANTOS -E.MERENIE #37 (230/250) PRELIM. FRAC DESIGN | | | | | | | | | | | |
| Stage No | Gone | Fluid ID | Prop ID | Pos | Concentration | Fl Vol | Ex Temp | Tim (min) | Visc (cp) | Fall Frac | |
| | | ID | ID | In | Now | Design | (MGal) | (deg_F) | (cp) | | |
| 1 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 0.9 | 0.7 |
| 2 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.0 | 0.7 |
| 3 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.1 | 0.5 |
| 4 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.1 | 1.43 |
| 5 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.1 | 0.3 |
| 6 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.2 | 0.3 |
| 7 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.3 | 0.3 |
| 8 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.3 | 1.43 |
| 9 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.3 | 0.3 |
| 10 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.3 | 1.43 |
| 11 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.4 | 0.4 |
| 12 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.4 | 0.3 |
| 13 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 0.3 |
| 14 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 15 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 0.3 |
| 16 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 17 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 0.3 |
| 18 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 19 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 20 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 21 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 22 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 23 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 24 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 25 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 26 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 27 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 28 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 29 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 30 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 31 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 32 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 33 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 34 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 35 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 36 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 37 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 38 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 39 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 40 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 41 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 42 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 43 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 44 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 45 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 46 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 47 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |
| 48 | 1 | 1 | 1 | 1 | 1 | 1 | 48 | 0.0 | 0.0 | 1.5 | 1.43 |

| GEOMETRY SUMMARY * At End of Pumping Schedule | | | | | | | | | | | |
|---|-------------|------------|---------------|-----------------|----------|----------|-----------|--------------------------|-----------|------|----------|
| SANTOS -E.MERENIE #37 (230/250) PRELIM. FRAC DESIGN | | | | | | | | | | | |
| Dstnce (ft) | Press (psi) | Avg Q (in) | Sh-Rate (BPM) | Sh-Rate (1/sec) | Total Up | Total Dn | Hght (ft) | Bank Prop Fraction (PSF) | Bank Prop | Pos | Stage No |
| 9 | 2678 | 0.26 | 7.5 | 39 | 100 | 36 | 48 | 81 | 0.00 | 1.17 | 1 |
| 20 | 2677 | 0.24 | 4.1 | 26 | 91 | 28 | 48 | 74 | 0.00 | 1.32 | 1 |
| 21 | 2677 | 0.24 | 3.5 | 24 | 89 | 26 | 48 | 72 | 0.00 | 1.37 | 1 |
| 22 | 2677 | 0.24 | 3.5 | 24 | 88 | 26 | 48 | 71 | 0.00 | 1.37 | 1 |
| 23 | 2677 | 0.24 | 3.4 | 23 | 88 | 25 | 48 | 70 | 0.00 | 1.37 | 1 |
| 24 | 2677 | 0.24 | 3.3 | 23 | 87 | 25 | 48 | 69 | 0.00 | 1.38 | 1 |
| 25 | 2676 | 0.24 | 3.0 | 21 | 86 | 23 | 48 | 67 | 0.00 | 1.64 | 2 |
| 26 | 2676 | 0.24 | 2.8 | 21 | 84 | 21 | 48 | 65 | 0.00 | 1.64 | 2 |
| 27 | 2676 | 0.23 | 2.6 | 20 | 82 | 20 | 48 | 65 | 0.00 | 1.55 | 2 |
| 28 | 2676 | 0.23 | 2.4 | 19 | 81 | 19 | 48 | 64 | 0.00 | 1.55 | 2 |
| 29 | 2676 | 0.23 | 2.2 | 18 | 80 | 17 | 47 | 62 | 0.00 | 1.56 | 2 |
| 30 | 2675 | 0.23 | 2.0 | 17 | 78 | 16 | 47 | 61 | 0.00 | 1.77 | 2 |
| 31 | 2675 | 0.22 | 1.8 | 17 | 76 | 15 | 46 | 56 | 0.03 | 2.16 | 2 |
| 32 | 2675 | 0.22 | 1.6 | 16 | 75 | 15 | 45 | 54 | 0.03 | 2.02 | 2 |
| 33 | 2675 | 0.22 | 1.5 | 15 | 75 | 15 | 45 | 53 | 0.03 | 2.05 | 2 |
| 34 | 2674 | 0.22 | 1.5 | 15 | 71 | 15 | 42 | 44 | 0.78 | 3.17 | 2 |
| 35 | 2673 | 0.20 | 1.3 | 15 | 65 | 13 | 37 | 34 | 1.00 | 3.99 | 2 |
| 36 | 2672 | 0.19 | 1.1 | 17 | 59 | 11 | 33 | 28 | 1.00 | 4.59 | 2 |
| 37 | 2671 | 0.18 | 0.9 | 18 | 59 | 10 | 30 | 22 | 1.00 | 3.29 | 2 |
| 38 | 1799 | 0.14 | 0.8 | 39 | 54 | 25 | 18 | 1.00 | 3.51 | 2 | 1 |
| 39 | 1795 | 0.14 | 0.8 | 42 | 49 | 8 | 22 | 18 | 1.00 | 3.68 | 2 |
| 40 | 1793 | 0.15 | 0.7 | 36 | 45 | 8 | 22 | 18 | 1.00 | 3.68 | 2 |
| 41 | 1162 | 0.10 | 0.6 | 93 | 45 | 8 | 22 | 18 | 1.00 | 2.40 | 2 |
| 42 | 1156 | 0.10 | 0.7 | 78 | 45 | 8 | 22 | 18 | 1.00 | 2.45 | 2 |
| 43 | 1153 | 0.11 | 0.5 | 57 | 45 | 8 | 22 | 18 | 1.00 | 2.71 | 2 |
| 44 | 309 | 0.04 | 0.4 | 853 | 45 | 8 | 22 | 18 | 1.00 | 0.92 | 2 |
| 45 | 234 | 0.05 | 0.6 | 645 | 45 | 8 | 22 | 18 | 1.00 | 1.14 | 2 |
| 46 | 147 | 0.05 | 0.4 | 788 | 45 | 8 | 22 | 18 | 1.00 | 1.09 | 2 |
| 47 | 126 | 0.06 | 0.1 | 130 | 45 | 8 | 22 | 18 | 1.00 | 1.38 | 2 |

| PROPPANT SUMMARY * At End of Pumping Schedule SANTOS - E.MERENIE #37 (230/250) PRELIM. FRAC DESIGN | | | |
|---|--------------------------------------|--------------|------|
| Lb/Sq-Ft Lost to Embedment | Prop Concentration(Total 1b/sq foot) | 0.200 | |
| Distance (ft) | KfW (md-ft) | Prop ID--> 1 | |
| 9.0 | 2051 | 1.20 | |
| 19.7 | 2351 | 1.30 | |
| 21.4 | 2463 | 1.40 | |
| 21.7 | 2468 | 1.40 | |
| 22.2 | 2473 | 1.40 | |
| 22.8 | 2477 | 1.40 | |
| 23.3 | 2483 | 1.40 | |
| 23.9 | 2489 | 1.40 | |
| 24.4 | 2496 | 1.40 | |
| 25.1 | 2765 | 1.50 | |
| 26.0 | 3037 | 1.60 | |
| 27.1 | 2836 | 1.50 | |
| 28.2 | 2849 | 1.60 | |
| 29.3 | 2863 | 1.60 | |
| 30.4 | 3299 | 1.80 | |
| 31.5 | 4140 | 2.20 | |
| 32.6 | 3843 | 2.00 | |
| 33.7 | 3890 | 2.00 | |
| 34.8 | 6254 | 3.20 | |
| 35.9 | 7994 | 4.00 | |
| 37.0 | 9256 | 4.60 | |
| 38.1 | 6519 | 3.30 | |
| 39.2 | 6982 | 3.50 | |
| 40.3 | 7339 | 3.70 | |
| 41.4 | 4637 | 2.40 | |
| 42.5 | 4737 | 2.40 | |
| 43.6 | 5291 | 2.70 | |
| 44.7 | 1509 | 0.90 | |
| 45.8 | 1979 | 1.10 | |
| 46.9 | 1876 | 1.10 | |
| 47.6 | 2477 | 1.40 | |
| Average Conductivity (md-ft) | | | 3270 |

| PROPPANT SUMMARY * At Fracture Closure SANTOS - E.MERENIE #37 (230/250) PRELIM. FRAC DESIGN | | | |
|--|--------------------------------------|--------------|------|
| Lb/Sq-Ft Lost to Embedment | Prop Concentration(Total 1b/sq foot) | 0.200 | |
| Distance (ft) | KfW (md-ft) | Prop ID--> 1 | |
| 9.0 | 1922 | 1.10 | |
| 19.7 | 2170 | 1.20 | |
| 21.4 | 2689 | 1.50 | |
| 22.2 | 2694 | 1.50 | |
| 22.8 | 2697 | 1.50 | |
| 23.3 | 2700 | 1.50 | |
| 23.9 | 2704 | 1.50 | |
| 23.9 | 2709 | 1.50 | |
| 24.4 | 2714 | 1.50 | |
| 25.1 | 2721 | 1.50 | |
| 26.0 | 3596 | 1.90 | |
| 27.1 | 3575 | 1.90 | |
| 28.2 | 3311 | 1.70 | |
| 29.3 | 3321 | 1.80 | |
| 30.4 | 3330 | 1.80 | |
| 31.5 | 4512 | 2.30 | |
| 32.6 | 4526 | 2.30 | |
| 33.7 | 4565 | 2.30 | |
| 34.8 | 6572 | 3.30 | |
| 35.9 | 8112 | 4.00 | |
| 37.0 | 9393 | 4.60 | |
| 38.1 | 6615 | 3.30 | |
| 39.2 | 7086 | 3.50 | |
| 40.3 | 7447 | 3.70 | |
| 41.4 | 4706 | 2.40 | |
| 42.5 | 4807 | 2.40 | |
| 43.6 | 5369 | 2.70 | |
| 44.7 | 1532 | 0.90 | |
| 45.8 | 2009 | 1.10 | |
| 46.9 | 1904 | 1.10 | |
| 47.6 | 2513 | 1.40 | |
| Average Conductivity (md-ft) | | | 3343 |

| | |
|--|---------------------|
| StimPlan 2.50 (TM) - NSI Technologies, Tulsa, OK | |
| Licensed To: Internal Use - NSI Technologies | |
| WELL ID: | |
| SANTOS -E.MEREENIE #37 (230/250) | PRELIM. FRAC DESIGN |
| DEPTH: Well Depth (ft) ... | 4732 |
| PRESSURE: Reservoir Pressure (psi) ... | 1770 |
| Closure Pressure (psi) ... | 3400 |
| TEMPERATURE: Bottom Hole Temperature (deg_F) ... | 143 |

Frac Summary * SANTOS -E.MEREENIE #37 (230/250) PRELIM. FRAC DESIGN
Filename: EM37PD3.FRK ; Jul 28, 95

| Design Data | | | | | | | | | |
|---|----------------------------------|-----------------|-------------------|--------------------------|----------------------|--|--|--|--|
| FLUID LOSS LAYERS: | Top (ft) | Bottom (ft) | Thick (ft) | Loss Coef. (ft/sqr(min)) | Spurt (Gal/100 ft^2) | | | | |
| 4610.0 | 4643.0 | 33.0 | 0.01600 | 0.50 | | | | | |
| 4643.0 | 4690.0 | 47.0 | 0.00300 | 0.00 | | | | | |
| 4690.0 | 4745.0 | 55.0 | 0.01200 | 0.40 | | | | | |
| FORMATION: 4745.0 | 4900.0 | 155.0 | 0.00010 | 0.00 | | | | | |
| Modulus (e6 psi) | Perforated Height (ft) | Growth | | | | | | | |
| | Permeability (md) | | | | | | | | |
| | Temperature: Bottom Hole (deg_F) | | | | | | | | |
| | 10,000 | 13.0 | | | | | | | |
| | 143 | 10.000 | | | | | | | |
| TEMPERATURE: Reservoir Pressure (psi) | Top | Botm | Gradient (psi/ft) | Modulus (e6 Psi) | Toughness (psi/in) | | | | |
| PRESSURE: Closure Pressure (psi) | 2100.0 | 2100.0 | 0.000 | 5.50 | 3000.0 | | | | |
| DEPTH: Well Depth (ft) | 32.0 | 3850.0 | 0.000 | 6.50 | 3000.0 | | | | |
| FORMATION LAYER DATA - Multi-Layer Growth | | | | | | | | | |
| Depth(ft) | Top | Bottom | Stress (psi) | Modulus (e6 Psi) | Toughness (psi/in) | | | | |
| | 4610.0 | 4643.0 | 33.0 | 0.000 | 5.50 | | | | |
| | 4643.0 | 4675.0 | 32.0 | 0.000 | 6.50 | | | | |
| | 4675.0 | 4690.0 | 15.0 | 0.000 | 6.50 | | | | |
| | 4690.0 | 4705.0 | 15.0 | 0.000 | 5.50 | | | | |
| | 4705.0 | 4709.0 | 4.0 | 0.000 | 6.00 | | | | |
| | 4709.0 | 4720.0 | 11.0 | 0.000 | 5.50 | | | | |
| | 4720.0 | 4732.0 | 12.0 | 0.000 | 6.00 | | | | |
| | 4732.0 | 4745.0 | 13.0 | 0.000 | 5.50 | | | | |
| | 4745.0 | 5000.0 | 0.000 | 7.50 | 3000.0 | | | | |
| 3-D SIMULATOR PROGRAM CONTROL | Step Size (ft) | Time Step (min) | | | | | | | |
| | 1.1 | Automatic | | | | | | | |

| | |
|-------------------------|--------------------------|
| Fluid ID No. 1 | 10# SLICK WATER |
| Specific Gravity | 1.04 |
| Damage Factor, | 2.72 |
| Proppant Stress (Mpsi) | 0.60 |
| KFW @ 2 #/sq ft (md-ft) | 10500 9200 7600 3200 500 |

| | |
|----------|-------------------|
| Q (_BPM) | dP/dL (psi/100ft) |
| 5.0 | 30.0 |
| 10.0 | 32.0 |
| 15.0 | 40.0 |
| 20.0 | 60.0 |

TABLE A-3

| | |
|---|--------|
| Calculated Results from 3-D Simulator STIMPLAN (TM), NSI, Tulsa, OK | |
| Licensed To: Internal Use - NSI Technologies | |
| 1/2 LENGTH: 'Hydraulic' length (ft) | 50.3 |
| PRORESSED LENGTH: Popped length (ft) | 50.3 |
| MAX NET PRESSURE (PSI): | 1815.6 |
| PRESSURE: Surface Pres-End of Pad (psi) | 50.3 |
| | 3180.4 |
| Surface Pres-Start of Flush (psi) | 5250.2 |
| MAXIMUM HYDRAULIC HORSEPOWER: | 5064.7 |
| MAX EXPOSURE TO FORM. TEMP. (MIN.) | 1969 |
| TIME TO CLOSE (MIN.) | 1.1 |
| RATE: Fluid Loss Rate during pad (_BPM) | 0.0 |
| EFFICIENCY: at end of pumping during pad | 14.72 |
| PROPPANT: Average In Situ Cone. (#/sq ft) | 0.13 |
| AVERAGE CONDUCTIVITY (MD-FT) | 1.0 |
| MAX FRACTURE HEIGHT (FT) | 1810 |
| HEIGHT: Avg width at end of pumping (in) | 110.5 |
| WIDTH: | 0.10 |

Fluid ID No. 2

BORAGEL_H3595

| Specific Gravity | vis (cp @ 170 1/sec) | @FormTemp | @1Hr | 02Hr | 04Hr | 08HR | 1.04 |
|---------------------|----------------------|-----------|-------|-------|------|------|------|
| non-Newtonian n' | 0.38 | 325 | 275 | 225 | 175 | 10 | 2 |
| K(lb.sec/ft^2)x1000 | 160.82 | 122.80 | 95.44 | 70.51 | 0.34 | 0.95 | 0.05 |
| | | | | | | | |

| Time History * NSI STIMPLAN 3-D Fracture Simulation SANTOS -E.MEREEVIE #37 (230/250) PRELIM. FRAC DESIGN | | | | | | | |
|---|------------|---------------|-------------|------------|---------------------|------------------------|-----------------|
| Time (min) | Pen (ft) | Pres (psi) | Rate (.BPM) | Prop (PPG) | SI Vol (MGal) | Efficiency (%) | W-Avg (ft) (in) |
| 4.3 | 21 | 206 | 5.00 | 0.0 | 0.9 | 0.01 | 4.7 |
| 5.1 | 22 | 215 | 5.00 | 0.0 | 1.1 | 0.02 | 4.8 |
| 5.6 | 23 | 226 | 5.00 | 0.0 | 1.2 | 0.02 | 5.0 |
| 6.2 | 24 | 235 | 5.00 | 0.0 | 1.3 | 0.02 | 5.0 |
| 6.8 | 25 | 242 | 5.00 | 0.0 | 1.4 | 0.01 | 5.0 |
| 7.2 | 26 | 252 | 5.00 | 0.0 | 1.5 | 0.01 | 4.6 |
| 7.2 | 27 | 776 | 15.00 | 0.0 | 1.5 | 0.03 | 8.1 |
| 7.3 | 28 | 765 | 15.00 | 0.0 | 1.6 | 0.03 | 12.3 |
| 7.6 | 29 | 611 | 15.00 | 0.0 | 1.8 | 0.04 | 13.7 |
| 7.7 | 30 | 564 | 15.00 | 0.0 | 1.8 | 0.04 | 67 |
| 7.8 | 32 | 520 | 15.00 | 0.0 | 1.9 | 0.04 | 14.9 |
| 8.0 | 33 | 482 | 15.00 | 0.0 | 2.0 | 0.04 | 69 |
| 8.2 | 34 | 461 | 15.00 | 0.0 | 2.2 | 0.04 | 14.6 |
| 8.4 | 35 | 448 | 15.00 | 0.0 | 2.3 | 0.04 | 72 |
| 8.6 | 36 | 440 | 15.00 | 0.0 | 2.4 | 0.04 | 0.02 |
| 8.8 | 37 | 441 | 15.00 | 0.0 | 2.5 | 0.04 | 13.9 |
| 8.9 | 38 | 444 | 15.00 | 0.0 | 2.6 | 0.04 | 14.1 |
| 9.2 | 39 | 443 | 15.00 | 0.0 | 2.8 | 0.04 | 84 |
| 9.4 | 40 | 442 | 15.00 | 0.0 | 2.9 | 0.04 | 14.3 |
| 9.6 | 41 | 442 | 15.00 | 0.0 | 3.1 | 0.04 | 89 |
| 9.9 | 43 | 443 | 15.00 | 0.0 | 3.2 | 0.04 | 14.3 |
| 10.1 | 44 | 446 | 15.00 | 0.0 | 3.4 | 0.04 | 91 |
| 10.4 | 45 | 435 | 15.00 | 0.0 | 3.5 | 0.04 | 14.2 |
| 10.6 | 46 | 431 | 15.00 | 0.0 | 3.7 | 0.04 | 93 |
| 10.9 | 47 | 428 | 15.00 | 0.0 | 3.8 | 0.04 | 14.5 |
| 11.1 | 48 | 426 | 15.00 | 0.5 | 4.0 | 0.04 | 93 |
| 11.4 | 49 | 427 | 15.00 | 0.5 | 4.2 | 0.04 | 14.7 |
| Bridge Stage 3 | at 11 min, | at 40.2 (ft), | | | | Avg Dia/W 0.03/0.01 in | |
| 12.2 | 50 | 578 | 15.00 | 0.5 | 4.7 | 0.05 | 12.8 |
| Bridge Stage 3 | at 12 min, | at 35.5 (ft), | | | | Avg Dia/W 0.03/0.03 in | |
| 13.5 | 50 | 638 | 15.00 | 2.0 | 5.5 | 0.07 | 13.1 |
| ScreenOut in Stage 5 at Time = | | | | | 13.5 min at 37 (ft) | | 110 0.05 |
| 14.0 | 50 | 796 | 15.00 | 4.0 | 5.8 | 0.08 | 10.4 |
| 14.4 | 50 | 970 | 15.00 | 5.0 | 6.1 | 0.09 | 110 0.07 |
| ScreenOut in Stage 7 at Time = | | | | | 14.4 min at 24 (ft) | | 9.9 0.08 |
| 14.9 | 50 | 1257 | 15.00 | 5.0 | 6.4 | 0.10 | 9.5 0.09 |
| 15.3 | 50 | 1529 | 15.00 | 6.0 | 6.6 | 0.12 | 9.1 0.09 |
| 15.8 | 50 | 1816 | 15.00 | 6.0 | 6.9 | 0.13 | 8.6 0.10 |
| ScreenOut in Stage 7 at Time = | | | | | 15.8 min at 22 (ft) | | |

GEOMETRY SUMMARY * At End of Pumping schedule
CANTOS - E MENDONTE #37 (230/250) PRELIM. FRAC DESIGN

GEOMETRY SUMMARY * At End of Pumping Schedule

| Dstance | Press | W-Avg | Q | Sh-Rate | Hght (ft) | | | Bank | | | Prop |
|---------|-------|-------|-----|---------|-----------|------|-------|---------|-------|------|------|
| | | | | | (ft) | (in) | (BPM) | (1/sec) | Total | Up | Dn |
| 9 | 1816 | 0.23 | 7.5 | 48 | 110 | 83 | 15 | 102 | 0.01 | 1.15 | |
| 19 | 1816 | 0.20 | 3.5 | 31 | 94 | 67 | 14 | 85 | 0.01 | 1.61 | |
| 21 | 1816 | 0.20 | 2.9 | 27 | 93 | 66 | 14 | 83 | 1.00 | 2.12 | |
| 23 | 1815 | 0.20 | 2.7 | 26 | 92 | 65 | 14 | 83 | 1.00 | 2.14 | |
| 24 | 1815 | 0.20 | 2.5 | 25 | 91 | 64 | 14 | 82 | 1.00 | 2.22 | |
| 25 | 967 | 0.10 | 2.3 | 115 | 90 | 63 | 14 | 81 | 0.81 | 0.89 | |
| 26 | 966 | 0.10 | 3.1 | 112 | 89 | 62 | 14 | 80 | 0.82 | 0.89 | |
| 27 | 964 | 0.10 | 3.0 | 110 | 88 | 61 | 14 | 79 | 0.83 | 0.89 | |
| 28 | 962 | 0.10 | 2.8 | 108 | 87 | 60 | 14 | 78 | 0.83 | 0.89 | |
| 29 | 959 | 0.10 | 2.6 | 105 | 85 | 59 | 14 | 76 | 0.84 | 0.89 | |
| 30 | 956 | 0.10 | 2.4 | 103 | 84 | 57 | 14 | 75 | 0.85 | 0.89 | |
| 31 | 953 | 0.10 | 2.3 | 100 | 82 | 56 | 13 | 73 | 0.89 | 0.91 | |
| 32 | 950 | 0.10 | 2.1 | 97 | 81 | 54 | 13 | 72 | 0.90 | 0.92 | |
| 33 | 946 | 0.09 | 1.9 | 94 | 79 | 52 | 13 | 70 | 0.92 | 0.92 | |
| 34 | 943 | 0.09 | 1.8 | 93 | 77 | 51 | 13 | 68 | 0.94 | 0.92 | |
| 35 | 940 | 0.09 | 1.6 | 93 | 75 | 49 | 13 | 66 | 1.00 | 0.95 | |
| 36 | 938 | 0.10 | 1.4 | 79 | 72 | 47 | 13 | 63 | 1.00 | 1.07 | |
| 38 | 938 | 0.05 | 1.3 | 326 | 70 | 44 | 13 | 60 | 0.74 | 0.42 | |
| 39 | 588 | 0.05 | 1.7 | 343 | 66 | 41 | 12 | 56 | 0.93 | 0.50 | |
| 40 | 574 | 0.04 | 1.4 | 431 | 54 | 32 | 8 | 47 | 0.91 | 0.41 | |
| 41 | 552 | 0.04 | 1.2 | 535 | 51 | 30 | 8 | 45 | 0.93 | 0.38 | |
| 42 | 523 | 0.03 | 1.1 | 603 | 47 | 28 | 7 | 42 | 0.96 | 0.35 | |
| 43 | 489 | 0.03 | 0.9 | 695 | 45 | 26 | 6 | 40 | 1.00 | 0.33 | |
| 44 | 448 | 0.03 | 0.8 | 721 | 44 | 25 | 6 | 39 | 1.00 | 0.33 | |
| 45 | 402 | 0.03 | 0.7 | 689 | 44 | 25 | 6 | 39 | 1.00 | 0.34 | |
| 46 | 347 | 0.03 | 0.6 | 631 | 44 | 25 | 6 | 39 | 1.00 | 0.58 | |
| 47 | 290 | 0.05 | 0.5 | 342 | 44 | 25 | 6 | 39 | 1.00 | 0.77 | |
| 49 | 232 | 0.07 | 0.3 | 224 | 44 | 25 | 6 | 39 | 1.00 | 1.57 | |
| 50 | 145 | 0.15 | 0.2 | 111 | 44 | 25 | 6 | 39 | 1.00 | 1.37 | |
| | 121 | 0.13 | 0.2 | 8 | 44 | 25 | 6 | 39 | 1.00 | 6 | |

**FLUID SUMMARY * At end of Pumping Schedule
SANTOS -E.MEREENIE #37 (230/250) PRELIM. FRAC DESIGN**

**FLUID SUMMARY * At End of Pumping Schedule
SANTOS -E.MERENIE #37 (230/250) PRELIM. FRAC DESIGN**

| Stage | Fluid No | Pos ID | Prop ID | Concentration In | Fl Vol Now | Ex Design | Temp (deg.F) | Time (min) | Visc (cp) | Fall Frac |
|-------|----------|--------|---------|------------------|------------|-----------|--------------|------------|-----------|-----------|
| 1 | 1 | 1 | 1 | 50.0 | 0.0 | 0.0 | 0.0 | 0.9 | 1.0 | 4.00 |
| 1 | 1 | 1 | 1 | 50.0 | 0.0 | 0.0 | 0.0 | 1.1 | 0.6 | 4.00 |
| 1 | 1 | 1 | 1 | 50.0 | 0.0 | 0.0 | 0.0 | 1.2 | 0.5 | 4.00 |
| 1 | 1 | 1 | 1 | 50.0 | 0.0 | 0.0 | 0.0 | 1.3 | 0.6 | 4.00 |
| 1 | 1 | 1 | 1 | 50.0 | 0.0 | 0.0 | 0.0 | 1.4 | 0.7 | 4.00 |
| 1 | 1 | 1 | 1 | 50.0 | 0.0 | 0.0 | 0.0 | 1.5 | 0.3 | 3.00 |
| 1 | 1 | 1 | 1 | 50.0 | 0.0 | 0.0 | 0.0 | 1.5 | 0.3 | 3.00 |
| 1 | 1 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 1.5 | 0.3 | 21.00 |
| 1 | 2 | 2 | 1 | 50.0 | 0.0 | 0.0 | 0.0 | 1.5 | 0.3 | 18.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 1.6 | 0.4 | 23.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 1.8 | 0.4 | 26.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 1.8 | 0.4 | 26.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 1.9 | 0.3 | 26.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 1.9 | 0.3 | 26.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 2.0 | 0.4 | 25.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 2.2 | 0.4 | 24.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 2.3 | 0.4 | 24.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 2.4 | 0.2 | 24.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 2.5 | 0.2 | 24.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 2.6 | 0.2 | 24.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 2.6 | 0.2 | 24.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 2.8 | 0.2 | 24.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 2.9 | 0.3 | 23.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 3.1 | 0.5 | 21.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 3.2 | 0.5 | 22.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 3.2 | 0.5 | 22.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 3.4 | 0.5 | 23.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 3.5 | 0.5 | 23.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 3.7 | 0.5 | 23.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.0 | 0.0 | 0.0 | 3.8 | 0.3 | 32.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.5 | 45.3 | 0.0 | 3.8 | 0.8 | 31.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.5 | 45.3 | 0.0 | 4.0 | 0.6 | 21.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.5 | 45.3 | 0.0 | 4.2 | 1.1 | 39.00 |
| 2 | 2 | 1 | 2 | 50.0 | 0.5 | 45.3 | 0.0 | 4.3 | 1.1 | 42.00 |
| 2 | 2 | 1 | 2 | 50.0 | 1.0 | 45.3 | 0.0 | 4.7 | 0.0 | 69.00 |
| 2 | 2 | 1 | 2 | 50.0 | 2.0 | 45.3 | 0.0 | 4.7 | 0.0 | 143 |
| 2 | 2 | 1 | 2 | 50.0 | 3.0 | 45.3 | 0.0 | 5.1 | 0.4 | 184.00 |
| 2 | 2 | 1 | 2 | 50.0 | 4.0 | 45.3 | 0.0 | 5.4 | 0.0 | 170.00 |
| 2 | 2 | 1 | 2 | 50.0 | 5.0 | 45.3 | 0.0 | 5.5 | 0.0 | 143 |
| 2 | 2 | 1 | 2 | 50.0 | 6.0 | 45.3 | 0.0 | 5.5 | 0.0 | 161.00 |
| 2 | 2 | 1 | 2 | 50.0 | 7.0 | 45.3 | 0.0 | 5.8 | 0.0 | 426.00 |
| 2 | 2 | 1 | 2 | 50.0 | 8.0 | 45.3 | 0.0 | 6.1 | 0.0 | 143 |
| 2 | 2 | 1 | 2 | 50.0 | 9.0 | 45.3 | 0.0 | 6.3 | 0.0 | 381.00 |
| 2 | 2 | 1 | 2 | 50.0 | 10.0 | 45.3 | 0.0 | 6.3 | 0.0 | 333.00 |
| 2 | 2 | 1 | 2 | 50.0 | 11.0 | 45.3 | 0.0 | 6.6 | 0.0 | 143 |
| 2 | 2 | 1 | 2 | 50.0 | 12.0 | 45.3 | 0.0 | 6.6 | 0.0 | 143 |
| 2 | 2 | 1 | 2 | 50.0 | 13.0 | 45.3 | 0.0 | 6.6 | 0.0 | 143 |
| 2 | 2 | 1 | 2 | 50.0 | 14.0 | 45.3 | 0.0 | 6.8 | 0.0 | 143 |

| PROPPANT SUMMARY * At End of Pumping Schedule | | | |
|---|--------------|--------------------------------------|------|
| SANTOS -E. MERENITE #37 (230/250) PRELIM. FRAC DESIGN | | | |
| Lb/Sq-ft Lost to Embedment | 0.200 | Average Conductivity (md-ft) | 1810 |
| Distance (ft) | Kfw (md-ft) | Prop Concentration(Total lb/sq foot) | |
| | Prop ID--> 1 | | |
| 8.8 | 2092 | 1.20 | |
| 19.3 | 3094 | 1.60 | |
| 21.5 | 4210 | 2.10 | |
| 22.6 | 4261 | 2.10 | |
| 23.7 | 4441 | 2.20 | |
| 24.8 | 1507 | 0.90 | |
| 25.7 | 1509 | 0.90 | |
| 26.6 | 1511 | 0.90 | |
| 27.7 | 1510 | 0.90 | |
| 28.8 | 1509 | 0.90 | |
| 29.9 | 1508 | 0.90 | |
| 31.0 | 1560 | 0.90 | |
| 32.1 | 1570 | 0.90 | |
| 33.2 | 1574 | 0.90 | |
| 34.3 | 1576 | 0.90 | |
| 35.4 | 1651 | 1.00 | |
| 36.5 | 1913 | 1.10 | |
| 37.6 | 491 | 0.40 | |
| 38.7 | 660 | 0.50 | |
| 39.8 | 450 | 0.40 | |
| 40.9 | 395 | 0.40 | |
| 42.0 | 330 | 0.40 | |
| 43.1 | 281 | 0.30 | |
| 44.2 | 266 | 0.30 | |
| 45.3 | 282 | 0.30 | |
| 46.4 | 307 | 0.30 | |
| 47.5 | 833 | 0.60 | |
| 48.6 | 1249 | 0.80 | |
| 49.7 | 3002 | 1.60 | |
| 50.2 | 2568 | 1.40 | |

| PROPPANT SUMMARY * At Fracture Closure | | | |
|---|--------------|--------------------------------------|------|
| SANTOS -E. MERENITE #37 (230/250) PRELIM. FRAC DESIGN | | | |
| Lb/Sq-ft Lost to Embedment | 0.200 | Average Conductivity (md-ft) | 1810 |
| Distance (ft) | Kfw (md-ft) | Prop Concentration(Total lb/sq foot) | |
| | Prop ID--> 1 | | |
| 8.8 | 2092 | 1.20 | |
| 19.3 | 3094 | 1.60 | |
| 21.5 | 4210 | 2.10 | |
| 22.6 | 4261 | 2.10 | |
| 23.7 | 4441 | 2.20 | |
| 24.8 | 1507 | 0.90 | |
| 25.7 | 1509 | 0.90 | |
| 26.6 | 1511 | 0.90 | |
| 27.7 | 1510 | 0.90 | |
| 28.8 | 1509 | 0.90 | |
| 29.9 | 1508 | 0.90 | |
| 31.0 | 1560 | 0.90 | |
| 32.1 | 1570 | 0.90 | |
| 33.2 | 1574 | 0.90 | |
| 34.3 | 1576 | 0.90 | |
| 35.4 | 1651 | 1.00 | |
| 36.5 | 1913 | 1.10 | |
| 37.6 | 491 | 0.40 | |
| 38.7 | 660 | 0.50 | |
| 39.8 | 450 | 0.40 | |
| 40.9 | 395 | 0.40 | |
| 42.0 | 330 | 0.40 | |
| 43.1 | 281 | 0.30 | |
| 44.2 | 266 | 0.30 | |
| 45.3 | 282 | 0.30 | |
| 46.4 | 307 | 0.30 | |
| 47.5 | 833 | 0.60 | |
| 48.6 | 1249 | 0.80 | |
| 49.7 | 3002 | 1.60 | |
| 50.2 | 2568 | 1.40 | |

TABLE A-4

| StimPlan 2.50 (TM). NSI Technologies, Tulsa, OK Licensed To: Internal Use - NSI Technologies | | | | | | | | | |
|---|--|--|--|--|--|--|--|--|--|
| WELL ID: WELL ID: EM#37 (190/230/250) MINIFRAC EVALUATION | | | | | | | | | |
| SANTOS - Depth (ft) 4690 | | | | | | | | | |
| DEPTH: Well Depth (ft) 4690 | | | | | | | | | |
| PRESSURE: Reservoir Pressure (psi) 1770 | | | | | | | | | |
| Closure Pressure (psi) 3300 | | | | | | | | | |
| TEMPERATURE: Bottom Hole Temperature (deg_F) 143 | | | | | | | | | |
| FLUID LOSS LAYERS: Top (ft) 4610.0 | | | | | | | | | |
| FLUID LOSS LAYERS: Bottom (ft) 4643.0 | | | | | | | | | |
| FLUID LOSS LAYERS: Thick (ft) 33.0 | | | | | | | | | |
| Loss Coef. (ft/sqr(min)) 0.01000 | | | | | | | | | |
| Spur (Gal/100 ft^2) 0.50 | | | | | | | | | |
| FORMATION: Modulus (e6_psi) 4745.0 | | | | | | | | | |
| FORMATION: Perforated Height (ft) 155.0 | | | | | | | | | |
| FORMATION: Permeability (md) 0.00010 | | | | | | | | | |
| TEMPERATURE: Bottom Hole (deg_F) 10.000 | | | | | | | | | |
| PRESSURE: Reservoir Pressure (psi) 1770.0 | | | | | | | | | |
| DEPTH: Closure Pressure (psi) 3300.0 | | | | | | | | | |
| DEPTH: Well Depth (ft) 4690.0 | | | | | | | | | |
| FORMATION LAYER DATA - Multi-Layer Height Growth | | | | | | | | | |
| ---Depth(ft)----- | | | | | | | | | |
| Top (psi/in) | | | | | | | | | |
| Bottom (psi/in) | | | | | | | | | |
| Modulus (e6_psi) | | | | | | | | | |
| Toughness (psi) | | | | | | | | | |
| NSI Technologies | | | | | | | | | |
| STIMPLAN (TM), NSI, Tulsa, OK | | | | | | | | | |
| Licensed To: Internal Use - NSI Technologies | | | | | | | | | |
| 3-D SIMULATOR Step Size (ft) 2.0 | | | | | | | | | |
| PROGRAM CONTROL Time Step (min) 2.0 | | | | | | | | | |
| Automatic | | | | | | | | | |
| Calculated Results from 3-D Simulator | | | | | | | | | |
| STIMPLAN (TM), NSI, Tulsa, OK | | | | | | | | | |
| LICENSED TO: Internal Use - NSI Technologies | | | | | | | | | |
| 1/2 LENGTH: 'Hydraulic' length (ft) 79.4 | | | | | | | | | |
| TIME: Max Exposure to Form. Temp. (min) 0.8 | | | | | | | | | |
| PRESSURE: Propped Length (ft) 901.8 | | | | | | | | | |
| TIME: Max Exposure to Close (min) 0.7 | | | | | | | | | |
| RATE: Fluid Loss Rate during pad (BPM) 0.00 | | | | | | | | | |
| EFFICIENCY: at end of pumping schedule 0.17 | | | | | | | | | |
| PROPPELLANT: Average In Situ Conc. (#/sq ft) 0.0 | | | | | | | | | |
| AVERAGE CONDUCTIVITY (md-ft) 0 | | | | | | | | | |
| HEIGHT: Max Fracture Height (ft) 82.4 | | | | | | | | | |
| WIDTH: Avg width at end of pumping (in) 0.05 | | | | | | | | | |
| Fluid ID No. 3 BORAGEL | | | | | | | | | |
| Specific Gravity 1.04 | | | | | | | | | |
| Vis (cp @ 170 1/sec) 2.65 | | | | | | | | | |
| 'Damage Factor' 0.70 | | | | | | | | | |
| Proppant Stress (Mpsi) 0.0 | | | | | | | | | |
| KFW @ 2 #/sq ft (md-ft) 2.0 | | | | | | | | | |
| Step Size (ft) 2.0 | | | | | | | | | |
| Time Step (min) 2.0 | | | | | | | | | |
| Automatic | | | | | | | | | |

Fluid ID No. 1

BORRAGEL_H3595

Time History * NSI STIMPLAN 3-D Fracture Simulation
SANTOS - EN#37 (190/230/250) MINIFRAC EVALUATION

| Specific Gravity | @Wellbore | @FormTemp | @1HR | @2HR | 1.04 |
|----------------------|-----------|-----------|-------|-------|------|
| vis (cp @ 170 1/sec) | 325 | 275 | 225 | 175 | 2 |
| non-Newtonian n | 0.38 | 0.40 | 0.41 | 0.42 | 0.50 |
| R(lb.sec/ft^2)x1000 | 160.82 | 122.80 | 95.44 | 70.51 | 0.34 |
| | | | | | 0.05 |

| Time (min) | Pen (ft) | Pres (psi) | Rate (_BPM) | Prop (_PPG) | SI Vol (MGal) | Efficiency (_BPM) | Loss (ft) | W-Avg (in) |
|------------|----------|------------|-------------|-------------|---------------|-------------------|-----------|------------|
| 0.2 | 11 | 441 | 5.00 | 0.0 | 0.0 | 0.14 | 4.2 | 31 0.01 |
| 0.3 | 13 | 460 | 5.00 | 0.0 | 0.1 | 0.16 | 4.1 | 31 0.02 |
| 0.4 | 15 | 513 | 5.00 | 0.0 | 0.1 | 0.16 | 4.3 | 31 0.02 |
| 0.5 | 17 | 543 | 5.00 | 0.0 | 0.1 | 0.14 | 4.7 | 36 0.02 |
| 0.5 | 18 | 518 | 5.00 | 0.0 | 0.1 | 0.12 | 3.9 | 37 0.01 |
| 0.5 | 20 | 615 | 9.00 | 0.0 | 0.1 | 0.13 | 7.6 | 40 0.01 |
| 0.6 | 22 | 629 | 9.00 | 0.0 | 0.1 | 0.13 | 7.4 | 42 0.01 |
| 0.6 | 24 | 633 | 9.00 | 0.0 | 0.2 | 0.13 | 7.8 | 43 0.02 |
| 0.7 | 26 | 644 | 9.00 | 0.0 | 0.2 | 0.13 | 7.8 | 55 0.02 |
| 0.8 | 28 | 617 | 9.00 | 0.0 | 0.2 | 0.13 | 8.0 | 55 0.02 |
| 0.8 | 30 | 690 | 10.00 | 0.0 | 0.2 | 0.13 | 8.2 | 57 0.02 |
| 1.0 | 33 | 734 | 10.00 | 0.0 | 0.3 | 0.13 | 8.5 | 69 0.02 |
| 1.1 | 35 | 727 | 13.00 | 0.0 | 0.4 | 0.15 | 10.3 | 71 0.02 |
| 1.2 | 37 | 801 | 13.00 | 0.0 | 0.4 | 0.16 | 9.6 | 73 0.02 |
| 1.3 | 39 | 810 | 14.00 | 0.0 | 0.5 | 0.17 | 11.1 | 74 0.02 |
| 1.4 | 41 | 803 | 14.00 | 0.0 | 0.5 | 0.17 | 11.3 | 74 0.02 |
| 1.5 | 43 | 816 | 15.00 | 0.0 | 0.6 | 0.17 | 11.6 | 75 0.03 |
| 1.6 | 45 | 821 | 15.00 | 0.0 | 0.6 | 0.18 | 11.7 | 75 0.03 |
| 1.7 | 47 | 824 | 15.00 | 0.0 | 0.7 | 0.18 | 11.9 | 75 0.03 |
| 1.8 | 49 | 831 | 15.00 | 0.0 | 0.8 | 0.18 | 11.7 | 75 0.03 |
| 1.9 | 51 | 836 | 15.00 | 0.0 | 0.8 | 0.18 | 12.2 | 75 0.03 |
| 2.0 | 53 | 838 | 15.00 | 0.0 | 0.9 | 0.18 | 12.3 | 75 0.03 |
| 2.1 | 55 | 845 | 15.00 | 0.0 | 0.9 | 0.18 | 12.3 | 76 0.03 |
| 2.2 | 57 | 850 | 15.00 | 0.0 | 1.0 | 0.18 | 12.4 | 76 0.04 |
| 2.3 | 59 | 852 | 15.00 | 0.0 | 1.1 | 0.18 | 12.3 | 76 0.04 |
| 2.4 | 61 | 856 | 15.00 | 0.0 | 1.2 | 0.18 | 12.4 | 77 0.04 |
| 2.5 | 63 | 861 | 15.00 | 0.0 | 1.2 | 0.18 | 12.5 | 77 0.04 |
| 2.7 | 65 | 867 | 15.00 | 0.0 | 1.3 | 0.18 | 12.6 | 78 0.04 |
| 2.8 | 67 | 871 | 15.00 | 0.0 | 1.4 | 0.18 | 12.6 | 78 0.04 |
| 2.9 | 69 | 875 | 15.00 | 0.0 | 1.5 | 0.18 | 12.7 | 79 0.04 |
| 3.1 | 71 | 879 | 15.00 | 0.0 | 1.6 | 0.17 | 12.7 | 79 0.04 |
| 3.2 | 73 | 882 | 15.00 | 0.0 | 1.7 | 0.17 | 12.7 | 80 0.04 |
| 3.3 | 75 | 886 | 15.00 | 0.0 | 1.8 | 0.17 | 12.6 | 80 0.04 |
| 3.5 | 77 | 889 | 15.00 | 0.0 | 1.9 | 0.17 | 12.7 | 81 0.04 |
| 3.7 | 79 | 902 | 15.00 | 0.0 | 2.0 | 0.17 | 12.2 | 82 0.05 |
| 3.8 | 79 | 812 | 0.00 | 0.0 | 2.0 | 0.15 | 18.5 | 82 0.04 |
| 3.8 | 79 | 721 | 0.00 | 0.0 | 2.0 | 0.13 | 11.4 | 82 0.04 |
| 3.9 | 79 | 631 | 0.00 | 0.0 | 2.0 | 0.12 | 10.9 | 82 0.03 |
| 4.0 | 79 | 541 | 0.00 | 0.0 | 2.0 | 0.10 | 10.5 | 82 0.03 |
| 4.1 | 79 | 451 | 0.00 | 0.0 | 2.0 | 0.08 | 10.1 | 82 0.02 |
| 4.2 | 79 | 361 | 0.00 | 0.0 | 2.0 | 0.07 | 9.8 | 82 0.02 |
| 4.3 | 79 | 271 | 0.00 | 0.0 | 2.0 | 0.05 | 9.5 | 82 0.02 |
| 4.4 | 79 | 180 | 0.00 | 0.0 | 2.0 | 0.04 | 9.2 | 82 0.02 |

GEOMETRY SUMMARY * At End of Pumping Schedule
SANTOS - EM#37 (190/230/250) MINIFRAC EVALUATION

| Dstance (ft) | Press (psi) | W-Avg (in) | O_BPM | Sh-Rate (1/sec) | Hight (ft) | Total Up | Bank Dn | Prop Fraction (PSF) | Bank Prop Fraction |
|--------------|-------------|------------|-------|-----------------|------------|----------|---------|---------------------|--------------------|
| 4 | 894 | 0.07 | 7.4 | 634 | 82 | 20 | 33 | 70 | 0.00 |
| 10 | 878 | 0.07 | 6.8 | 637 | 80 | 18 | 33 | 68 | 0.00 |
| 12 | 872 | 0.07 | 6.7 | 646 | 79 | 17 | 33 | 68 | 0.00 |
| 14 | 866 | 0.07 | 6.6 | 659 | 79 | 16 | 32 | 67 | 0.00 |
| 16 | 859 | 0.07 | 6.4 | 672 | 78 | 15 | 32 | 66 | 0.00 |
| 17 | 854 | 0.06 | 6.3 | 685 | 77 | 15 | 32 | 66 | 0.00 |
| 19 | 847 | 0.06 | 6.2 | 705 | 77 | 14 | 32 | 65 | 0.00 |
| 21 | 839 | 0.06 | 6.1 | 713 | 76 | 14 | 32 | 65 | 0.00 |
| 23 | 832 | 0.06 | 5.9 | 718 | 76 | 13 | 32 | 64 | 0.00 |
| 25 | 825 | 0.06 | 5.8 | 726 | 75 | 13 | 32 | 64 | 0.00 |
| 27 | 817 | 0.06 | 5.6 | 734 | 75 | 13 | 32 | 64 | 0.00 |
| 29 | 810 | 0.06 | 5.5 | 742 | 75 | 13 | 31 | 63 | 0.00 |
| 31 | 801 | 0.06 | 5.3 | 757 | 74 | 13 | 31 | 63 | 0.00 |
| 34 | 791 | 0.06 | 5.1 | 760 | 74 | 13 | 31 | 63 | 0.00 |
| 36 | 783 | 0.05 | 4.9 | 767 | 74 | 13 | 31 | 62 | 0.00 |
| 38 | 775 | 0.05 | 4.8 | 774 | 74 | 13 | 30 | 62 | 0.00 |
| 40 | 767 | 0.05 | 4.6 | 780 | 73 | 13 | 30 | 62 | 0.00 |
| 42 | 759 | 0.05 | 4.5 | 785 | 73 | 13 | 30 | 61 | 0.00 |
| 44 | 750 | 0.05 | 4.3 | 790 | 73 | 13 | 29 | 61 | 0.00 |
| 46 | 741 | 0.05 | 4.1 | 794 | 72 | 13 | 29 | 61 | 0.00 |
| 48 | 732 | 0.05 | 3.9 | 797 | 72 | 13 | 29 | 60 | 0.00 |
| 50 | 745 | 0.05 | 3.7 | 756 | 72 | 13 | 29 | 60 | 0.00 |
| 52 | 725 | 0.04 | 3.4 | 957 | 72 | 13 | 28 | 60 | 0.00 |
| 54 | 714 | 0.04 | 3.2 | 1046 | 70 | 13 | 27 | 58 | 0.00 |
| 56 | 704 | 0.04 | 2.9 | 1117 | 67 | 13 | 24 | 54 | 0.00 |
| 58 | 693 | 0.03 | 2.6 | 1134 | 64 | 12 | 23 | 52 | 0.00 |
| 60 | 668 | 0.03 | 2.3 | 1906 | 59 | 9 | 19 | 46 | 0.00 |
| 62 | 639 | 0.02 | 2.0 | 2235 | 58 | 9 | 19 | 45 | 0.00 |
| 64 | 615 | 0.03 | 1.8 | 1813 | 44 | 4 | 10 | 31 | 0.00 |
| 66 | 610 | 0.03 | 1.6 | 1801 | 43 | 4 | 9 | 31 | 0.00 |
| 68 | 555 | 0.02 | 1.3 | 2457 | 39 | 4 | 6 | 31 | 0.00 |
| 70 | 561 | 0.03 | 1.1 | 1916 | 32 | 2 | 0 | 31 | 0.00 |
| 72 | 531 | 0.02 | 0.8 | 3899 | 30 | 0 | 0 | 30 | 0.00 |
| 74 | 433 | 0.01 | 0.5 | 9999 | 25 | 0 | 0 | 25 | 0.00 |
| 76 | 359 | 0.01 | 0.4 | 9999 | 20 | 0 | 0 | 20 | 0.00 |
| 78 | 269 | 0.01 | 0.2 | 9999 | 16 | 0 | 0 | 16 | 0.00 |

| |
|--|
| StimPlan 2.50 (TM) - NSI Technologies, Tulsa, OK |
| Licensed To: Internal Use - NSI Technologies |
| WELL ID: |
| SANTOS - EM#37 (190/230/250) FINAL FRAC DESIGN |
| DEPTH: Well Depth (ft) 4690 |
| PRESSURE: Reservoir Pressure (psi) 1770 |
| Closure Pressure (psi) 3300 |
| TEMPERATURE: Bottom Hole Temperature (deg_F) 143 |

Frac Summary * SANTOS - EM#37 (190/230/250) FINAL FRAC DESIGN
Filename: EM37FD.FRK ; Jul 30, 95

| Design Data | | | | | | | |
|--|----------------|-----------------|---|---------------------------|----------------------|------|--------|
| FLUID LOSS LAYERS: | Top (ft) | Bottom (ft) | Thick (ft) | Loss Coef. (ft/sqrt(min)) | Spurt (Gal/100 ft^2) | | |
| 4610.0 | 4643.0 | 33.0 | 0.01000 | 0.50 | | | |
| 4643.0 | 4690.0 | 47.0 | 0.00010 | 0.00 | | | |
| 4690.0 | 4745.0 | 55.0 | 0.00500 | 0.20 | | | |
| 4745.0 | 4900.0 | 155.0 | 0.00010 | 0.00 | | | |
| FORMATION: Modulus (e6_psi) | | | | | 6.63 | | |
| Perforated Height (ft) | | | | | 30.0 | | |
| Bottom Hole (deg_F) | | | | | 10.00 | | |
| Permeability (md) | | | | | 14.3 | | |
| TEMPERATURE: Reservoir Pressure (psi) | | | | | 1770.0 | | |
| PRESSURE: Closure Pressure (psi) | | | | | 3300.0 | | |
| DEPTH: Well Depth (ft) | | | | | 4690.0 | | |
| FORMATION LAYER DATA - Multi-Layer Height Growth | | | | | | | |
| ----Depth (ft)---- | | | | | | | |
| Top | Bottom | Thick | Stress (psi) -- Gradient Modulus (psi/in) | Bottom (psi/in) | | | |
| 4610.0 | 4643.0 | 33.0 | 2100.0 | 2100.0 | 0.000 | 5.50 | 3000.0 |
| 4643.0 | 4675.0 | 32.0 | 4500.0 | 4500.0 | 0.000 | 8.00 | 3000.0 |
| 4675.0 | 4690.0 | 15.0 | 4500.0 | 4500.0 | 0.000 | 8.00 | 3000.0 |
| 4690.0 | 4705.0 | 15.0 | 3300.0 | 3300.0 | 0.000 | 6.50 | 3000.0 |
| 4705.0 | 4709.0 | 4.0 | 4000.0 | 4000.0 | 0.000 | 7.50 | 3000.0 |
| 4709.0 | 4720.0 | 11.0 | 3400.0 | 3400.0 | 0.000 | 6.50 | 3000.0 |
| 4720.0 | 4732.0 | 12.0 | 4050.0 | 4050.0 | 0.000 | 7.50 | 3000.0 |
| 4732.0 | 4745.0 | 13.0 | 3500.0 | 3500.0 | 0.000 | 6.50 | 3000.0 |
| Total Slurry ... 8.1 Total Fluid ... 7.4 | 4745.0 | 5000.0 | 0.000 | 8.00 | 3000.0 | | |
| Total Proppant ... 14.8 Avg. Conc 2.0 | 4745.0 | 5000.0 | 0.000 | 8.00 | 3000.0 | | |
| Total Pump Time 18.0 min | 4745.0 | 5000.0 | 0.000 | 8.00 | 3000.0 | | |
| PROGRAM CONTROL | Step Size (ft) | Time Step (min) | | | 3.0 | | |
| 3-D SIMULATOR | | | | | 1.0 | | |

| | |
|---|-------------------|
| Proppant ID No. 1 | 20- 40 CARGO-LITE |
| Specific Gravity | 2.72 |
| 'Damage Factor' | 0.60 |
| Proppant Stress (Mpsi) | 0.16 |
| KW @ 2 #/sq ft (md-ft) 10500 9200 7600 3200 500 | 8 16 |

| | |
|----------------------------|-------------|
| Fluid ID No. 2 | SLICK_WATER |
| Specific Gravity | 1.04 |
| Vis (cp @ 170 1/sec) | 0.60 |
| 'n' non-Newtonian | 0.90 |
| K (lb.sec/ft^2)x1000 | 0.34 |
| FormTemp @2Hr | 0.34 |
| FormTemp @8Hr | 0.34 |
| Time Step (min) | 0.34 |

| | |
|---|--------|
| 1/2 LENGTH: 'Hydraulic' length (ft) | 117.2 |
| Propped Length (ft) | 115.7 |
| Max Net Pressure (psi) | 2694.5 |
| TIME: Max Exposure to Form. Temp. (min) | 4.6 |
| Time to Close (min) | 6.4 |
| RATE: Fluid Loss Rate during pad (BPM) | 12.87 |
| EFFICIENCY: at end of pumping schedule | 0.27 |
| PROPPANT: Average In Situ Conc. (#/sq ft) | 1.0 |
| Average Conductivity (md-ft) | 1874 |
| HEIGHT: Max Fracture Height (ft) | 123.1 |
| WIDTH: Avg width at end of pumping (in) | 0.18 |

TABLE A-5

Fluid ID No. 1

BORAGEL_H3595

| Specific Gravity | @FormTemp | @1HR | @2HR | @4HR | 0.04 |
|----------------------|-----------|--------|-------|-------|------|
| vis (cp @ 170 1/sec) | 325 | 225 | 175 | 10 | 2 |
| non-Newtonian n' | 0.38 | 0.40 | 0.41 | 0.42 | 0.44 |
| K(lb.sec/ft^2)x1000 | 160.82 | 122.80 | 95.44 | 70.51 | 0.95 |

Time History * NSI STIMPLAN 3-D Fracture Simulation
SANTOS - EM#37 (190/230/250) FINAL FRAC DESIGN

| Time (min) | Pen (ft) | Pres (psi) | Rate (BPM) | Prop (PPG) | SI. Vol (MGal) | Efficiency (% BPM) | Loss (ft) | W-Avg (in) |
|--------------------|----------|------------|-------------|----------------------|----------------|--------------------|-----------|------------|
| 0.3 | 14 | 355 | 5.00 | 0.0 | 0.1 | 0.10 | 4.4 | 31 0.01 |
| 0.4 | 17 | 381 | 5.00 | 0.0 | 0.1 | 0.11 | 4.3 | 32 0.01 |
| 0.6 | 20 | 408 | 5.00 | 0.0 | 0.1 | 0.11 | 4.5 | 34 0.01 |
| 0.7 | 23 | 426 | 5.00 | 0.0 | 0.1 | 0.10 | 4.7 | 34 0.01 |
| 0.9 | 26 | 441 | 5.00 | 0.0 | 0.2 | 0.09 | 4.8 | 35 0.01 |
| 1.0 | 29 | 455 | 5.00 | 0.0 | 0.2 | 0.08 | 4.8 | 35 0.01 |
| 1.3 | 32 | 464 | 5.00 | 0.0 | 0.3 | 0.07 | 4.8 | 35 0.01 |
| 1.5 | 35 | 468 | 5.00 | 0.0 | 0.3 | 0.07 | 4.8 | 36 0.01 |
| 1.8 | 38 | 476 | 5.00 | 0.0 | 0.4 | 0.07 | 4.8 | 36 0.01 |
| 2.1 | 41 | 484 | 5.00 | 0.0 | 0.4 | 0.07 | 4.8 | 36 0.02 |
| 2.4 | 44 | 491 | 5.00 | 0.0 | 0.5 | 0.06 | 4.8 | 36 0.02 |
| 2.7 | 47 | 498 | 5.00 | 0.0 | 0.6 | 0.06 | 4.8 | 36 0.02 |
| 3.1 | 50 | 501 | 5.00 | 0.0 | 0.6 | 0.06 | 4.8 | 36 0.02 |
| 3.5 | 53 | 507 | 5.00 | 0.0 | 0.7 | 0.06 | 4.8 | 37 0.02 |
| 3.9 | 56 | 513 | 5.00 | 0.0 | 0.8 | 0.06 | 4.8 | 37 0.02 |
| 4.3 | 59 | 517 | 5.00 | 0.0 | 0.9 | 0.05 | 4.8 | 37 0.02 |
| 4.8 | 62 | 523 | 5.00 | 0.0 | 1.0 | 0.05 | 4.8 | 38 0.02 |
| 5.3 | 65 | 530 | 5.00 | 0.0 | 1.1 | 0.05 | 4.9 | 38 0.02 |
| 5.9 | 68 | 531 | 5.00 | 0.0 | 1.2 | 0.05 | 4.8 | 38 0.02 |
| 6.5 | 71 | 544 | 5.00 | 0.0 | 1.4 | 0.05 | 4.8 | 39 0.02 |
| 7.2 | 73 | 537 | 5.00 | 0.0 | 1.5 | 0.05 | 4.8 | 39 0.02 |
| 7.4 | 76 | 980 | 8.00 | 0.0 | 1.6 | 0.05 | 5.9 | 58 0.02 |
| 7.9 | 79 | 907 | 8.00 | 0.0 | 1.8 | 0.06 | 6.7 | 75 0.02 |
| 8.4 | 81 | 957 | 12.00 | 0.0 | 2.0 | 0.09 | 8.4 | 82 0.03 |
| 9.3 | 84 | 1153 | 15.00 | 0.0 | 2.6 | 0.13 | 11.1 | 123 0.03 |
| 10.3 | 84 | 938 | 15.00 | 0.0 | 3.2 | 0.16 | 11.3 | 123 0.05 |
| 10.5 | 87 | 976 | 15.00 | 0.0 | 3.3 | 0.15 | 14.2 | 123 0.05 |
| 10.6 | 90 | 942 | 15.00 | 0.0 | 3.4 | 0.15 | 12.4 | 123 0.05 |
| 10.7 | 93 | 922 | 15.00 | 0.0 | 3.5 | 0.15 | 12.9 | 123 0.05 |
| 10.9 | 96 | 913 | 15.00 | 0.0 | 3.6 | 0.15 | 12.6 | 123 0.05 |
| 11.1 | 99 | 914 | 15.00 | 0.5 | 3.7 | 0.15 | 12.9 | 123 0.05 |
| 11.3 | 102 | 915 | 15.00 | 0.5 | 3.8 | 0.15 | 12.9 | 123 0.05 |
| 11.6 | 105 | 920 | 15.00 | 0.5 | 4.0 | 0.15 | 13.0 | 123 0.05 |
| 11.9 | 108 | 925 | 15.00 | 0.5 | 4.2 | 0.15 | 13.2 | 123 0.05 |
| 12.2 | 111 | 932 | 15.00 | 1.0 | 4.4 | 0.15 | 13.1 | 123 0.05 |
| 12.5 | 114 | 940 | 15.00 | 1.0 | 4.6 | 0.15 | 13.1 | 123 0.05 |
| 13.4 | 117 | 1082 | 15.00 | 1.0 | 5.2 | 0.16 | 11.3 | 123 0.06 |
| 14.3 | 117 | 1325 | 15.00 | 3.0 | 5.8 | 0.18 | 9.3 | 123 0.09 |
| Bridge Stage 5 at | | | 14 min, at | 99.3 (ft) | Avg Dia/W 0.03 | /0.05 in | | |
| ScreenOut in Stage | | | 5 at Time = | 14.3 min at 107 (ft) | | | | |
| 15.3 | 117 | 1630 | 15.00 | 4.0 | 6.3 | 0.21 | 8.4 | 123 0.11 |
| 16.2 | 117 | 1960 | 15.00 | 5.0 | 6.9 | 0.23 | 7.7 | 123 0.13 |
| 17.1 | 117 | 2316 | 15.00 | 6.0 | 7.5 | 0.25 | 7.2 | 123 0.15 |
| 18.0 | 117 | 2694 | 15.00 | 7.0 | 8.1 | 0.27 | 6.8 | 123 0.18 |
| 18.8 | 117 | 2425 | 0.00 | 0.0 | 8.1 | 0.25 | 6.6 | 123 0.17 |
| 19.7 | 117 | 2156 | 0.00 | 0.0 | 8.1 | 0.22 | 6.3 | 123 0.15 |
| 20.6 | 117 | 1886 | 0.00 | 0.0 | 8.1 | 0.20 | 6.0 | 123 0.14 |
| 21.5 | 117 | 1617 | 0.00 | 0.0 | 8.1 | 0.17 | 5.8 | 123 0.13 |
| 22.5 | 117 | 1347 | 0.00 | 0.0 | 8.1 | 0.15 | 5.6 | 123 0.12 |

| | | | | | | | | | |
|------|-----|------|------|-----|-----|------|-----|-----|------|
| 23.5 | 117 | 1078 | 0.00 | 0.0 | 8.1 | 0.14 | 5.4 | 123 | 0.11 |
| 24.4 | 117 | 808 | 0.00 | 0.0 | 8.1 | 0.13 | 5.2 | 123 | 0.11 |

| GEOMETRY SUMMARY * At End of Pumping Schedule SANTOS - EM#37 (190/230/250) FINAL FRAC DESIGN | | | | | | | | | |
|---|-------------|------------|---------|-----------------|----------|-----------|---------|------|----------------|
| Dstnce (ft) | Press (Psi) | W-Avg (in) | Q (BPM) | Sh-Rate (1/sec) | Total Up | Hght (ft) | Bank Dn | Prop | Fraction (PSF) |
| 5 | 2694 | 0.25 | 7.4 | 33 | 123 | 48 | 45 | 105 | 0.00 |
| 12 | 2693 | 0.22 | 6.4 | 42 | 108 | 36 | 41 | 92 | 0.00 |
| 15 | 2692 | 0.22 | 6.2 | 41 | 104 | 35 | 39 | 89 | 0.00 |
| 18 | 2691 | 0.22 | 5.9 | 41 | 101 | 33 | 38 | 86 | 0.00 |
| 21 | 2690 | 0.22 | 5.7 | 41 | 97 | 32 | 36 | 83 | 0.00 |
| 24 | 2688 | 0.22 | 5.4 | 41 | 94 | 30 | 34 | 80 | 0.00 |
| 27 | 2687 | 0.22 | 5.2 | 41 | 91 | 28 | 34 | 78 | 0.00 |
| 30 | 2686 | 0.22 | 5.0 | 41 | 89 | 25 | 33 | 76 | 0.00 |
| 33 | 2684 | 0.22 | 4.8 | 41 | 86 | 23 | 33 | 73 | 0.00 |
| 36 | 2683 | 0.21 | 4.6 | 43 | 82 | 19 | 33 | 70 | 0.00 |
| 39 | 2682 | 0.21 | 4.4 | 42 | 81 | 18 | 33 | 69 | 0.00 |
| 42 | 2680 | 0.21 | 4.2 | 40 | 80 | 18 | 33 | 68 | 0.00 |
| 45 | 2679 | 0.21 | 4.0 | 40 | 78 | 15 | 32 | 66 | 0.00 |
| 48 | 2677 | 0.21 | 3.8 | 40 | 77 | 15 | 32 | 66 | 0.00 |
| 51 | 2676 | 0.20 | 3.6 | 39 | 76 | 14 | 32 | 65 | 0.00 |
| 54 | 2675 | 0.20 | 3.4 | 39 | 76 | 13 | 32 | 64 | 0.00 |
| 57 | 2673 | 0.20 | 3.2 | 37 | 75 | 13 | 32 | 64 | 0.00 |
| 60 | 2672 | 0.20 | 3.0 | 36 | 75 | 13 | 31 | 63 | 0.00 |
| 63 | 2670 | 0.19 | 2.8 | 35 | 74 | 13 | 31 | 63 | 0.00 |
| 66 | 2669 | 0.19 | 2.6 | 33 | 74 | 13 | 31 | 63 | 0.00 |
| 69 | 2667 | 0.19 | 2.4 | 32 | 74 | 13 | 30 | 62 | 0.00 |
| 72 | 2666 | 0.19 | 2.2 | 30 | 73 | 13 | 30 | 62 | 0.00 |
| 75 | 2665 | 0.18 | 2.0 | 28 | 73 | 13 | 30 | 61 | 0.00 |
| 78 | 2663 | 0.18 | 1.8 | 26 | 72 | 13 | 29 | 61 | 0.00 |
| 80 | 2662 | 0.18 | 1.6 | 25 | 72 | 13 | 29 | 60 | 0.00 |
| 82 | 2661 | 0.18 | 1.5 | 23 | 71 | 13 | 28 | 60 | 0.00 |
| 84 | 2660 | 0.18 | 1.3 | 20 | 71 | 13 | 28 | 59 | 0.00 |
| 86 | 2660 | 0.17 | 1.3 | 21 | 71 | 13 | 28 | 59 | 0.00 |
| 89 | 2658 | 0.17 | 1.1 | 18 | 70 | 13 | 27 | 58 | 0.00 |
| 92 | 2657 | 0.16 | 0.9 | 18 | 66 | 12 | 24 | 53 | 0.00 |
| 95 | 2655 | 0.15 | 0.7 | 18 | 57 | 9 | 18 | 45 | 0.00 |
| 98 | 2649 | 0.13 | 0.5 | 25 | 42 | 4 | 8 | 31 | 0.00 |
| 101 | 2634 | 0.13 | 0.4 | 27 | 32 | 2 | 0 | 31 | 0.15 |
| 104 | 2626 | 0.13 | 0.3 | 21 | 32 | 2 | 0 | 31 | 0.79 |
| 107 | 2211 | 0.13 | 0.2 | 22 | 30 | 0 | 0 | 30 | 1.00 |
| 110 | 889 | 0.05 | 0.2 | 256 | 22 | 0 | 0 | 22 | 1.00 |
| 113 | 295 | 0.02 | 0.2 | 2676 | 18 | 0 | 0 | 18 | 1.00 |
| 116 | 188 | 0.04 | 0.2 | 1156 | 17 | 0 | 0 | 17 | 1.00 |

13 0 1 1 7 8.0 8.8 7.3 7.5 0.0 75 387 0.00

| FLUID SUMMARY * At End of Pumping Schedule SANTOS - EM#37 (190/230/250) FINAL FRAC DESIGN | | | | | | | | | | | |
|--|------|----------|---------|-----|---------------|---------------|---------------|--------------|-----------|-----------|----------|
| Stage No | Gone | Fluid ID | Prop ID | Pos | Concentration | Fl Vol (Mgal) | Ex Time (min) | Temp (deg_F) | Visc (cp) | Fall Frac | |
| | | | | In | Now Design | | | | | | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.1 | 0.1 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.1 | 0.3 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.1 | 0.3 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.1 | 0.2 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.2 | 0.2 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.2 | 0.3 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.3 | 0.3 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.3 | 0.3 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.4 | 0.3 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.4 | 0.3 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.5 | 0.3 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.6 | 0.4 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.6 | 0.4 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.7 | 0.4 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.7 | 0.5 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.8 | 0.5 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 0.9 | 0.5 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 1.0 | 0.5 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 1.1 | 0.6 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 1.2 | 0.6 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 1.4 | 0.4 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 1.5 | 0.4 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 1.5 | 0.5 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 1.6 | 0.5 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 1.6 | 0.6 | 143 | 6 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 1.8 | 0.7 | 143 | 22 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 1.8 | 1.7 | 143 | 19 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 2.0 | 1.0 | 143 | 14 0.00 | |
| 1 | 1 | 2 | 1 | 117 | 0.0 | 0.0 | 2.0 | 1.6 | 143 | 26 0.00 | |
| 2 | 2 | 1 | 1 | 117 | 0.0 | 0.0 | 2.6 | 1.0 | 143 | 12 0.00 | |
| 2 | 2 | 1 | 1 | 117 | 0.0 | 0.0 | 3.2 | 1.1 | 143 | 15 0.00 | |
| 2 | 2 | 1 | 1 | 117 | 0.0 | 0.0 | 3.3 | 1.0 | 143 | 15 0.00 | |
| 3 | 3 | 1 | 1 | 117 | 0.0 | 0.0 | 3.4 | 1.4 | 143 | 15 0.00 | |
| 3 | 3 | 1 | 1 | 117 | 0.0 | 0.0 | 2.0 | 1.0 | 143 | 86 0.00 | |
| 4 | 4 | 1 | 1 | 117 | 0.0 | 0.0 | 3.5 | 1.1 | 143 | 20 0.00 | |
| 4 | 4 | 1 | 1 | 117 | 0.0 | 0.0 | 3.5 | 1.8 | 143 | 294 0.00 | |
| 4 | 4 | 1 | 1 | 117 | 0.5 | 45.3 | 3.6 | 1.5 | 143 | 20 0.00 | |
| 4 | 4 | 1 | 1 | 117 | 0.5 | 45.3 | 3.7 | 1.5 | 143 | 352 0.00 | |
| 4 | 4 | 1 | 1 | 109 | 0.5 | 45.3 | 0.0 | 3.7 | 143 | 20 0.00 | |
| 5 | 5 | 1 | 1 | 109 | 0.5 | 45.3 | 0.0 | 3.8 | 2.2 | 143 | 403 0.00 |
| 5 | 5 | 1 | 1 | 107 | 0.5 | 45.3 | 0.0 | 4.0 | 1.9 | 143 | 408 0.00 |
| 5 | 5 | 1 | 1 | 107 | 0.5 | 45.3 | 0.0 | 3.4 | 1.43 | 477 0.00 | |
| 5 | 5 | 1 | 1 | 107 | 1.0 | 45.3 | 0.0 | 4.2 | 3.4 | 143 | 490 0.00 |
| 6 | 6 | 1 | 1 | 107 | 1.0 | 45.3 | 0.0 | 4.2 | 3.4 | 143 | 278 0.00 |
| 6 | 6 | 1 | 1 | 102 | 1.0 | 45.3 | 0.0 | 4.4 | 3.7 | 143 | 352 0.00 |
| 6 | 6 | 0 | 1 | 102 | 1.0 | 20.8 | 0.5 | 4.6 | 4.6 | 143 | 387 0.00 |
| 6 | 6 | 0 | 1 | 98 | 1.0 | 8.9 | 0.9 | 4.6 | 4.6 | 143 | 355 0.00 |
| 7 | 7 | 0 | 1 | 94 | 2.0 | 13.9 | 1.3 | 5.0 | 3.7 | 143 | 477 0.00 |
| 8 | 8 | 0 | 1 | 89 | 3.0 | 16.2 | 1.8 | 5.1 | 3.7 | 143 | 327 0.00 |
| 8 | 8 | 0 | 1 | 83 | 3.0 | 10.1 | 2.5 | 5.4 | 2.7 | 143 | 310 0.00 |
| 9 | 9 | 0 | 1 | 76 | 4.0 | 11.4 | 3.0 | 5.7 | 1.8 | 143 | 304 0.00 |
| 9 | 9 | 0 | 1 | 69 | 4.0 | 8.4 | 3.8 | 5.9 | 1.8 | 143 | 303 0.00 |
| 10 | 10 | 0 | 1 | 60 | 5.0 | 9.6 | 4.3 | 6.1 | 0.9 | 143 | 331 0.00 |
| 10 | 10 | 0 | 1 | 51 | 5.0 | 7.9 | 5.1 | 6.3 | 0.6 | 143 | 344 0.00 |
| 11 | 11 | 0 | 1 | 41 | 6.0 | 9.0 | 5.4 | 6.6 | 0.0 | 143 | 80 |
| 11 | 11 | 0 | 1 | 32 | 6.0 | 7.7 | 6.2 | 6.7 | 0.0 | 143 | 80 |
| 12 | 12 | 0 | 1 | 23 | 7.0 | 8.7 | 6.4 | 7.1 | 0.0 | 103 | 80 |
| 12 | 12 | 0 | 1 | 15 | 7.0 | 7.8 | 7.2 | 7.1 | 0.0 | 15 | 80 |

| PROPPANT SUMMARY * At End of Pumping Schedule SANTOS - EM#37 (190/230/250) FINAL FRAC DESIGN | | | |
|---|--|--------------|------|
| Lb/Sq-Ft Lost to Embedment | Prop Concentration(Total lb/sq foot) | 0.200 | |
| Distance (ft) | KFW (md-ft) | Prop ID--> 1 | |
| 5.3 | 2085 | 1.10 | |
| 12.0 | 1831 | 1.00 | |
| 15.0 | 1738 | 1.00 | |
| 18.0 | 1796 | 1.00 | |
| 21.0 | 1803 | 1.00 | |
| 24.0 | 1807 | 1.00 | |
| 27.0 | 1795 | 1.00 | |
| 30.0 | 1736 | 1.00 | |
| 33.0 | 1602 | 0.90 | |
| 36.0 | 1753 | 1.00 | |
| 39.0 | 1749 | 1.00 | |
| 42.0 | 1747 | 1.00 | |
| 45.0 | 1736 | 1.00 | |
| 48.0 | 1645 | 0.90 | |
| 51.0 | 1467 | 0.90 | |
| 54.0 | 1563 | 0.90 | |
| 57.0 | 1702 | 1.00 | |
| 60.0 | 1691 | 1.00 | |
| 63.0 | 1680 | 1.00 | |
| 66.0 | 1505 | 0.90 | |
| 69.0 | 1437 | 0.90 | |
| 72.0 | 1508 | 0.90 | |
| 75.0 | 1836 | 1.00 | |
| 77.6 | 1825 | 1.00 | |
| 79.8 | 1633 | 0.90 | |
| 82.5 | 1595 | 0.90 | |
| 84.1 | 1574 | 0.90 | |
| 85.7 | 1569 | 0.90 | |
| 88.7 | 2088 | 1.20 | |
| 91.7 | 1830 | 1.00 | |
| 94.7 | 1849 | 1.00 | |
| 97.7 | 1549 | 0.90 | |
| 100.7 | 1403 | 0.80 | |
| 103.7 | 2368 | 1.30 | |
| 106.7 | 2207 | 1.20 | |
| 109.7 | 677 | 0.50 | |
| 112.7 | 61 | 0.20 | |
| 115.7 | 392 | 0.40 | |
| Average Conductivity (md-ft) | | | 1656 |

| PROPPANT SUMMARY * At Fracture Closure SANTOS - EM#37 (190/230/250) FINAL FRAC DESIGN | | | |
|--|--|--------------|------|
| Lb/Sq-Ft Lost to Embedment | Prop Concentration(Total lb/sq foot) | 0.200 | |
| Distance (ft) | KFW (md-ft) | Prop ID--> 1 | |
| 5.3 | 1419 | 0.80 | |
| 12.0 | 1262 | 0.70 | |
| 15.0 | 1278 | 0.80 | |
| 18.0 | 1291 | 0.80 | |
| 21.0 | 1333 | 0.80 | |
| 24.0 | 1690 | 0.90 | |
| 27.0 | 1688 | 0.90 | |
| 30.0 | 1686 | 0.90 | |
| 33.0 | 1684 | 0.90 | |
| 36.0 | 1682 | 0.90 | |
| 39.0 | 1683 | 0.90 | |
| 42.0 | 1706 | 0.90 | |
| 45.0 | 2080 | 1.10 | |
| 48.0 | 1984 | 1.10 | |
| 51.0 | 1959 | 1.00 | |
| 54.0 | 1936 | 1.00 | |
| 57.0 | 1928 | 1.00 | |
| 60.0 | 1887 | 1.00 | |
| 63.0 | 1988 | 1.10 | |
| 66.0 | 2146 | 1.10 | |
| 69.0 | 2137 | 1.10 | |
| 72.0 | 2136 | 1.10 | |
| 75.0 | 2053 | 1.10 | |
| 77.6 | 2035 | 1.10 | |
| 79.8 | 2505 | 1.30 | |
| 82.5 | 2553 | 1.30 | |
| 84.1 | 2512 | 1.30 | |
| 85.7 | 2428 | 1.20 | |
| 88.7 | 2383 | 1.20 | |
| 91.7 | 3023 | 1.30 | |
| 94.7 | 3069 | 1.50 | |
| 97.7 | 2924 | 1.50 | |
| 100.7 | 2807 | 1.40 | |
| 103.7 | 2742 | 1.40 | |
| 106.7 | 2326 | 1.20 | |
| 109.7 | 714 | 0.50 | |
| 112.7 | 64 | 0.20 | |
| 115.7 | 413 | 0.40 | |
| Average Conductivity (md-ft) | | | 1874 |

Frac Summary * SANTOS - EM#37 (190/230/250) POST-FRAC EVALUATION
 Filename: EM37PF1.FRK ; Feb 12, 96

| Design Data | | | | | | |
|---|----------------------------------|-------------|-------------------|---------------------------|----------------------------------|--|
| FLUID LOSS LAYERS: | Top (ft) | Bottom (ft) | Thickness (ft) | Loss Coef. (ft/sqrt(min)) | Spurt (Gal/100 ft ²) | |
| 4610.0 | 4643.0 | 33.0 | 0.01000 | 0.50 | | |
| 4643.0 | 4690.0 | 47.0 | 0.00010 | 0.00 | | |
| 4690.0 | 4745.0 | 55.0 | 0.00440 | 0.45 | | |
| 4745.0 | 4900.0 | 155.0 | 0.00010 | 0.00 | | |
| FORMATION: Modulus (e6 psi) | | | 6.63 | | | |
| Perforated Height (ft) | | | 30.0 | | | |
| Permeability (md) | | | 10.000 | | | |
| TEMPERATURE: Bottom Hole (deg_F) | | | 143 | | | |
| PRESSURE: Reservoir Pressure (psi) | | | 1770.0 | | | |
| DEPTH: Closure Pressure (psi) | | | 3300.0 | | | |
| Well Depth (ft) | | | 4690.0 | | | |
| FORMATION LAYER DATA - Multi-Layer Height Growth - Stress (psi) -- Gradient Modulus Toughness | | | | | | |
| Top Botm. | Thick. | Top Botm. | (psi/ft) (e6 psi) | (psi/in) | | |
| 4610.0 | 4643.0 | 33.0 | 2100.0 | 0.000 | 5.50 | |
| 4643.0 | 4675.0 | 32.0 | 4500.0 | 0.000 | 8.00 | |
| 4675.0 | 4690.0 | 15.0 | 4500.0 | 0.000 | 8.00 | |
| 4690.0 | 4705.0 | 15.0 | 3300.0 | 0.000 | 6.50 | |
| 4705.0 | 4709.0 | 4.0 | 4000.0 | 0.000 | 7.50 | |
| 4709.0 | 4720.0 | 11.0 | 3400.0 | 0.000 | 6.50 | |
| 4722.0 | 4732.0 | 12.0 | 4050.0 | 0.000 | 7.00 | |
| 4732.0 | 4745.0 | 13.0 | 3500.0 | 0.000 | 6.50 | |
| 4745.0 | Fluid Pressure Gradient (psi/ft) | 4500.0 | 0.000 | 7.50 | 3000.0 | |
| PROGRAM CONTROL | Step Size (ft) | | 3.0 | | | |
| | Time Step (min) | | 1.0 | | | |
| Initial Fracture Top (ft)..... | | | | | | |
| | Initial Fracture Bottom (ft) | | 4690 | | | |
| | | 4720 | | | | |

6.1

| StimPlan 2.50 (TM) - NSI Technologies, Tulsa, OK Licensed To: Internal Use - NSI Technologies | | | |
|--|---------------------------------|----------------------|------|
| WELL ID: | | | |
| SANTOS - EM#37 | (190/230/250) | POST-FRAC EVALUATION | |
| DEPTH: | Well Depth (ft) | | 4690 |
| PRESSURE: | Reservoir Pressure (psi) | | 1770 |
| CLOSURE PRESSURE: | Closure Pressure (psi) | | 3300 |
| TEMPERATURE: | Bottom Hole Temperature (deg_F) | | 143 |

| ** Pumping Schedule ** | | | | | | |
|------------------------|---------------|-----------------|-------------|------------|-----------|-----------------|
| SL Vol (Mgal) | Fl Vol (Mgal) | Conc (_PPG) | Rate (_BPM) | Fluid Type | Prop Type | Cum Prop (MLbs) |
| 1.57 | 1.57 | 0.0 | 4.80 | 2 | 1 | 0.0 |
| 0.57 | 0.57 | 0.0 | 8.00 | 1 | 1 | 0.0 |
| 0.57 | 0.57 | 0.0 | 13.75 | 1 | 1 | 0.0 |
| 0.72 | 0.72 | 0.0 | 14.84 | 1 | 1 | 0.0 |
| 0.86 | 0.83 | 0.7 | 15.25 | 1 | 1 | 0.6 |
| 0.49 | 0.46 | 1.3 | 15.21 | 1 | 1 | 0.8 |
| 0.49 | 0.44 | 2.4 | 15.40 | 1 | 1 | 2.2 |
| 0.48 | 0.41 | 3.7 | 15.46 | 1 | 1 | 0.8 |
| 0.70 | 0.57 | 5.0 | 15.29 | 1 | 1 | 6.6 |
| 0.63 | 0.49 | 6.3 | 15.23 | 1 | 1 | 9.7 |
| 0.46 | 0.34 | 7.7 | 16.67 | 1 | 1 | 12.3 |
| 0.36 | 0.26 | 8.5 | 16.10 | 1 | 1 | 14.5 |
| 0.24 | 0.18 | 7.4 | 16.10 | 1 | 1 | 15.8 |
| Total Slurry ... | 8.1 | | | | | 7.4 |
| Total Proppant ... | 15.8 | Avg. Conc | 2.1 | | | |
| Total Pump Time | 18.8 min | | | | | |

TABLE A-6

| SLICK WATER | | | | | | |
|-------------------------|-------|------|------|------|-----|------|
| Specific Gravity | | | | | | 2.72 |
| 'Damage Factor' | | | | | | 0.60 |
| Proppant Stress (Mpsi) | 0 | 2 | 4 | 8 | 16 | |
| KRW @ 2 #/sq ft (md-ft) | 10500 | 9200 | 7600 | 3200 | 500 | |
| Fluid ID No. 2 | | | | | | |
| Specific Gravity | | | | | | |
| 'Damage Factor' | | | | | | |
| Proppant Stress (Mpsi) | 0 | 2 | 4 | 8 | 16 | |
| KRW @ 2 #/sq ft (md-ft) | 10500 | 9200 | 7600 | 3200 | 500 | |

Calculated Results from 3-D Simulator
 STIMPLAN (TM) - NSI , Tulsa,OK
 Licensed To: Internal Use - NSI Technologies

| SLICK WATER | | | | | | |
|-----------------------------------|-------|------|------|------|------|-------|
| Specific Gravity | | | | | | 1.04 |
| 'Weibor @FormTwp | | | | | | 0.6HR |
| vis (cp @ 170 1/sec) | 2 | 2 | 2 | 2 | 2 | 0.8HR |
| non-Newtonian 'n' | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| K(lb.sec./ft ²).x1000 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |

| Fluid ID No. | 1 | BORAGEL_H3595 | | | | | |
|----------------------|--------|---------------|--------|--------|-------|------|------|
| Specific Gravity | 1.04 | | | | | | |
| vis (cp @ 170 1/sec) | 0.400 | @Wellbor | 0.04 | 0.04 | | | |
| non-Newtonian n | 0.38 | 0.350 | 0.1Hr | 0.2Hr | | | |
| K(lb.sec/ft^2)x1000 | 156.29 | 0.40 | 0.41 | 0.42 | 0.90 | 0.95 | |
| | 197.93 | 156.29 | 116.65 | 116.65 | 70.51 | 0.34 | 0.05 |

| Time History * NSI STIMPLAN 3-D Fracture Simulation SANTOS - EM#37 (190/230/250) POST-FRAC EVALUATION | | | | | | | | | |
|---|----------|------------|------------|------------|----------------|----------------|------------|-------------|------------|
| Time (min) | Pen (ft) | Pres (psi) | Rate (BPM) | PROP (PPG) | SI Vol (McGal) | Efficiency (%) | Loss (BPM) | Height (ft) | W-Avg (in) |
| 0.3 | 14 | 243 | 4.80 | 0.0 | 0.1 | 0.08 | 4.3 | 30 | 0.01 |
| 0.4 | 17 | 262 | 4.80 | 0.0 | 0.1 | 0.10 | 4.2 | 30 | 0.01 |
| 0.5 | 20 | 285 | 4.80 | 0.0 | 0.1 | 0.09 | 4.5 | 30 | 0.01 |
| 0.6 | 23 | 298 | 4.80 | 0.0 | 0.1 | 0.08 | 4.6 | 30 | 0.01 |
| 0.7 | 26 | 305 | 4.80 | 0.0 | 0.2 | 0.07 | 4.6 | 30 | 0.01 |
| 0.9 | 29 | 313 | 4.80 | 0.0 | 0.2 | 0.07 | 4.6 | 30 | 0.01 |
| 1.1 | 32 | 320 | 4.80 | 0.0 | 0.2 | 0.06 | 4.7 | 31 | 0.01 |
| 1.3 | 35 | 325 | 4.80 | 0.0 | 0.3 | 0.06 | 4.6 | 31 | 0.01 |
| 1.5 | 38 | 330 | 4.80 | 0.0 | 0.3 | 0.06 | 4.6 | 32 | 0.01 |
| 1.7 | 41 | 335 | 4.80 | 0.0 | 0.3 | 0.06 | 4.6 | 32 | 0.01 |
| 1.9 | 44 | 340 | 4.80 | 0.0 | 0.4 | 0.05 | 4.6 | 32 | 0.01 |
| 2.2 | 47 | 344 | 4.80 | 0.0 | 0.4 | 0.05 | 4.6 | 32 | 0.01 |
| 2.4 | 50 | 349 | 4.80 | 0.0 | 0.5 | 0.05 | 4.7 | 33 | 0.01 |
| 2.7 | 53 | 353 | 4.80 | 0.0 | 0.6 | 0.05 | 4.7 | 33 | 0.01 |
| 3.0 | 56 | 357 | 4.80 | 0.0 | 0.6 | 0.05 | 4.7 | 33 | 0.01 |
| 3.4 | 59 | 362 | 4.80 | 0.0 | 0.7 | 0.05 | 4.6 | 33 | 0.01 |
| 3.7 | 62 | 363 | 4.80 | 0.0 | 0.8 | 0.05 | 4.7 | 34 | 0.01 |
| 4.1 | 65 | 367 | 4.80 | 0.0 | 0.8 | 0.05 | 4.7 | 34 | 0.01 |
| 4.4 | 68 | 372 | 4.80 | 0.0 | 0.9 | 0.04 | 4.7 | 34 | 0.01 |
| 4.8 | 71 | 375 | 4.80 | 0.0 | 1.0 | 0.04 | 4.7 | 34 | 0.01 |
| 5.3 | 74 | 376 | 4.80 | 0.0 | 1.1 | 0.04 | 4.7 | 34 | 0.01 |
| 5.8 | 77 | 381 | 4.80 | 0.0 | 1.2 | 0.04 | 4.7 | 34 | 0.01 |
| 6.3 | 80 | 383 | 4.80 | 0.0 | 1.3 | 0.04 | 4.7 | 34 | 0.01 |
| 6.8 | 83 | 385 | 4.80 | 0.0 | 1.4 | 0.04 | 4.7 | 34 | 0.02 |
| 7.4 | 86 | 392 | 4.80 | 0.0 | 1.5 | 0.04 | 4.7 | 34 | 0.02 |
| 7.8 | 88 | 393 | 4.80 | 0.0 | 1.6 | 0.04 | 4.6 | 34 | 0.02 |
| 8.0 | 91 | 1249 | 8.00 | 0.0 | 1.6 | 0.05 | 5.8 | 51 | 0.02 |
| 8.9 | 94 | 1387 | 8.00 | 0.0 | 1.9 | 0.08 | 5.7 | 77 | 0.02 |
| 9.5 | 94 | 815 | 8.00 | 0.0 | 2.1 | 0.09 | 6.8 | 91 | 0.02 |
| 11.1 | 94 | 1162 | 13.75 | 0.0 | 3.1 | 0.13 | 10.5 | 136 | 0.03 |
| 12.1 | 95 | 1023 | 14.84 | 0.0 | 3.7 | 0.17 | 9.3 | 140 | 0.05 |
| 12.3 | 95 | 1012 | 15.25 | 0.7 | 3.8 | 0.17 | 15.1 | 141 | 0.05 |
| 12.4 | 98 | 999 | 15.25 | 0.7 | 3.8 | 0.17 | 8.9 | 141 | 0.05 |
| 12.6 | 101 | 1008 | 15.25 | 0.7 | 4.0 | 0.17 | 11.1 | 141 | 0.05 |
| 12.8 | 104 | 973 | 15.25 | 0.7 | 4.2 | 0.17 | 12.3 | 141 | 0.05 |
| 13.0 | 107 | 976 | 15.25 | 0.7 | 4.3 | 0.18 | 11.1 | 141 | 0.05 |
| 13.3 | 110 | 979 | 15.21 | 1.3 | 4.4 | 0.18 | 12.0 | 141 | 0.05 |
| 13.5 | 113 | 981 | 15.21 | 1.3 | 4.6 | 0.18 | 11.8 | 141 | 0.05 |
| 13.8 | 116 | 991 | 15.21 | 1.3 | 4.8 | 0.18 | 11.3 | 141 | 0.05 |
| 14.1 | 119 | 1004 | 15.40 | 2.4 | 5.0 | 0.19 | 11.4 | 141 | 0.06 |
| Bridge Stage 5 at 14 min, at 89.2 (ft), Avg Dia/W 0.03/0.03 in ScreenOut in Stage 5 at 14 min, at 92.2 (ft), Avg Dia/W 0.03/0.04 in | | | | | | | | | |
| 15.0 | 119 | 1227 | 15.40 | 2.4 | 5.6 | 0.21 | 8.8 | 141 | 0.08 |
| Bridge Stage 5 at 15 min, at 100.9 (ft), Avg Dia/W 0.03/0.05 in | | | | | | | | | |
| 16.0 | 119 | 1516 | 15.46 | 3.7 | 6.2 | 0.24 | 7.7 | 141 | 0.10 |
| 16.9 | 119 | 1831 | 15.29 | 5.0 | 6.8 | 0.27 | 7.0 | 141 | 0.12 |
| 17.9 | 119 | 2167 | 15.23 | 6.3 | 7.4 | 0.29 | 6.5 | 141 | 0.14 |
| 18.8 | 119 | 2577 | 16.67 | 7.7 | 8.1 | 0.32 | 6.1 | 141 | 0.17 |
| 19.9 | 119 | 2319 | 15.21 | 0.0 | 8.1 | 0.29 | 5.9 | 141 | 0.16 |
| 21.0 | 119 | 2061 | 0.00 | 0.0 | 8.1 | 0.26 | 5.5 | 141 | 0.14 |
| 22.3 | 119 | 1804 | 0.00 | 0.0 | 8.1 | 0.23 | 5.2 | 141 | 0.13 |
| 23.6 | 119 | 1546 | 0.00 | 0.0 | 8.1 | 0.20 | 5.0 | 141 | 0.12 |

| | | | | | | | | | |
|------|-----|------|------|-----|-----|------|-----|-----|------|
| 25.0 | 119 | 1288 | 0.00 | 0.0 | 8.1 | 0.17 | 4.8 | 141 | 0.10 |
| 26.4 | 119 | 1031 | 0.00 | 0.0 | 8.1 | 0.14 | 4.6 | 141 | 0.10 |
| 27.5 | 119 | 773 | 0.00 | 0.0 | 8.1 | 0.14 | 4.4 | 141 | 0.09 |

| GEOMETRY SUMMARY * At End of Pumping Schedule SANTOS - EM#37 (190/230/250) POST-FRAC EVALUATION | | | | | | | | | |
|--|-------|-------|-------|---------|-------|------------|------|------|----------------|
| Dstnhd | Press | W-Avg | Q | Sh-Rate | Total | Right (ft) | Bank | Prop | Fraction (PSF) |
| (ft) | (psi) | (in) | (BPM) | (1/sec) | Up | Dn | Up | Dn | |
| 5 | 2576 | 0.23 | 8.3 | 40 | 14.1 | 4.3 | 68 | 124 | 0.00 |
| 12 | 2575 | 0.21 | 7.2 | 43 | 12.8 | 3.8 | 60 | 105 | 0.00 |
| 15 | 2574 | 0.21 | 6.9 | 42 | 12.5 | 3.7 | 58 | 105 | 0.01 |
| 18 | 2572 | 0.21 | 6.6 | 42 | 12.3 | 3.6 | 57 | 103 | 0.00 |
| 21 | 2571 | 0.21 | 6.4 | 42 | 12.1 | 3.5 | 56 | 100 | 0.00 |
| 24 | 2569 | 0.21 | 6.1 | 41 | 11.8 | 3.4 | 54 | 98 | 0.00 |
| 27 | 2568 | 0.21 | 5.8 | 41 | 11.6 | 3.3 | 53 | 95 | 0.00 |
| 30 | 2567 | 0.21 | 5.6 | 40 | 11.3 | 3.2 | 51 | 93 | 0.00 |
| 33 | 2565 | 0.20 | 5.3 | 40 | 11.2 | 3.1 | 50 | 91 | 0.00 |
| 36 | 2564 | 0.20 | 5.1 | 39 | 11.0 | 3.0 | 50 | 90 | 0.00 |
| 39 | 2562 | 0.20 | 4.9 | 38 | 10.8 | 3.0 | 49 | 88 | 0.00 |
| 42 | 2561 | 0.20 | 4.6 | 37 | 10.7 | 2.9 | 48 | 87 | 0.00 |
| 45 | 2560 | 0.20 | 4.4 | 36 | 10.5 | 2.8 | 47 | 85 | 0.00 |
| 48 | 2558 | 0.20 | 4.2 | 35 | 10.3 | 2.7 | 46 | 84 | 0.00 |
| 51 | 2557 | 0.20 | 3.9 | 35 | 10.1 | 2.6 | 45 | 82 | 0.00 |
| 54 | 2556 | 0.20 | 3.7 | 34 | 9.9 | 2.5 | 43 | 80 | 0.00 |
| 57 | 2554 | 0.19 | 3.5 | 33 | 9.6 | 2.4 | 42 | 79 | 0.00 |
| 60 | 2553 | 0.19 | 3.2 | 32 | 9.5 | 2.3 | 41 | 77 | 0.00 |
| 63 | 2551 | 0.19 | 3.0 | 31 | 9.3 | 2.3 | 40 | 76 | 0.00 |
| 66 | 2550 | 0.19 | 2.8 | 29 | 9.1 | 2.2 | 39 | 74 | 0.00 |
| 69 | 2549 | 0.19 | 2.6 | 28 | 8.9 | 2.1 | 39 | 73 | 0.00 |
| 72 | 2547 | 0.19 | 2.4 | 27 | 8.8 | 2.0 | 38 | 71 | 0.00 |
| 75 | 2546 | 0.19 | 2.2 | 25 | 8.6 | 1.9 | 37 | 70 | 0.00 |
| 78 | 2545 | 0.18 | 1.9 | 24 | 8.3 | 1.8 | 36 | 68 | 0.00 |
| 81 | 2543 | 0.18 | 1.7 | 22 | 8.1 | 1.6 | 35 | 66 | 0.00 |
| 84 | 2542 | 0.18 | 1.5 | 21 | 7.9 | 1.5 | 34 | 64 | 0.00 |
| 87 | 2541 | 0.18 | 1.3 | 19 | 7.7 | 1.4 | 33 | 63 | 0.00 |
| 89 | 2540 | 0.18 | 1.2 | 17 | 7.6 | 1.3 | 32 | 62 | 0.00 |
| 92 | 2539 | 0.17 | 1.0 | 16 | 7.4 | 1.3 | 31 | 60 | 0.00 |
| 94 | 2538 | 0.15 | 0.8 | 19 | 6.5 | 1.2 | 23 | 52 | 0.00 |
| 94 | 2538 | 0.15 | 0.8 | 19 | 6.4 | 1.2 | 23 | 52 | 0.00 |
| 95 | 2537 | 0.15 | 0.7 | 19 | 6.3 | 1.1 | 22 | 51 | 0.00 |
| 97 | 2536 | 0.14 | 0.7 | 19 | 6.0 | 1.0 | 20 | 47 | 0.00 |
| 100 | 2532 | 0.13 | 0.5 | 21 | 4.8 | 5 | 13 | 35 | 0.00 |
| 103 | 2517 | 0.12 | 0.3 | 28 | 2 | 0 | 31 | 37 | 0.85 |
| 106 | 2507 | 0.13 | 0.3 | 20 | 30 | 0 | 30 | 1.00 | 1.38 |
| 109 | 532 | 0.03 | 0.2 | 1486 | 26 | 0 | 26 | 1.00 | 0.28 |
| 112 | 452 | 0.02 | 0.6 | 2255 | 18 | 0 | 18 | 1.00 | 0.20 |
| 115 | 351 | 0.02 | 0.4 | 4124 | 16 | 0 | 16 | 1.00 | 0.22 |
| 118 | 215 | 0.03 | 0.2 | 2285 | 15 | 0 | 15 | 1.00 | 0.29 |

| FLUID SUMMARY * At End of Pumping Schedule | | | | | | | | | |
|---|------|----------|---------|-----|-----------------------------|---------------|--------------|--------------|---------------------|
| SANTOS - EM#37 (190/230/250) POST-FRAC EVALUATION | | | | | | | | | |
| Stage No | Gone | Fluid ID | Prop ID | Pos | Concentration In Now Design | F1 Vol (MGal) | Ex Tim (min) | Temp (deg_F) | Visc (cp) Fall Frac |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.1 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.2 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.1 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.1 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.2 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.2 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.2 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.3 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.3 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.4 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.4 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.5 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.6 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.6 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.7 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.8 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.8 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 0.9 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 1.0 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 1.1 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 1.2 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 1.3 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 1.4 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 1.5 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 1.6 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 1.6 | 143 21.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 1.6 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 1.7 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 1.8 | 143 1.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 1.9 | 143 2.400 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 1.9 | 143 13.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 2.1 | 143 13.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 2.1 | 143 13.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 2.7 | 143 16.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 3.1 | 143 15.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.0 | 0.0 | 3.4 | 143 20.000 |
| 1 | 1 | 2 | 1 | 1 | 119 | 0.7 | 45.3 | 0.0 | 3.7 31.000 |
| 1 | 1 | 2 | 1 | 1 | 107 | 0.7 | 45.3 | 0.0 | 3.8 569.000 |
| 1 | 1 | 2 | 1 | 1 | 107 | 0.7 | 45.3 | 0.0 | 3.8 208.000 |
| 1 | 1 | 2 | 1 | 1 | 107 | 0.7 | 45.3 | 0.0 | 3.5 591.000 |
| 1 | 1 | 2 | 1 | 1 | 107 | 0.7 | 45.3 | 0.0 | 3.5 311.000 |
| 1 | 1 | 2 | 1 | 1 | 105 | 0.7 | 39.1 | 0.3 | 4.0 639.000 |
| 1 | 1 | 2 | 1 | 1 | 101 | 0.7 | 7.6 | 0.8 | 4.7 595.000 |
| 1 | 1 | 2 | 1 | 1 | 100 | 1.3 | 12.2 | 1.0 | 4.3 642.000 |
| 1 | 1 | 2 | 1 | 1 | 98 | 1.3 | 8.3 | 1.3 | 4.7 550.000 |
| 1 | 1 | 2 | 1 | 1 | 94 | 1.3 | 5.8 | 1.8 | 4.4 614.000 |
| 1 | 1 | 2 | 1 | 1 | 91 | 1.3 | 4.5 | 2.2 | 4.4 554.000 |
| 1 | 1 | 2 | 1 | 1 | 90 | 2.4 | 8.4 | 2.4 | 4.7 505.000 |
| 1 | 1 | 2 | 1 | 1 | 87 | 2.4 | 7.3 | 2.7 | 4.9 639.000 |
| 1 | 1 | 2 | 1 | 1 | 82 | 2.4 | 6.0 | 3.2 | 5.1 505.000 |
| 1 | 1 | 2 | 1 | 1 | 74 | 3.7 | 8.6 | 3.7 | 5.4 478.000 |
| 1 | 1 | 2 | 1 | 1 | 68 | 3.7 | 6.6 | 4.6 | 5.5 447.000 |
| 1 | 1 | 2 | 1 | 1 | 59 | 5.0 | 8.6 | 4.9 | 5.9 423.000 |
| 1 | 1 | 2 | 1 | 1 | 49 | 5.0 | 7.1 | 5.9 | 6.1 423.000 |
| 1 | 1 | 2 | 1 | 1 | 40 | 6.3 | 8.8 | 6.1 | 6.4 408.000 |
| 1 | 1 | 2 | 1 | 1 | 31 | 6.3 | 7.7 | 6.9 | 6.6 392.000 |

| PROPPANT SUMMARY * At End of Pumping Schedule SANTOS - EM#37 (190/230/250) POST-FRAC EVALUATION | | | |
|--|-------------|--|--|
| Lb/Sq-ft Lost to Embedment 0.200 | | | |
| Distance (ft) | Kfw (md-ft) | Prop Concentration(Total 1b/sq foot) Prop ID--> 1 | |
| 5.3 | 1738 | 1.00 | |
| 12.0 | 1853 | 1.00 | |
| 15.0 | 1802 | 1.00 | |
| 18.0 | 1833 | 1.00 | |
| 21.0 | 1851 | 1.00 | |
| 24.0 | 1851 | 1.00 | |
| 27.0 | 1733 | 1.00 | |
| 30.0 | 1555 | 0.90 | |
| 33.0 | 1580 | 0.90 | |
| 36.0 | 1741 | 1.00 | |
| 39.0 | 1732 | 1.00 | |
| 42.0 | 1724 | 1.00 | |
| 45.0 | 1611 | 0.90 | |
| 48.0 | 1380 | 0.80 | |
| 51.0 | 1437 | 0.80 | |
| 54.0 | 1632 | 0.90 | |
| 57.0 | 1622 | 0.90 | |
| 60.0 | 1615 | 0.90 | |
| 63.0 | 1605 | 0.90 | |
| 66.0 | 1375 | 0.80 | |
| 69.0 | 1333 | 0.80 | |
| 72.0 | 1532 | 0.90 | |
| 75.0 | 1524 | 0.90 | |
| 78.0 | 1325 | 0.80 | |
| 81.0 | 1014 | 0.70 | |
| 84.0 | 1056 | 0.70 | |
| 86.7 | 1229 | 0.80 | |
| 89.4 | 1086 | 0.70 | |
| 92.4 | 719 | 0.50 | |
| 94.0 | 737 | 0.50 | |
| 94.3 | 744 | 0.50 | |
| 94.9 | 742 | 0.50 | |
| 96.8 | 991 | 0.60 | |
| 99.8 | 1189 | 0.70 | |
| 102.8 | 1454 | 0.90 | |
| 105.8 | 2642 | 1.40 | |
| 108.8 | 169 | 0.30 | |
| 111.8 | 7 | 0.20 | |
| 114.8 | 44 | 0.20 | |
| 117.8 | 209 | 0.30 | |

Average Conductivity (md-ft) 1389

| PROPPANT SUMMARY * At Fracture Closure SANTOS - EM#37 (190/230/250) POST-FRAC EVALUATION | | | |
|---|-------------|--|--|
| Lb/Sq-Ft Lost to Embedment 0.200 | | | |
| Distance (ft) | Kfw (md-ft) | Prop Concentration(Total 1b/sq foot) Prop ID--> 1 | |
| 5.3 | 1073 | 0.70 | |
| 12.0 | 1332 | 0.80 | |
| 15.0 | 1337 | 0.80 | |
| 18.0 | 1349 | 0.80 | |
| 21.0 | 1356 | 0.80 | |
| 24.0 | 1438 | 0.80 | |
| 27.0 | 1555 | 0.90 | |
| 30.0 | 1565 | 0.90 | |
| 33.0 | 1569 | 0.90 | |
| 36.0 | 1566 | 0.90 | |
| 39.0 | 1401 | 0.80 | |
| 42.0 | 1396 | 0.80 | |
| 45.0 | 1747 | 0.90 | |
| 48.0 | 2018 | 1.10 | |
| 51.0 | 1671 | 0.90 | |
| 54.0 | 1674 | 0.90 | |
| 57.0 | 1637 | 0.90 | |
| 60.0 | 1513 | 0.80 | |
| 63.0 | 1517 | 0.90 | |
| 66.0 | 2014 | 1.10 | |
| 69.0 | 2011 | 1.10 | |
| 72.0 | 2011 | 1.10 | |
| 75.0 | 2014 | 1.10 | |
| 78.0 | 1855 | 1.00 | |
| 81.0 | 2393 | 1.20 | |
| 84.0 | 2153 | 1.10 | |
| 86.7 | 2158 | 1.10 | |
| 89.4 | 1725 | 0.90 | |
| 92.4 | 2330 | 1.20 | |
| 94.0 | 2584 | 1.30 | |
| 94.3 | 2082 | 1.10 | |
| 94.9 | 2468 | 1.30 | |
| 96.8 | 2716 | 1.40 | |
| 99.8 | 3235 | 1.60 | |
| 102.8 | 2473 | 1.30 | |
| 105.8 | 2351 | 1.20 | |
| 108.8 | 177 | 0.30 | |
| 111.8 | 8 | 0.20 | |
| 114.8 | 46 | 0.20 | |
| 117.8 | 219 | 0.30 | |

Average Conductivity (md-ft) 1608

Frac Summary * SANTOS - EM#37 (190/230/250) POST-FRAC EVALUATION
Filename: EM37PF1.FRK ; Feb 12, 96

| | | | | | |
|--|--|--|--|--|--|
| StimPlan 2.50 (TM) • NSI Technologies, Tulsa, OK Licensed To: Internal Use - NSI Technologies | | | | | |
| | | | | | |

| Design Data | | | | | |
|--|-----------------|-------------------|---------------|---------------------------|---------------------|
| FLUID LOSS LAYERS: | Top (ft) | Bottom (ft) | Thick (ft) | Loss Coef. (ft/sqrt(min)) | Sput (Gal/100 ft^2) |
| 4610.0 | 4643.0 | 33.0 | 0.01000 | 0.50 | |
| 4643.0 | 4690.0 | 47.0 | 0.00010 | 0.00 | |
| 4690.0 | 4745.0 | 55.0 | 0.00340 | 0.25 | |
| FORMATION: Modulus (e6 psi) | 155.0 | 0.00010 | 0.00 | 6.63 | |
| Perforated Height (ft) | 30.0 | | | | |
| Permeability (md) | 10.000 | 143 | | | |
| TEMPERATURE: Reservoir Pressure (psi) | 1770.0 | | | | |
| PRESSURE: Closure Pressure (psi) | 3300.0 | | | | |
| DEPTH: Wall Depth (ft) | 4690.0 | | | | |
| FORMATION LAYER DATA - Multi-Layer Height Growth -Stress (psi) - Stress (psi) -- Gradient Modulus Toughness | | | | | |
| TOP Botm | Thick | Top Botm (psi/ft) | Botm (psi/in) | (e6 psi) | (psi/in) |
| 4610.0 | 4643.0 | 33.0 | 2100.0 | 0.000 | 5.50 |
| 4643.0 | 4675.0 | 32.0 | 4500.0 | 0.000 | 8.00 |
| 4675.0 | 4690.0 | 15.0 | 4500.0 | 0.000 | 8.00 |
| 4690.0 | 4705.0 | 15.0 | 3300.0 | 0.000 | 6.50 |
| 4705.0 | 4709.0 | 4.0 | 4000.0 | 0.000 | 7.50 |
| 4709.0 | 4720.0 | 11.0 | 3400.0 | 0.000 | 6.50 |
| 4720.0 | 4732.0 | 12.0 | 4050.0 | 0.000 | 7.00 |
| 4732.0 | 4745.0 | 13.0 | 3500.0 | 0.000 | 6.50 |
| 4745.0 | | | 4500.0 | 0.000 | 7.50 |
| Fluid Pressure Gradient (psi/ft) | 3.0 | | | | |
| Initial Fracture Top (ft) | 1.0 | | | | |
| Initial Fracture Bottom (ft) | 0.450 | | | | |
| PROGRAM CONTROL | Step Size (ft) | 3.0 | | | |
| | Time Step (min) | 1.0 | | | |

| Pumping Schedule ** | | | | | |
|---------------------|---------------|------------|------------|-----------------|-----------|
| SI Vol (MGal) | Fl Vol (MGal) | Conc (PPM) | Rate (BPM) | Fluid Type | Prop Type |
| 0.53 | 0.53 | 0.0 | 8.00 | 1 | 1 |
| 0.57 | 0.57 | 0.0 | 13.75 | 1 | 1 |
| 0.72 | 0.72 | 0.0 | 14.84 | 1 | 1 |
| 0.86 | 0.83 | 0.7 | 15.25 | 1 | 1 |
| 0.49 | 0.46 | 1.3 | 15.21 | 1 | 1 |
| 0.49 | 0.44 | 2.4 | 15.40 | 1 | 2.2 |
| 0.48 | 0.41 | 3.7 | 15.46 | 1 | 3.8 |
| 0.70 | 0.57 | 5.0 | 15.29 | 1 | 6.6 |
| 0.63 | 0.49 | 6.3 | 15.23 | 1 | 9.7 |
| 0.46 | 0.34 | 7.7 | 16.67 | 1 | 12.3 |
| 0.36 | 0.26 | 8.5 | 16.10 | 1 | 14.5 |
| 0.24 | 0.18 | 7.4 | 16.10 | 1 | 15.8 |
| Total Slurry ... | 6.5 | | | Total Fluid ... | 5.8 |
| Total Proppant ... | 15.8 | | | Avg. Conc ... | 2.7 |
| Total Pump Time | 10.9 | min | | | |

| | | | | | | | | | | |
|-------------------|-------------------|--|--|--|--|--|--|--|--|--|
| Proppant ID No. 1 | 20- 40 CARBO-LITE | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |

| | |
|--|--|
| Calculated Results from 3-D Simulator STIMPLAN (TM), NSI, Tulsa,OK | Licensed To: Internal Use - NSI Technologies |
| | |
| | |
| | |
| | |

| | | | | | | | | | | |
|-------------------------------|---------------|--|--|--|--|--|--|--|--|--|
| Fluid ID No. 1 | BORAGEL_H3595 | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| Specific Gravity | | | | | | | | | | |
| Damage Factor | | | | | | | | | | |
| Proppant Stress (Mpsi) | | | | | | | | | | |
| KfW @ 2 #/sq ft (md-ft) 10500 | | | | | | | | | | |

TABLE A-7

Time History * NSI STIMPLAN 3-D Fracture Simulation
SANTOS - EM#37 (190/230/250) POST-FRAC EVALUATION

| Time (min) | Pen (ft) | Pres (psi) | Rate (BPM) | Prop (PPG) | SI Vol (MGal) | Efficiency (%) | Loss (BPM) | Hght (ft) | W-Avg (in) |
|--|----------|------------|------------|------------|---------------|----------------|------------|------------------------|------------|
| 0.1 | 14 | 790 | 8.00 | 0.0 | 0.0 | 0.34 | 5.3 | 31.0 | 0.02 |
| 0.2 | 17 | 791 | 8.00 | 0.0 | 0.1 | 0.36 | 5.0 | 36.0 | 0.03 |
| 0.2 | 20 | 853 | 8.00 | 0.0 | 0.1 | 0.34 | 5.6 | 43.0 | 0.03 |
| 0.3 | 23 | 859 | 8.00 | 0.0 | 0.1 | 0.32 | 6.2 | 50.0 | 0.03 |
| 0.4 | 26 | 888 | 8.00 | 0.0 | 0.1 | 0.29 | 6.3 | 56.0 | 0.02 |
| 0.5 | 29 | 892 | 8.00 | 0.0 | 0.2 | 0.27 | 6.6 | 63.0 | 0.02 |
| 0.7 | 32 | 882 | 8.00 | 0.0 | 0.2 | 0.24 | 6.9 | 69.0 | 0.02 |
| 1.0 | 35 | 870 | 8.00 | 0.0 | 0.3 | 0.22 | 6.6 | 76.0 | 0.02 |
| 1.2 | 38 | 866 | 8.00 | 0.0 | 0.4 | 0.23 | 6.2 | 83.0 | 0.03 |
| 1.6 | 41 | 884 | 8.00 | 0.0 | 0.5 | 0.23 | 6.0 | 90.0 | 0.03 |
| 1.7 | 44 | 924 | 13.75 | 0.0 | 0.6 | 0.25 | 7.7 | 93.0 | 0.03 |
| 1.8 | 47 | 956 | 13.75 | 0.0 | 0.7 | 0.27 | 8.0 | 95.0 | 0.04 |
| 1.9 | 50 | 967 | 13.75 | 0.0 | 0.7 | 0.28 | 8.5 | 98.0 | 0.04 |
| 2.0 | 53 | 968 | 13.75 | 0.0 | 0.8 | 0.28 | 9.2 | 100.0 | 0.04 |
| 2.2 | 56 | 966 | 13.75 | 0.0 | 0.9 | 0.29 | 9.3 | 102.0 | 0.04 |
| 2.3 | 59 | 967 | 13.75 | 0.0 | 1.0 | 0.29 | 9.4 | 105.0 | 0.04 |
| 2.5 | 62 | 969 | 13.75 | 0.0 | 1.0 | 0.29 | 9.4 | 106.0 | 0.04 |
| 2.6 | 65 | 973 | 13.75 | 0.0 | 1.1 | 0.29 | 9.5 | 108.0 | 0.04 |
| 2.8 | 68 | 986 | 14.84 | 0.0 | 1.2 | 0.30 | 9.8 | 110.0 | 0.05 |
| 3.0 | 71 | 991 | 14.84 | 0.0 | 1.3 | 0.30 | 9.9 | 112.0 | 0.05 |
| 3.1 | 74 | 996 | 14.84 | 0.0 | 1.4 | 0.30 | 10.1 | 113.0 | 0.05 |
| 3.3 | 77 | 1001 | 14.84 | 0.0 | 1.5 | 0.30 | 10.2 | 115.0 | 0.05 |
| 3.5 | 80 | 1002 | 14.84 | 0.0 | 1.6 | 0.30 | 10.3 | 117.0 | 0.05 |
| 3.6 | 83 | 1008 | 14.84 | 0.0 | 1.8 | 0.30 | 10.3 | 118.0 | 0.05 |
| 3.8 | 86 | 1010 | 14.84 | 0.0 | 1.9 | 0.30 | 10.3 | 120.0 | 0.05 |
| 4.0 | 89 | 1028 | 15.25 | 0.7 | 2.0 | 0.31 | 10.0 | 121.0 | 0.05 |
| 4.2 | 92 | 1028 | 15.21 | 1.3 | 2.1 | 0.31 | 10.1 | 123.0 | 0.05 |
| 4.4 | 95 | 1032 | 15.25 | 0.7 | 2.3 | 0.30 | 10.7 | 125.0 | 0.06 |
| 4.6 | 98 | 1033 | 15.25 | 0.7 | 2.4 | 0.30 | 10.6 | 126.0 | 0.06 |
| 4.8 | 101 | 1040 | 15.25 | 0.7 | 2.5 | 0.30 | 10.4 | 127.0 | 0.06 |
| 5.1 | 104 | 1047 | 15.25 | 0.7 | 2.7 | 0.30 | 10.9 | 129.0 | 0.06 |
| 5.3 | 107 | 1050 | 15.21 | 1.3 | 2.8 | 0.30 | 10.9 | 130.0 | 0.06 |
| 5.5 | 110 | 1052 | 15.21 | 1.3 | 3.0 | 0.30 | 10.8 | 132.0 | 0.06 |
| 5.8 | 113 | 1059 | 15.21 | 1.3 | 3.1 | 0.30 | 10.6 | 133.0 | 0.06 |
| Bridge Stage 4 at 6 min, at 92.7 (ft) | | | | | | | | Avg Dia/W 0.03/0.04 in | |
| 6.0 | 116 | 1065 | 15.21 | 1.3 | 3.3 | 0.30 | 10.8 | 135.0 | 0.06 |
| Bridge Stage 4 at 6 min, at 104.0 (ft) | | | | | | | | Avg Dia/W 0.03/0.03 in | |
| 6.8 | 119 | 1167 | 15.40 | 2.4 | 3.8 | 0.31 | 9.4 | 135.0 | 0.07 |
| Bridge Stage 4 at 7 min, at 100.5 (ft) | | | | | | | | Avg Dia/W 0.03/0.04 in | |
| Screenout in Stage 4 at Time = 6.8 min at 112.0 (ft) | | | | | | | | | |
| 7.6 | 119 | 1389 | 15.46 | 3.7 | 4.3 | 0.34 | 7.7 | 135.0 | 0.09 |
| Bridge Stage 4 at 8 min, at 107.6 (ft) | | | | | | | | Avg Dia/W 0.03/0.05 in | |
| 8.4 | 119 | 1642 | 15.29 | 5.0 | 4.8 | 0.36 | 6.9 | 135.0 | 0.11 |
| 9.2 | 119 | 1917 | 15.23 | 6.3 | 5.4 | 0.38 | 6.3 | 135.0 | 0.13 |
| 10.1 | 119 | 2208 | 15.23 | 6.3 | 5.9 | 0.40 | 5.9 | 135.0 | 0.15 |
| 10.9 | 119 | 2240 | 16.10 | 8.5 | 6.5 | 0.42 | 5.5 | 135.0 | 0.18 |
| 12.1 | 119 | 2286 | 0.00 | 0.0 | 6.5 | 0.38 | 5.2 | 135.0 | 0.16 |
| 13.6 | 119 | 2032 | 0.00 | 0.0 | 6.5 | 0.34 | 4.8 | 135.0 | 0.15 |
| 15.1 | 119 | 1778 | 0.00 | 0.0 | 6.5 | 0.30 | 4.5 | 135.0 | 0.13 |
| 16.7 | 119 | 1524 | 0.00 | 0.0 | 6.5 | 0.26 | 4.2 | 135.0 | 0.11 |
| 18.4 | 119 | 1270 | 0.00 | 0.0 | 6.5 | 0.22 | 4.0 | 135.0 | 0.09 |
| 20.1 | 119 | 1016 | 0.00 | 0.0 | 6.5 | 0.18 | 3.7 | 135.0 | 0.09 |
| 21.4 | 119 | 762 | 0.00 | 0.0 | 6.5 | 0.17 | 3.6 | 135.0 | 0.09 |

GEOMETRY SUMMARY * At End of Pumping Schedule
SANTOS - EM#37 (190/230/250) POST-FRAC EVALUATION

| Distance (ft) | Press (psi) | W-Avg (in) | Q (BPM) | Sh-Rate (1/sec) | Total Up | Height (ft) | Dn | Bank | Prop Fraction (PSF) |
|---------------|-------------|------------|---------|-----------------|----------|-------------|----|------|---------------------|
| 5 | 2539 | 0.22 | 8.0 | 43 | 135 | 4.1 | 64 | 116 | 0.00 |
| 12 | 2537 | 0.21 | 7.0 | 40 | 131 | 3.9 | 62 | 111 | 0.00 |
| 15 | 2535 | 0.21 | 6.8 | 40 | 129 | 3.8 | 60 | 109 | 0.00 |
| 18 | 2534 | 0.21 | 6.5 | 39 | 127 | 3.8 | 59 | 107 | 0.00 |
| 21 | 2532 | 0.21 | 6.3 | 38 | 126 | 3.7 | 57 | 106 | 0.00 |
| 24 | 2530 | 0.21 | 6.0 | 38 | 124 | 3.6 | 57 | 104 | 0.00 |
| 27 | 2528 | 0.21 | 5.8 | 37 | 122 | 3.6 | 56 | 102 | 0.00 |
| 30 | 2526 | 0.21 | 5.5 | 36 | 120 | 3.5 | 55 | 100 | 0.00 |
| 33 | 2525 | 0.21 | 5.3 | 36 | 119 | 3.4 | 54 | 98 | 0.00 |
| 36 | 2523 | 0.21 | 5.0 | 35 | 117 | 3.3 | 53 | 96 | 0.00 |
| 39 | 2521 | 0.21 | 4.8 | 34 | 115 | 3.2 | 52 | 94 | 0.00 |
| 43 | 2519 | 0.20 | 4.5 | 33 | 113 | 3.2 | 51 | 92 | 0.00 |
| 46 | 2517 | 0.20 | 4.2 | 32 | 111 | 3.1 | 50 | 90 | 0.00 |
| 49 | 2516 | 0.20 | 4.0 | 31 | 109 | 3.0 | 49 | 89 | 0.00 |
| 52 | 2514 | 0.20 | 3.8 | 30 | 107 | 2.9 | 48 | 87 | 0.00 |
| 55 | 2512 | 0.20 | 3.5 | 29 | 105 | 2.8 | 47 | 86 | 0.00 |
| 58 | 2511 | 0.20 | 3.3 | 28 | 103 | 2.7 | 46 | 84 | 0.00 |
| 61 | 2509 | 0.20 | 3.1 | 27 | 101 | 2.6 | 45 | 82 | 0.00 |
| 64 | 2507 | 0.20 | 2.9 | 26 | 99 | 2.5 | 44 | 81 | 0.00 |
| 67 | 2506 | 0.19 | 2.7 | 25 | 97 | 2.4 | 42 | 79 | 0.00 |
| 70 | 2504 | 0.19 | 2.4 | 24 | 95 | 2.3 | 41 | 77 | 0.00 |
| 73 | 2503 | 0.19 | 2.2 | 23 | 93 | 2.2 | 40 | 75 | 0.00 |
| 76 | 2501 | 0.19 | 2.0 | 22 | 89 | 2.1 | 39 | 73 | 0.00 |
| 79 | 2499 | 0.19 | 1.8 | 21 | 87 | 1.9 | 37 | 71 | 0.00 |
| 82 | 2498 | 0.18 | 1.6 | 20 | 84 | 1.8 | 36 | 69 | 0.00 |
| 85 | 2496 | 0.18 | 1.4 | 19 | 82 | 1.7 | 35 | 67 | 0.00 |
| 88 | 2495 | 0.18 | 1.3 | 18 | 77 | 1.7 | 33 | 63 | 0.00 |
| 91 | 2493 | 0.17 | 1.1 | 18 | 73 | 1.3 | 30 | 60 | 0.00 |
| 94 | 2491 | 0.15 | 0.9 | 19 | 69 | 1.3 | 26 | 57 | 0.00 |
| 97 | 2489 | 0.15 | 0.7 | 19 | 63 | 1.1 | 22 | 51 | 0.00 |
| 100 | 2487 | 0.14 | 0.6 | 19 | 55 | 8 | 17 | 42 | 0.00 |
| 103 | 2484 | 0.13 | 0.4 | 18 | 49 | 6 | 13 | 36 | 0.00 |
| 106 | 2479 | 0.12 | 0.3 | 19 | 40 | 4 | 6 | 31 | 0.00 |
| 109 | 2463 | 0.12 | 0.2 | 19 | 32 | 2 | 0 | 31 | 0.07 |
| 112 | 2451 | 0.12 | 0.2 | 13 | 30 | 0 | 0 | 30 | 1.00 |
| 115 | 369 | 0.02 | 0.1 | 1470 | 24 | 0 | 0 | 24 | 1.00 |
| 118 | 207 | 0.04 | 0.2 | 644 | 22 | 0 | 0 | 22 | 1.00 |

GEOMETRY SUMMARY * At End of Pumping Schedule
SANTOS - EM#37 (190/230/250) POST-FRAC EVALUATION

FLUID SUMMARY * At End of Pumping Schedule
 SANTOS - EM#37 (190/230/250) POST-FRAC EVALUATION

| Stage No | Gone | Fluid ID | Prop ID | Pos (ft) | Concentration In Now Design | Fl Vol (MGal) | Ex Tim (min) | Temp (deg F) | Visc (cp) | Fall Frac | |
|----------|------|----------|---------|----------|-----------------------------|---------------|--------------|--------------|-----------|-----------|----------|
| 1 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.0 | 0.2 | 143 | 29 0.00 | |
| 1 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.1 | 0.3 | 143 | 33 0.00 | |
| 1 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.1 | 0.4 | 143 | 33 0.00 | |
| 1 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.1 | 0.4 | 143 | 35 0.00 | |
| 1 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.1 | 0.2 | 143 | 36 0.00 | |
| 1 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.2 | 0.5 | 143 | 34 0.00 | |
| 1 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.2 | 0.6 | 143 | 33 0.00 | |
| 1 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.3 | 0.7 | 143 | 29 0.00 | |
| 1 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.4 | 0.6 | 143 | 32 0.00 | |
| 1 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.5 | 0.6 | 143 | 32 0.00 | |
| 1 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.5 | 0.6 | 143 | 32 0.00 | |
| 2 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.6 | 0.7 | 143 | 33 0.00 | |
| 2 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.7 | 0.7 | 143 | 33 0.00 | |
| 2 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.7 | 0.9 | 143 | 33 0.00 | |
| 2 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.8 | 0.9 | 143 | 34 0.00 | |
| 2 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 0.9 | 1.0 | 143 | 34 0.00 | |
| 2 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.0 | 1.2 | 143 | 34 0.00 | |
| 2 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.0 | 1.2 | 143 | 34 0.00 | |
| 2 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.0 | 1.2 | 143 | 34 0.00 | |
| 2 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.1 | 1.3 | 143 | 33 0.00 | |
| 3 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.1 | 1.3 | 143 | 34 0.00 | |
| 3 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.2 | 1.3 | 143 | 34 0.00 | |
| 3 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.3 | 1.4 | 143 | 35 0.00 | |
| 3 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.4 | 1.4 | 143 | 35 0.00 | |
| 3 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.5 | 1.6 | 143 | 35 0.00 | |
| 3 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.6 | 1.7 | 143 | 37 0.00 | |
| 3 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.8 | 1.8 | 143 | 47 0.00 | |
| 3 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.8 | 2.3 | 143 | 47 0.00 | |
| 4 | 1 | 1 | 1 | 119 | 0.7 | 45.3 | 0.0 | 1.9 | 2.1 | 143 | 47 0.00 |
| 4 | 1 | 1 | 1 | 119 | 0.7 | 45.3 | 0.0 | 2.0 | 1.9 | 143 | 64 0.00 |
| 4 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.5 | 1.6 | 143 | 35 0.00 | |
| 4 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.6 | 1.7 | 143 | 37 0.00 | |
| 4 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.8 | 1.8 | 143 | 47 0.00 | |
| 4 | 1 | 1 | 1 | 119 | 0.0 | 0.0 | 1.8 | 2.3 | 143 | 47 0.00 | |
| 4 | 1 | 1 | 1 | 119 | 0.7 | 45.3 | 0.0 | 2.0 | 2.1 | 143 | 776 0.00 |
| 4 | 1 | 1 | 1 | 119 | 0.7 | 45.3 | 0.0 | 2.7 | 4.8 | 143 | 802 0.00 |
| 4 | 1 | 1 | 1 | 113 | 0.7 | 45.3 | 0.0 | 2.1 | 3.3 | 143 | 419 0.00 |
| 4 | 1 | 1 | 1 | 113 | 0.7 | 45.3 | 0.0 | 2.3 | 4.7 | 143 | 749 0.00 |
| 4 | 1 | 1 | 1 | 111 | 0.7 | 22.5 | 0.4 | 2.4 | 5.3 | 143 | 831 0.00 |
| 4 | 0 | 1 | 1 | 107 | 0.7 | 6.8 | 0.8 | 2.5 | 5.1 | 143 | 802 0.00 |
| 4 | 0 | 1 | 1 | 104 | 0.7 | 4.3 | 1.2 | 2.7 | 4.8 | 143 | 802 0.00 |
| 5 | 0 | 1 | 1 | 102 | 1.3 | 8.0 | 1.4 | 2.7 | 4.8 | 143 | 811 0.00 |
| 5 | 0 | 1 | 1 | 100 | 1.3 | 6.3 | 1.7 | 2.8 | 4.6 | 143 | 783 0.00 |
| 5 | 0 | 1 | 1 | 96 | 1.3 | 6.7 | 2.1 | 2.9 | 4.1 | 143 | 785 0.00 |
| 5 | 0 | 1 | 1 | 92 | 1.3 | 3.8 | 2.6 | 3.1 | 4.1 | 143 | 802 0.00 |
| 5 | 0 | 1 | 1 | 90 | 1.3 | 3.3 | 2.9 | 3.1 | 4.1 | 143 | 811 0.00 |
| 6 | 0 | 1 | 1 | 87 | 2.4 | 6.3 | 3.1 | 3.2 | 3.3 | 143 | 808 0.00 |
| 6 | 0 | 1 | 1 | 81 | 2.4 | 5.2 | 3.7 | 3.5 | 3.3 | 143 | 754 0.00 |
| 7 | 0 | 1 | 1 | 75 | 3.7 | 7.8 | 4.0 | 3.6 | 2.5 | 143 | 710 0.00 |
| 7 | 0 | 1 | 1 | 69 | 3.7 | 6.5 | 4.7 | 3.9 | 2.5 | 143 | 672 0.00 |
| 8 | 0 | 1 | 1 | 61 | 5.0 | 8.6 | 5.0 | 4.1 | 1.7 | 143 | 637 0.00 |
| 8 | 0 | 1 | 1 | 52 | 5.0 | 7.2 | 5.8 | 4.5 | 0.8 | 143 | 598 0.00 |
| 9 | 0 | 1 | 1 | 44 | 6.3 | 9.1 | 5.9 | 4.5 | 0.8 | 143 | 573 0.00 |
| 9 | 0 | 1 | 1 | 37 | 6.3 | 8.0 | 6.7 | 4.9 | 0.0 | 143 | 552 0.00 |
| 9 | 0 | 1 | 1 | 28 | 6.3 | 7.3 | 7.3 | 5.0 | 0.0 | 109 | 555 0.00 |
| 10 | 0 | 1 | 1 | 21 | 7.7 | 8.9 | 7.4 | 5.3 | 0.0 | 84 | 557 0.00 |
| 11 | 0 | 1 | 1 | 15 | 8.5 | 9.8 | 7.4 | 5.3 | 0.0 | 80 | 547 0.00 |
| 11 | 0 | 1 | 1 | 11 | 8.5 | 9.1 | 8.0 | 5.7 | 0.0 | 76 | 534 0.00 |
| 12 | 0 | 1 | 1 | 3 | 7.4 | 7.8 | 8.0 | 5.7 | 0.0 | 73 | 526 0.00 |

| PROPPANT SUMMARY * At End of Pumping Schedule | | | |
|---|-------------------------|--|--|
| SANTOS - EM#37 (190/230/250) POST-FRAC EVALUATION | | | |
| Lb/Sq-Ft | Lost to Embedment | 0.200 | |
| Distance (ft) | KFW (md-ft) | Prop Concentration(Total 1b/sq foot) Prop ID--> 1 | |
| 5.3 | 1693 | 1.00 | |
| 12.0 | 1821 | 1.00 | |
| 15.0 | 1848 | 1.00 | |
| 18.0 | 1780 | 1.00 | |
| 21.0 | 1778 | 1.00 | |
| 24.0 | 1779 | 1.00 | |
| 27.0 | 1640 | 0.90 | |
| 30.0 | 1569 | 0.90 | |
| 33.0 | 1612 | 0.90 | |
| 36.0 | 1615 | 0.90 | |
| 39.5 | 1618 | 0.90 | |
| 42.9 | 1638 | 0.90 | |
| 45.9 | 1469 | 0.90 | |
| 48.9 | 1440 | 0.80 | |
| 51.9 | 1432 | 0.80 | |
| 54.9 | 1423 | 0.80 | |
| 57.9 | 1451 | 0.90 | |
| 60.9 | 1641 | 0.90 | |
| 63.9 | 1412 | 0.80 | |
| 66.9 | 1215 | 0.70 | |
| 69.9 | 1208 | 0.70 | |
| 72.9 | 1266 | 0.80 | |
| 75.9 | 1296 | 0.80 | |
| 78.9 | 894 | 0.60 | |
| 81.9 | 885 | 0.60 | |
| 84.9 | 920 | 0.60 | |
| 87.9 | 1013 | 0.70 | |
| 90.9 | 459 | 0.40 | |
| 93.9 | 486 | 0.40 | |
| 96.9 | 579 | 0.50 | |
| 99.9 | 784 | 0.60 | |
| 102.9 | 539 | 0.40 | |
| 105.9 | 573 | 0.50 | |
| 108.9 | 872 | 0.60 | |
| 111.9 | 2459 | 1.30 | |
| 114.9 | 26 | 0.20 | |
| 117.9 | 357 | 0.40 | |

Average Conductivity (md-ft) 1287

| PROPPANT SUMMARY * At Fracture Closure | | | |
|---|-------------------------|--|--|
| SANTOS - EM#37 (190/230/250) POST-FRAC EVALUATION | | | |
| Lb/Sq-Ft | Lost to Embedment | 0.200 | |
| Distance (ft) | KFW (md-ft) | Prop Concentration(Total 1b/sq foot) Prop ID--> 1 | |
| 5.3 | 1004 | 0.60 | |
| 12.0 | 1192 | 0.70 | |
| 15.0 | 1198 | 0.70 | |
| 18.0 | 1205 | 0.70 | |
| 21.0 | 1225 | 0.70 | |
| 24.0 | 1302 | 0.80 | |
| 27.0 | 1284 | 0.70 | |
| 30.0 | 1290 | 0.80 | |
| 33.0 | 1295 | 0.80 | |
| 36.0 | 1301 | 0.80 | |
| 39.5 | 1876 | 1.00 | |
| 42.9 | 1941 | 1.00 | |
| 45.9 | 1907 | 1.00 | |
| 48.9 | 1903 | 1.00 | |
| 51.9 | 1900 | 1.00 | |
| 54.9 | 1917 | 1.00 | |
| 57.9 | 1512 | 0.80 | |
| 60.9 | 1510 | 0.80 | |
| 63.9 | 1508 | 0.80 | |
| 66.9 | 1507 | 0.80 | |
| 69.9 | 1535 | 0.90 | |
| 72.9 | 1949 | 1.00 | |
| 75.9 | 1810 | 1.00 | |
| 78.9 | 1644 | 0.90 | |
| 81.9 | 1643 | 0.90 | |
| 84.9 | 2180 | 1.10 | |
| 87.9 | 1589 | 0.90 | |
| 90.9 | 1377 | 0.80 | |
| 93.9 | 1297 | 0.80 | |
| 96.9 | 1912 | 1.00 | |
| 99.9 | 1651 | 0.90 | |
| 102.9 | 2539 | 1.30 | |
| 105.9 | 1804 | 1.00 | |
| 108.9 | 2001 | 1.10 | |
| 111.9 | 2281 | 1.20 | |
| 114.9 | 27 | 0.20 | |
| 117.9 | 374 | 0.40 | |

Average Conductivity (md-ft) 1519

APPENDIX B

Svc. Co. Treatment Job Log

