

APPENDIX 2

DRILL STEM TEST RESULTS

FORMATION TESTING SERVICE REPORT



Duncan, Oklahoma 73536



A Halliburton Company

NOMENCLATURE

B	= Formation Volume Factor (Res Vol / Std Vol)	—	
c_t	= System Total Compressibility	(Vol / Vol) / psi	
DR	= Damage Ratio	—	
h	= Estimated Net Pay Thickness	Ft	
k	= Permeability	md	
m	{	(Liquid) Slope Extrapolated Pressure Plot	psi cycle
		(Gas) Slope Extrapolated m(P) Plot	MM psi ² / cp cycle
m(P*)	= Real Gas Potential at P*	MM psi ² cp	
m(P_f)	= Real Gas Potential at P _f	MM psi ² cp	
AOF₁	= Maximum Indicated Absolute Open Flow at Test Conditions	MCFD	
AOF₂	= Minimum Indicated Absolute Open Flow at Test Conditions ..	MCFD	
P*	= Extrapolated Static Pressure	Psig	
P_f	= Final Flow Pressure	Psig	
Q	= Liquid Production Rate During Test	BPD	
Q₁	= Theoretical Liquid Production w/ Damage Removed	BPD	
Q_g	= Measured Gas Production Rate	MCFD	
r_i	= Approximate Radius of Investigation	Ft	
r_w	= Radius of Well Bore	Ft	
S	= Skin Factor		
t	= Total Flow Time Previous to Closed-in	Minutes	
Δt	= Closed-in Time at Data Point	Minutes	
T	= Temperature Rankine	R	
φ	= Porosity	—	
μ	= Viscosity of Gas or Liquid	cp	
Log	= Common Log		

DRILL STEM TEST REPORT

OPERATOR: MOONIE OIL NL DATE: 19-3-86
WELL NAME: EAST MEREENIE NO. 28 A P BASIN: AMADEUS
FIELD: MEREENIE STRUCTURE:
TEST NO: 1 FORMATION: PACOOTA P3 SAND NO: P3-120/130
ELEVATIONS GL: 2455 FT KB: 2475 FT PACKER AT: 4701.09 FT
INTERVAL: 4706 TO 4756 FT TEST TYPE: OPEN HOLE

TEST STATISTICS

COMPANY: HALLIBURTON OPERATOR: NORM COWLEY
TOOL: HYDROSPRING CHOKE SIZE TOP: .5 INS BOTTOM: .75 INS
ANCHOR LENGTH: 17.06 FT OD: 5 INS
PERFORATED: 4738.94 TO 4756 FT LENGTH: 17.06 FT
PRESSURE RECORDER: TYPE POSITION DEPTH CLOCK
1. BOURDON TUBE TOP 4678.99 24 HR
2. BOURDON TUBE BOTTOM 4754 FT 24 HR

CAPACITIES

HOLE SIZE: 7.625 INS INTERVAL: 4706 TO 4756 FT
RAT HOLE: 7.625 INS INTERVAL: 4701.09 TO 4756 FT
DRILL PIPE: .01422 BLS/FT COLLARS: .0049 BLS/FT

TIME RECORD

<u>ACTUAL</u>		<u>ELAPSED TIMES</u>	
START CLOCK:	0134 HRS	START TO SEPERATOR:	HRS
START IN HOLE:	0204 HRS	STOP SEPERATOR:	HRS
TOOL OPENED:	0714 HRS	IF:	20 MINS
TOOL SHUT:	0734 HRS	ISI:	40 MINS
TOOL OPENED:	0814 HRS	FF:	302 MINS
TOOL SHUT:	1316 HRS	FSI:	358 MINS
PACK PULLED:	1914 HRS	TOTAL FLOW:	322 MINS
OUT OF HOLE:	0030 HRS	SEPERATOR FLOW:	MINS

PRESSURE RECORD

CHART: BOTTOM CLOCK: 24 HR
IHP: 2095 PSI
IFP: 54.6 PSI
ISIP: 1395.8 PSI
FFP: 185.4 PSI
FSIP: 1639.4 PSI
FHP: 2081 PSI
WHFP: PSI

RECOVERY

GTS: 15 MIN AT CU FT/D
OTS: MIN AT BLS/D (US)
WTS: MIN AT BLS/D (US)
GOR: CU FT/BL
ORIFICE SIZE: INS
FLOW PROVER PRESSURE: PSI
SG OF GAS: GM/CC
SG OF OIL: API AT °F
WATER SALINITY: PPM
MAXIMUM TEMP: 146 °F

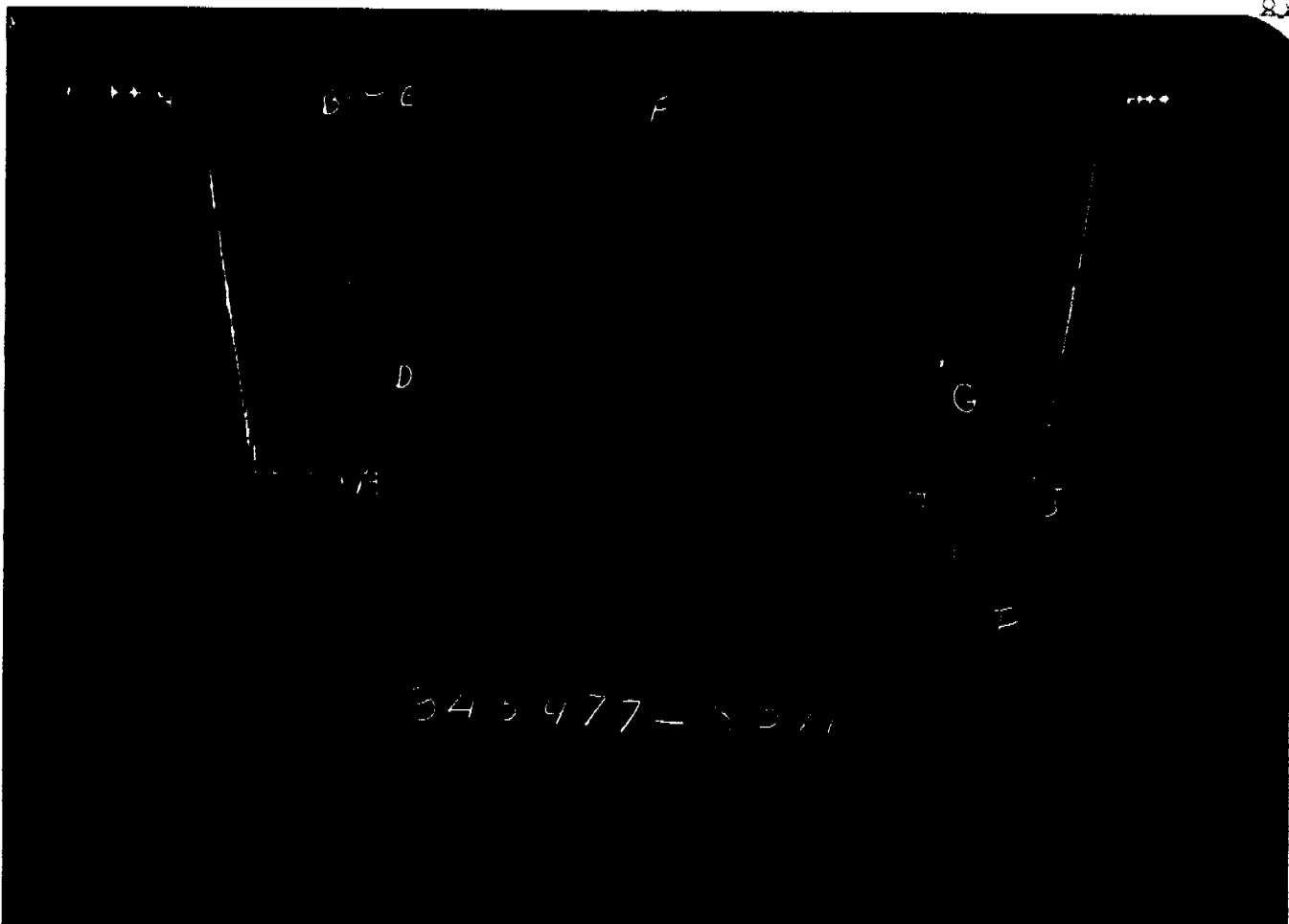
NATURE OF BLOW: INITIAL FLOW; INSTANT WEAK BLOW INCREASING TO STRONG AFTER 2 MINS REDUCING TO MODERATE AFTER 16 MINS. GTS AFTER 15 MINS. MANIFOLD OPEN WITH 1 PSI FROM 0716 - 0743 HRS FINAL FLOW; GAS AT SURFACE, 6 PSI AT 0816 HRS DECREASING TO 0 PSI AT 0850 HRS. STRONG BLOW DECREASING TO WEAK AT 0950 HRS. AT 1124 HRS SURGING FROM VERY WEAK TO MODERATE IN 1-2 MIN CYCLES. AT 1234 HRS SURGING FROM DEAD TO STRONG IN 10 MIN CYCLES. REVERSE CIRCULATION RECOVERED 7.7 BBLs OF RAT-HOLE OIL MUD (GAS CUT). CHART SHOWS GAS BUBBLING OR PLUGGING AT END OF FF. LOW PERMEABILITY WITH HIGH RESERVOIR PRESSURE.



TICKET NO. 34547700
02-APR-86
ALICE SPRINGS

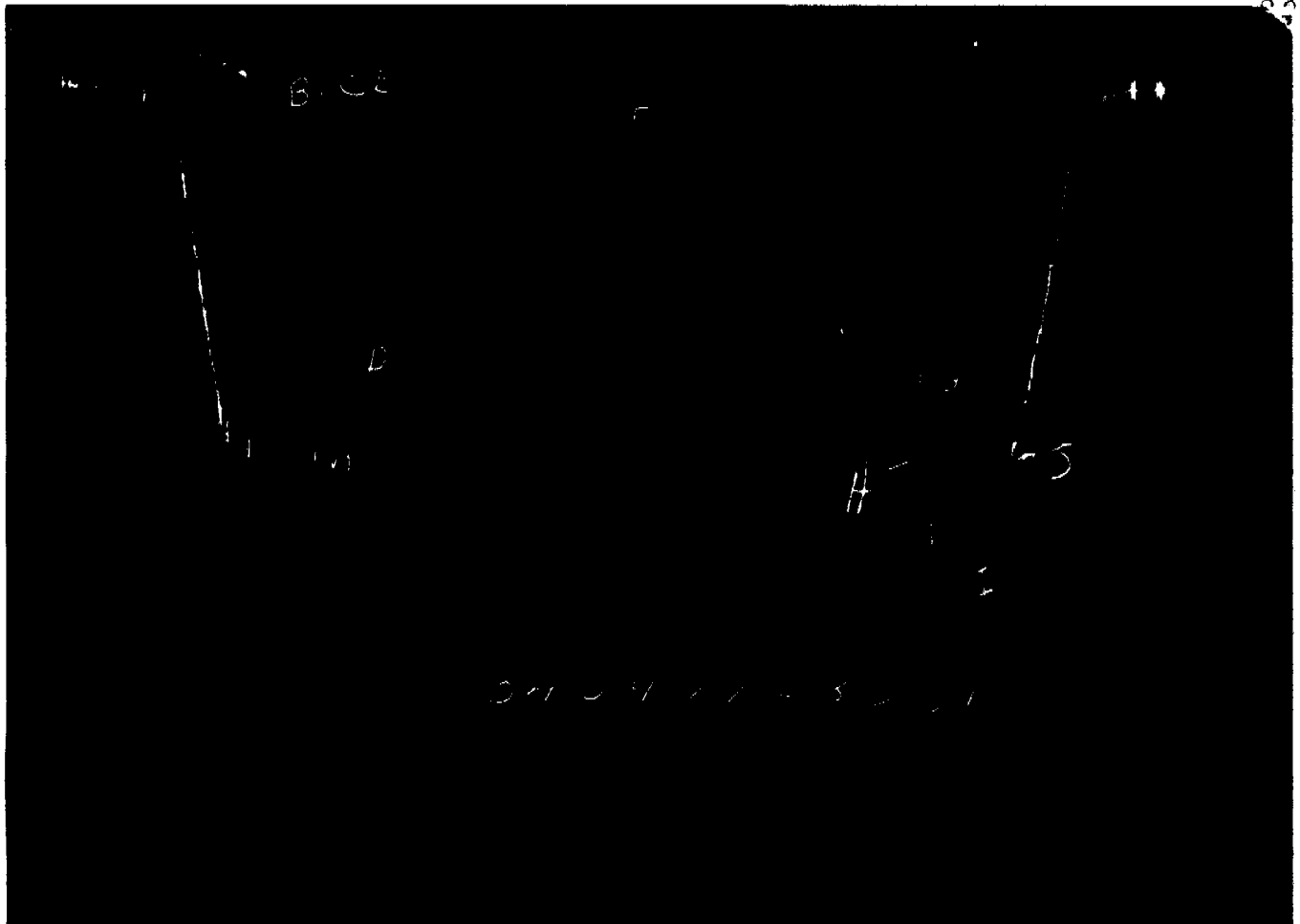
FORMATION TESTING SERVICE REPORT

EAST MERENIE 28
LEASE NAME WELL NO. TEST NO. 1
4701.0 - 4756.0
TESTED INTERVAL
MOONIE OIL COMPANY LTD.
LEASE OWNER/COMPANY NAME
LEGAL LOCATION SEE REMARKS
SEC. - TYP. - RNS. FIELD AREA
AMARDEUS BASIN
COUNTY N. TERRITORY
STATE AUSTRALIA DR



GAUGE NO: 8511 DEPTH: 4678.0 BLANKED OFF: NO HOUR OF CLOCK: 24

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	2029	2031.7			
B	INITIAL FIRST FLOW	24	22.9	20.0	19.9	F
C	FINAL FIRST FLOW	45	48.3			
C	INITIAL FIRST CLOSED-IN	45	48.3	40.0	39.3	C
D	FINAL FIRST CLOSED-IN	1355	1358.9			
E	INITIAL SECOND FLOW	71	68.8	302.0	303.5	F
F	FINAL SECOND FLOW	163	167.9			
F	INITIAL SECOND CLOSED-IN	163	167.9	358.0	357.3	C
G	FINAL SECOND CLOSED-IN	1593	1598.0			
H	HYDROSTATIC		2031.3			
I	REVERSING		2631.9			
J	FINAL HYDROSTATIC	2026	2047.8			



GAUGE NO: 8531 DEPTH: 4753.0 BLANKED OFF: YES HOUR OF CLOCK: 24

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	2095	2075.1			
B	INITIAL FIRST FLOW	59	54.2	20.0	19.9	F
C	FINAL FIRST FLOW	65	62.6			
C	INITIAL FIRST CLOSED-IN	65	62.6	40.0	39.3	C
D	FINAL FIRST CLOSED-IN	1396	1398.3			
E	INITIAL SECOND FLOW	76	63.3	302.0	303.5	F
F	FINAL SECOND FLOW	185	184.0			
F	INITIAL SECOND CLOSED-IN	185	184.0	358.0	357.3	C
G	FINAL SECOND CLOSED-IN	1639	1635.2			
H	HYDROSTATIC		2077.5			
I	REVERSING		2686.5			
J	FINAL HYDROSTATIC	2081	2094.4			

EQUIPMENT & HOLE DATA

FORMATION TESTED: PACQOITA P3-120/130
 NET PAY (ft): _____
 GROSS TESTED FOOTAGE: 55.0
 ALL DEPTHS MEASURED FROM: KELLY BUSHING
 CASING PERFS. (ft): _____
 HOLE OR CASING SIZE (in): 7.625
 ELEVATION (ft): 2475.0
 TOTAL DEPTH (ft): 4756.0
 PACKER DEPTH(S) (ft): 4693. 4701
 FINAL SURFACE CHOKE (in): 0.50000
 BOTTOM HOLE CHOKE (in): 0.750
 MUD WEIGHT (lb/gal): 8.30
 MUD VISCOSITY (sec): 45
 ESTIMATED HOLE TEMP. (°F): _____
 ACTUAL HOLE TEMP. (°F): 146 @ 4752.0 ft

TICKET NUMBER: 34547700
 DATE: 3-19-86 TEST NO: 1
 TYPE DST: OPEN HOLE
 HALLIBURTON CAMP: ALICE SPRINGS
 TESTER: N. COWLEY
 WITNESS: A. EDWARDS 22222
 DRILLING CONTRACTOR: MEREENIE #1

FLUID PROPERTIES FOR RECOVERED MUD & WATER

SOURCE	RESISTIVITY	CHLORIDES
_____	_____ °F	_____ ppm
_____	_____ °F	_____ ppm
_____	_____ °F	_____ ppm
_____	_____ °F	_____ ppm
_____	_____ °F	_____ ppm
_____	_____ °F	_____ ppm

SAMPLER DATA

Pstg AT SURFACE: _____
 cu.ft. OF GAS: _____
 cc OF OIL: _____
 cc OF WATER: _____
 cc OF MUD: _____
 TOTAL LIQUID cc: _____

HYDROCARBON PROPERTIES

OIL GRAVITY (°API): _____ °F
 GAS/OIL RATIO (cu.ft. per bbl): _____
 GAS GRAVITY: _____

CUSHION DATA

TYPE	AMOUNT	WEIGHT
_____	_____	_____
_____	_____	_____

RECOVERED:

7.7 BBLs. OF GAS CUT RAT HOLE MUD

MEASURED FROM
TESTER VALVE

REMARKS:

LEGAL LOCATION: LAT. 24 DEGREES, 01', 33" SOUTH AND
 LONG. 131 DEGREES, 36', 58" EAST

COMPLETE CALCULATION SERVICE COULD NOT BE PERFORMED DUE TO LACK OF SUFFICIENT HYDROCARBON PRODUCTION FROM WHICH TO OBTAIN A PRODUCTION RATE. PLOTS ARE INCLUDED AT THE END OF THIS REPORT FOR YOUR INSPECTION.

TYPE & SIZE MEASURING DEVICE: _____ 6" CERAMIC SURFACE CHOKE _____				TICKET NO: 34547700	
TIME	CHOKE SIZE	SURFACE PRESSURE PSI	GAS RATE MCF	LIQUID RATE BPD	REMARKS
3-19-86					
0145					MADE UP TOOL
0257					TOOL MADE UP AND WENT IN HOLE
0630					HEAD UP
0709					SEATED PACKERS WITH 30,000#
0714	.50				OPENED TOOL WITH A VERY WEAK BLOW
0716	.50	1			BLOW INCREASED TO STRONG
0729	.50	1			GAS TO SURFACE IN 15 MINUTES
0730	.50	1			BLOW DECREASED TO MODERATE BLOW
0734		1			CLOSED TOOL
0814	.50				OPENED TOOL WITH A MODERATE BLOW AND GAS TO SURFACE
0815	.50	2.50			BLOW INCREASED TO A STRONG BLOW
0816	.50	6			
0819	.50	2			
0839	.50	1			BLOW DECREASED TO A MODERATE BLOW
0850	.50				
0950	.50				BLOW DECREASED TO A WEAK BLOW
1030	.50				WEAK BLOW
1124	.50				BLOW SURGING FROM A WEAK TO MODERATE BLOW IN 1 MINUTE CYCLES
1200	.50				SAME AS ABOVE
1234	.50				BLOW SURGING BETWEEN DEAD AND STRONG IN 10 MINUTES CYCLES
1316					CLOSED TOOL
1914					PULLED FREE AND OPENED BYPASS
1922					DROPPED BAR TO REVERSE CIRCULATE
1923					PIN BROKE-STARTED REVERSING
2100					HEAD DOWN AND PUMPED PILL
2120					PULLED OUT OF HOLE
2320					TOOL AT FLOOR

TICKET NO: 34547700
 CLOCK NO: 29491 HOUR: 24



GAUGE NO: 8511
 DEPTH: 4678.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	22.9			
2	2.0	40.1	17.2		
3	4.0	47.0	6.8		
4	6.0	48.9	2.0		
5	8.0	48.9	0.0		
6	10.0	48.9	0.0		
7	12.0	48.9	0.0		
8	14.0	48.9	0.0		
9	16.0	48.4	-0.5		
10	18.0	48.4	0.0		
C 11	19.9	48.3	-0.1		
FIRST CLOSED-IN					
C 1	0.0	48.3			
2	1.0	89.7	41.4	1.0	1.303
3	2.0	131.8	83.6	1.8	1.046
4	3.0	178.0	129.7	2.6	0.882
5	4.0	227.2	178.9	3.3	0.777
6	5.0	271.6	223.3	4.0	0.695
7	6.0	318.8	270.5	4.6	0.636
8	7.0	370.7	322.4	5.2	0.583
9	8.0	416.7	368.4	5.7	0.542
10	9.0	456.8	408.6	6.2	0.508
11	10.0	503.6	455.3	6.7	0.475
12	12.0	597.5	549.2	7.5	0.425
13	14.0	677.2	628.9	8.2	0.385
14	16.0	760.8	712.5	8.9	0.352
15	18.0	836.2	787.9	9.5	0.324
16	20.0	905.9	857.6	10.0	0.300
17	22.0	970.7	922.4	10.5	0.280
18	24.0	1043.7	995.4	10.9	0.262
19	26.0	1105.6	1057.3	11.3	0.247
20	28.0	1156.3	1108.0	11.6	0.233
21	30.0	1203.5	1155.2	12.0	0.221
22	35.0	1302.1	1253.8	12.7	0.196
D 23	39.3	1358.9	1310.6	13.2	0.178
SECOND FLOW					
E 1	0.0	68.8			
2	10.0	88.7	19.9		
3	20.0	90.7	2.0		
4	30.0	91.4	0.8		
5	40.0	91.4	0.0		
6	50.0	91.7	0.3		
7	60.0	92.1	0.4		
8	70.0	95.3	3.2		
9	80.0	98.3	3.0		
10	90.0	101.6	3.3		

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND FLOW - CONTINUED					
11	100.0	104.7	3.2		
12	110.0	107.8	3.0		
13	120.0	111.4	3.7		
14	130.0	114.1	2.6		
15	140.0	118.0	3.9		
16	150.0	121.3	3.3		
17	160.0	124.6	3.3		
18	170.0	127.9	3.3		
19	180.0	132.5	4.6		
20	190.0	136.1	3.6		
21	200.0	137.6	1.6		
22	210.0	141.6	3.9		
23	220.0	144.7	3.2		
24	230.0	147.1	2.4		
25	240.0	149.9	2.8		
26	250.0	151.1	1.2		
27	260.0	158.9	7.9		
28	270.0	155.3	-3.7		
29	280.1	149.5	-5.8		
30	290.0	167.0	17.5		
31	300.0	168.6	1.6		
F 32	303.5	167.9	-0.7		
SECOND CLOSED-IN					
F 1	0.0	167.9			
2	1.0	178.8	10.9	1.0	2.499
3	2.0	200.1	32.2	2.0	2.212
4	3.0	223.8	55.9	3.0	2.039
5	4.0	244.9	77.0	3.9	1.917
6	5.0	263.8	95.9	4.9	1.816
7	6.0	285.0	117.1	5.9	1.740
8	7.0	310.8	142.9	6.8	1.676
9	8.0	338.4	170.5	7.8	1.616
10	9.0	362.8	194.9	8.8	1.565
11	10.0	383.2	215.3	9.7	1.522
12	12.0	431.7	263.8	11.6	1.446
13	14.0	489.7	321.8	13.5	1.381
14	16.0	547.6	379.7	15.2	1.326
15	18.0	593.8	425.9	17.1	1.278
16	20.0	670.7	502.8	18.8	1.235
17	22.0	756.3	588.4	20.6	1.195
18	24.0	857.4	689.5	22.3	1.161
19	26.0	952.9	785.0	24.1	1.128
20	28.0	1047.3	879.4	25.8	1.098
21	30.0	1138.6	970.7	27.4	1.071
22	35.0	1293.9	1126.0	31.6	1.011
23	40.0	1384.2	1216.3	35.6	0.958
24	45.0	1435.8	1267.9	39.5	0.913
25	50.0	1465.3	1297.4	43.3	0.873
26	55.0	1484.7	1316.8	47.0	0.838
27	60.0	1499.2	1331.3	50.6	0.805
28	70.0	1517.6	1349.7	57.5	0.750

REMARKS:

TICKET NO: 34547700
CLOCK NO: 29491 HOUR: 24



GAUGE NO: 8511
DEPTH: 4678.0

REF	MINUTES	PRESSURE	ΔP	$\frac{1 \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND CLOSED-IN - CONTINUED					
29	80.0	1530.3	1362.4	64.1	0.703
30	90.0	1540.2	1372.3	70.4	0.662
31	100.0	1547.5	1379.6	76.4	0.627
32	110.0	1554.5	1386.6	82.1	0.595
33	120.0	1559.4	1391.6	87.5	0.568
34	135.0	1566.3	1398.4	95.3	0.531
35	150.0	1572.2	1404.3	102.5	0.499
36	165.0	1575.2	1407.3	109.3	0.471
37	180.0	1578.3	1410.5	115.6	0.447
38	195.0	1582.3	1414.4	121.6	0.425
39	210.0	1585.7	1417.8	127.3	0.405
40	225.0	1586.9	1419.0	132.7	0.387
41	240.0	1587.5	1419.6	137.8	0.371
42	260.0	1588.7	1420.8	144.1	0.351
43	280.0	1590.2	1422.3	150.1	0.333
44	300.0	1591.5	1423.6	155.6	0.318
45	320.0	1593.2	1425.3	160.9	0.303
46	340.0	1594.9	1427.0	165.7	0.290
G 47	357.3	1598.0	1430.1	169.8	0.280

REF	MINUTES	PRESSURE	ΔP	$\frac{1 \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$

REMARKS:

TICKET NO: 34547700
 CLOCK NO: 29475 HOUR: 24



GAUGE NO: 8531
 DEPTH: 4753.0

REF	MINUTES	PRESSURE	AP	$\frac{1 \times \Delta t}{1 + \Delta t}$	$\log \frac{1 + \Delta t}{\Delta t}$
FIRST FLOW					
B	1	0.0	54.2		
	2	2.0	62.6	8.4	
	3	4.0	62.6	0.0	
	4	6.0	62.6	0.0	
	5	8.0	62.2	-0.4	
	6	10.0	62.2	0.0	
	7	12.0	62.2	0.0	
	8	14.0	62.2	0.0	
	9	16.0	62.2	0.0	
	10	18.0	62.2	0.0	
C	11	19.9	62.6	0.4	
FIRST CLOSED-IN					
C	1	0.0	62.6		
	2	1.0	132.9	70.2	1.0 1.311
	3	2.0	172.8	110.1	1.8 1.036
	4	3.0	220.4	157.7	2.6 0.885
	5	4.0	269.1	206.5	3.4 0.773
	6	5.0	319.8	257.2	4.0 0.697
	7	6.0	370.9	308.3	4.6 0.636
	8	7.0	420.6	358.0	5.2 0.583
	9	8.0	461.5	398.9	5.7 0.543
	10	9.0	503.6	441.0	6.2 0.508
	11	10.0	556.5	493.9	6.7 0.476
	12	12.0	646.9	584.3	7.5 0.424
	13	14.0	728.6	665.9	8.2 0.384
	14	16.0	811.6	748.9	8.9 0.351
	15	18.0	890.7	828.0	9.4 0.324
	16	20.0	958.4	895.7	10.0 0.300
	17	22.0	1022.5	959.9	10.4 0.280
	18	24.0	1085.4	1022.8	10.9 0.262
	19	26.0	1139.3	1076.7	11.3 0.247
	20	28.0	1191.3	1128.6	11.6 0.233
	21	30.0	1241.8	1179.2	12.0 0.221
	22	35.0	1338.2	1275.6	12.7 0.195
D	23	39.3	1398.3	1335.7	13.2 0.178
SECOND FLOW					
E	1	0.0	63.3		
	2	10.0	95.1	31.7	
	3	20.0	98.7	3.7	
	4	30.0	100.4	1.7	
	5	40.0	101.4	1.0	
	6	50.0	101.4	0.0	
	7	60.0	106.7	5.3	
	8	70.0	110.8	4.1	
	9	80.0	113.9	3.1	
	10	90.0	117.3	3.4	

REF	MINUTES	PRESSURE	AP	$\frac{1 \times \Delta t}{1 + \Delta t}$	$\log \frac{1 + \Delta t}{\Delta t}$
SECOND FLOW - CONTINUED					
	11	100.0	121.6	4.4	
	12	110.0	124.3	2.7	
	13	120.0	127.7	3.4	
	14	130.0	131.3	3.7	
	15	140.1	134.3	2.9	
	16	150.0	137.9	3.7	
	17	160.0	141.9	3.9	
	18	170.0	146.3	4.5	
	19	180.0	149.7	3.4	
	20	190.0	153.8	4.1	
	21	200.0	155.3	1.5	
	22	210.0	156.7	1.4	
	23	220.0	163.2	6.5	
	24	230.0	163.1	-0.1	
	25	240.0	163.2	0.1	
	26	250.0	166.6	3.4	
	27	260.0	174.2	7.6	
	28	270.0	169.0	-5.2	
	29	280.0	158.0	-11.0	
	30	290.0	180.6	22.6	
	31	300.0	184.1	3.5	
F	32	303.5	184.0	-0.1	
SECOND CLOSED-IN					
F	1	0.0	184.0		
	2	1.0	198.6	14.6	1.0 2.501
	3	2.0	219.4	35.4	2.0 2.208
	4	3.0	241.0	57.0	3.0 2.039
	5	4.0	264.7	80.8	4.0 1.912
	6	5.0	289.9	105.9	5.0 1.815
	7	6.0	310.8	126.8	5.9 1.740
	8	7.0	335.3	151.3	6.9 1.673
	9	8.0	358.4	174.4	7.8 1.615
	10	9.0	379.9	195.9	8.8 1.567
	11	10.0	400.6	216.6	9.7 1.524
	12	12.0	453.7	269.7	11.6 1.446
	13	14.0	518.2	334.3	13.4 1.382
	14	16.0	571.9	387.9	15.2 1.327
	15	18.0	617.3	433.3	17.0 1.279
	16	20.0	689.7	505.7	18.8 1.235
	17	22.0	783.6	599.6	20.6 1.196
	18	24.0	870.8	686.8	22.3 1.161
	19	26.0	962.0	778.0	24.1 1.128
	20	28.0	1065.0	881.0	25.8 1.098
	21	30.0	1154.3	970.3	27.4 1.072
	22	35.0	1315.0	1131.0	31.6 1.010
	23	40.0	1411.9	1228.0	35.6 0.958
	24	45.0	1463.6	1279.6	39.5 0.913
	25	50.0	1496.9	1313.0	43.3 0.873
	26	55.0	1519.7	1335.7	47.0 0.837
	27	60.0	1535.8	1351.8	50.6 0.805
	28	70.0	1553.8	1369.8	57.5 0.750

REMARKS:

TICKET NO: 34547700

CLOCK NO: 29475 HOUR: 24



GAUGE NO: 8531
























DEPTH: 4753.0

REF	MINUTES	PRESSURE	AP	$\frac{1 \times \Delta t}{1 + \Delta t}$	$\log \frac{1 + \Delta t}{\Delta t}$
SECOND CLOSED-IN - CONTINUED					
29	80.0	1567.7	1383.8	64.1	0.703
30	90.0	1577.7	1393.8	70.4	0.662
31	100.0	1585.5	1401.5	76.4	0.627
32	110.0	1592.0	1408.0	82.1	0.595
33	120.0	1597.5	1413.5	87.5	0.568
34	135.0	1603.7	1419.7	95.2	0.531
35	150.0	1609.3	1425.3	102.5	0.499
36	165.0	1613.5	1429.5	109.3	0.471
37	180.0	1616.1	1432.1	115.6	0.447
38	195.0	1620.7	1436.7	121.6	0.425
39	210.0	1623.9	1440.0	127.3	0.405
40	225.0	1625.5	1441.5	132.7	0.387
41	240.0	1625.5	1441.5	137.8	0.371
42	260.0	1626.9	1442.9	144.1	0.351
43	280.0	1628.5	1444.5	150.1	0.333
44	300.0	1629.7	1445.7	155.6	0.318
45	320.0	1631.4	1447.4	160.9	0.303
46	340.0	1632.7	1448.7	165.7	0.290
G 47	357.3	1635.2	1451.2	169.8	0.280

REF	MINUTES	PRESSURE	AP	$\frac{1 \times \Delta t}{1 + \Delta t}$	$\log \frac{1 + \Delta t}{\Delta t}$

REMARKS:

TICKET NO. 34547700

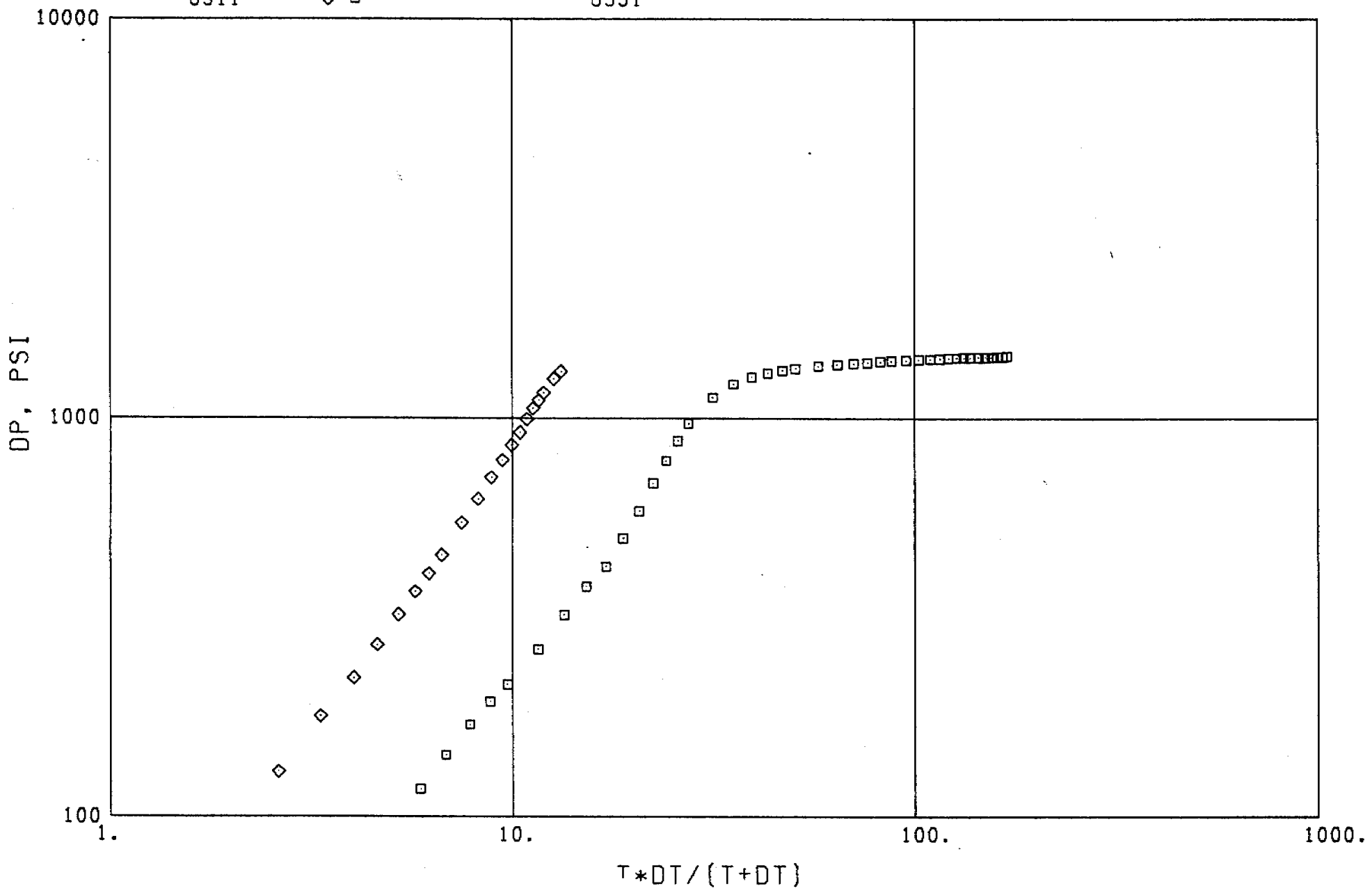
		O.D.	I.D.	LENGTH	DEPTH	
1		DRILL PIPE.....	4.500	3.826	3950.4	
4		FLEX WEIGHT.....	4.500	2.764	182.3	
3		DRILL COLLARS.....	6.250	2.375	457.8	
9		STABILIZER.....	6.438	2.375	6.5	
3		DRILL COLLARS.....	6.250	2.375	30.7	
50		IMPACT REVERSING SUB.....	6.250	3.000	1.0	4627.6
3		DRILL COLLARS.....	6.250	2.375	30.4	
9		STABILIZER.....	6.438	2.313	6.6	
258		BAR CATCHER SUB	6.250	1.000	1.0	4666.0
12		DUAL CIP VALVE.....	5.000	0.870	4.9	
60		HYDROSPRING TESTER.....	5.000	0.750	5.3	4676.0
80		AP RUNNING CASE.....	5.000	2.250	4.1	4678.0
15		JAR.....	5.000	1.750	5.0	
16		VR SAFETY JOINT.....	5.000	1.000	2.8	
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	4693.3
18		DISTRIBUTOR VALVE.....	5.000	1.680	2.0	
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	4701.0
19		ANCHOR PIPE SAFETY JOINT.....	5.000	1.500	4.3	
5		CROSSOVER.....	6.250	2.200	1.0	
3		DRILL COLLARS.....	6.250	2.375	30.2	
5		CROSSOVER.....	6.250	2.250	1.0	
20		FLUSH JOINT ANCHOR.....	5.000	2.370	13.0	
81		BLANKED-OFF RUNNING CASE.....	5.000		4.1	4753.0
TOTAL DEPTH						4756.0

EQUIPMENT DATA

TICKET NO 34547700

GAUGE NO CIP 1 2
8511 ◇ □

GAUGE NO CIP 1 2
8531

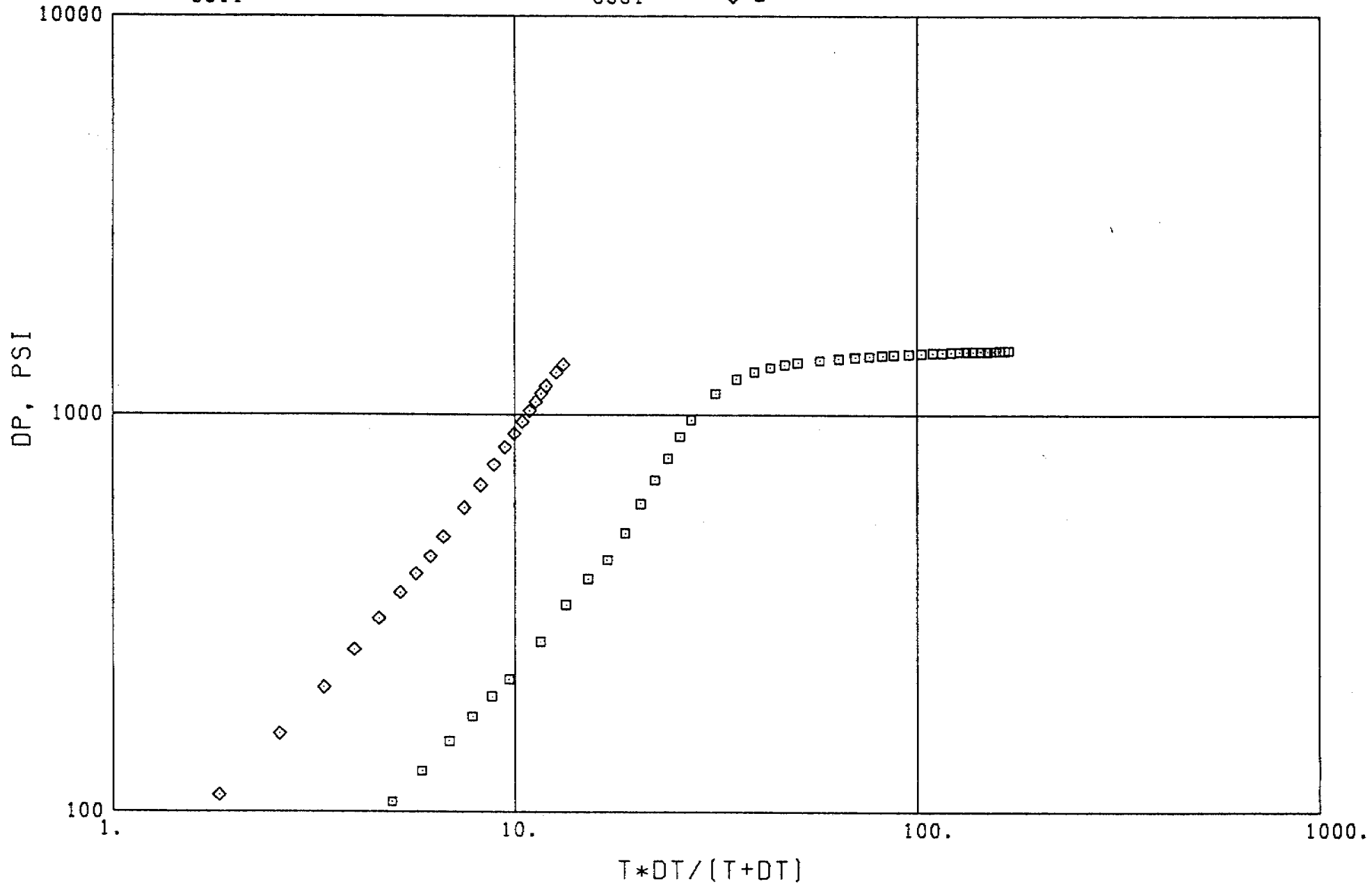


0.98

TICKET NO 34547700

GAUGE NO CIP 1 2
8511

GAUGE NO CIP 1 2
8531 \diamond \square

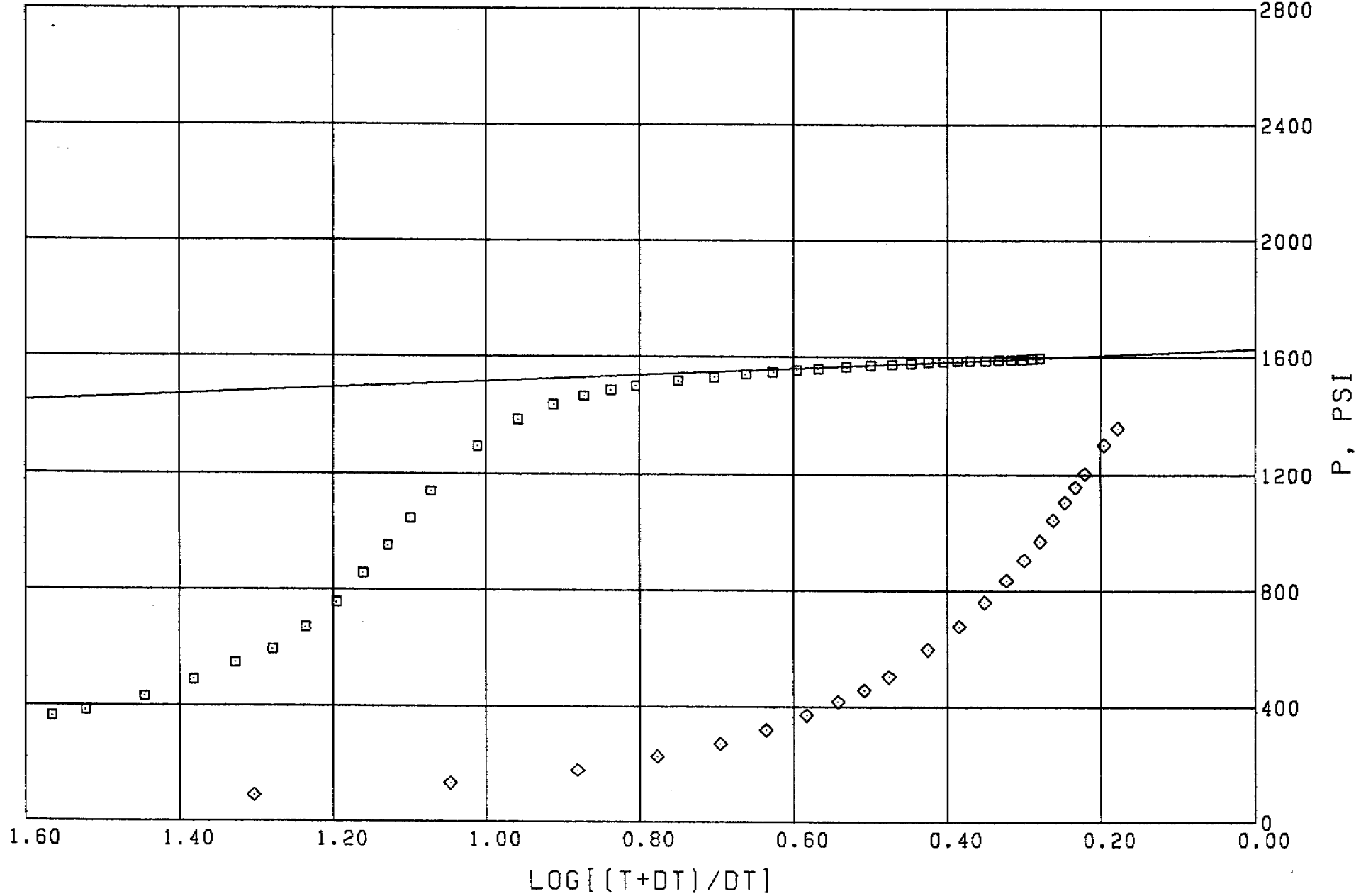


0.00

TICKET NO 34547700

GAUGE NO CIP 1 2
8511 ◇ □

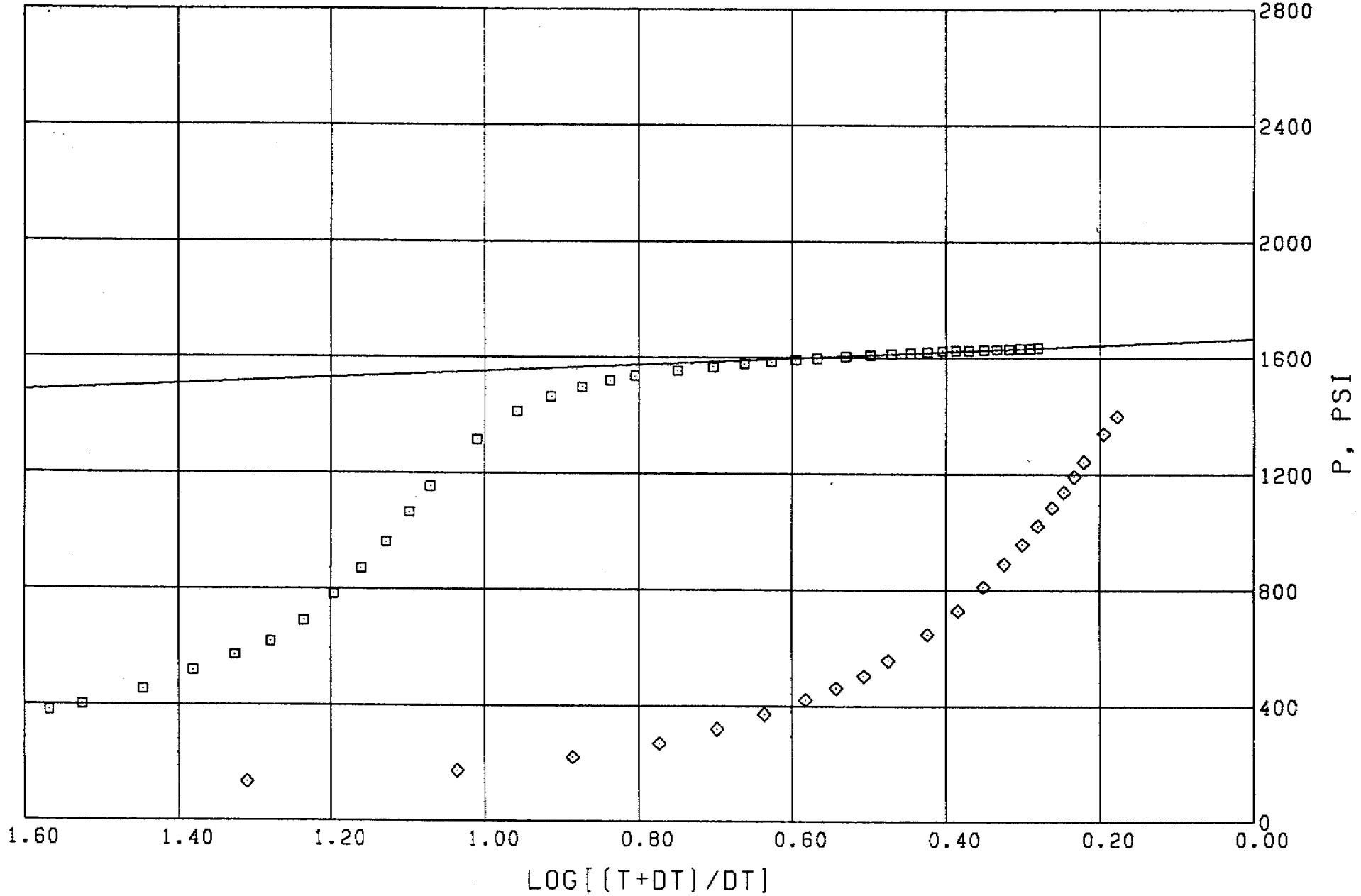
GAUGE NO CIP 1 2
8531



TICKET NO 34547700

GAUGE NO CIP 1 2
8511

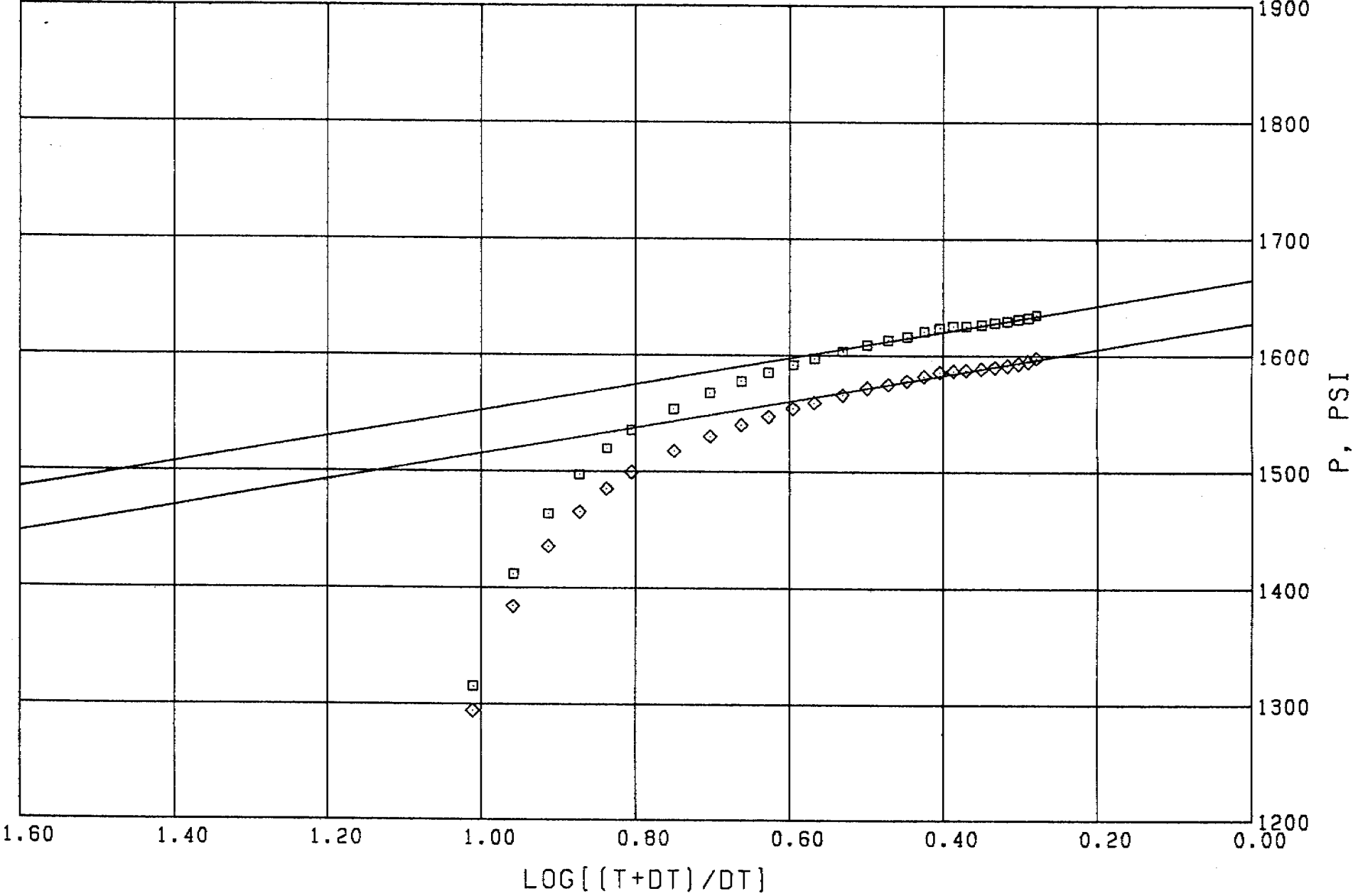
GAUGE NO CIP 1 2
8531 \diamond \square



TICKET NO 34547700

GAUGE NO CIP 1 2
8511 ◇

GAUGE NO CIP 1 2
8531 □



DRILL STEM TEST REPORT

OPERATOR: MOONIE OIL NL DATE: 22-3-86
WELL NAME: EAST MEREENIE NO. 28 A P BASIN: AMADEUS
FIELD: MEREENIE STRUCTURE:
TEST NO: 2 FORMATION: PACOOTA P3 SAND NO: P3-120/250
ELEVATIONS GL: 2455 FT KB: 2475 FT PACKER AT: 4702.88 FT
INTERVAL: 4706 TO 4910 FT TEST TYPE: DUAL PACKER DST

TEST STATISTICS

COMPANY: HALLIBURTON OPERATOR: NORM COWLEY
TOOL: HYDROSPRING CHOKE SIZE TOP: .5 INS BOTTOM: .75 INS
ANCHOR LENGTH: 37.06 FT OD: 5 INS
PERFORATED: 4872.94 TO 4910 FT LENGTH: 37.06 FT
PRESSURE RECORDER: TYPE POSITION DEPTH CLOCK
1. BOURDON TUBE TOP 4680.69 24 HR
2. BOURDON TUBE BOTTOM 4908 FT 24 HR

CAPACITIES

HOLE SIZE: 7.625 INS INTERVAL: 4706 TO 4910 FT
RAT HOLE: 7.625 INS INTERVAL: 4702.88 TO 4910 FT
DRILL PIPE: .014229 BLS/FT COLLARS: .0049 BLS/FT

TIME RECORD

<u>ACTUAL</u>		<u>ELAPSED TIMES</u>
START CLOCK:	0912 HRS	START TO SEPERATOR: 1717 HRS
START IN HOLE:	0939 HRS	STOP SEPERATOR: 1830 HRS
TOOL OPENED:	1428 HRS	IF: 20 MINS
TOOL SHUT:	1448 HRS	ISI: 40 MINS
TOOL OPENED:	1528 HRS	FF: 178 MINS
TOOL SHUT:	1830 HRS	FSI: 404 MINS
PACK PULLED:	0114 HRS	TOTAL FLOW: 198 MINS
OUT OF HOLE:	0806 HRS	SEPERATOR FLOW: 73 MINS

PRESSURE RECORD

CHART: BOTTOM CLOCK: 24 HR
IHP: 2206.7 PSI
IFP: 382 PSI
ISIP: 1771.8 PSI
FFP: 474.7 PSI
FSIP: 1766.2 PSI
FHP: 2184.4 PSI
WHFP: 80 PSI

RECOVERY

GTS: 8 MIN AT 237000 CU FT/D
OTS: 96 MIN AT 418 BLS/D (US)
WTS: MIN AT BLS/D (US)
GOR: 567 CU FT/BL
ORIFICE SIZE: .5 INS
FLOW PROVER PRESSURE: 40 PSI
SG OF GAS: .987 GM/CC
SG OF OIL: 47.8 API AT 60°F
WATER SALINITY: PPM
MAXIMUM TEMP: 150 °F

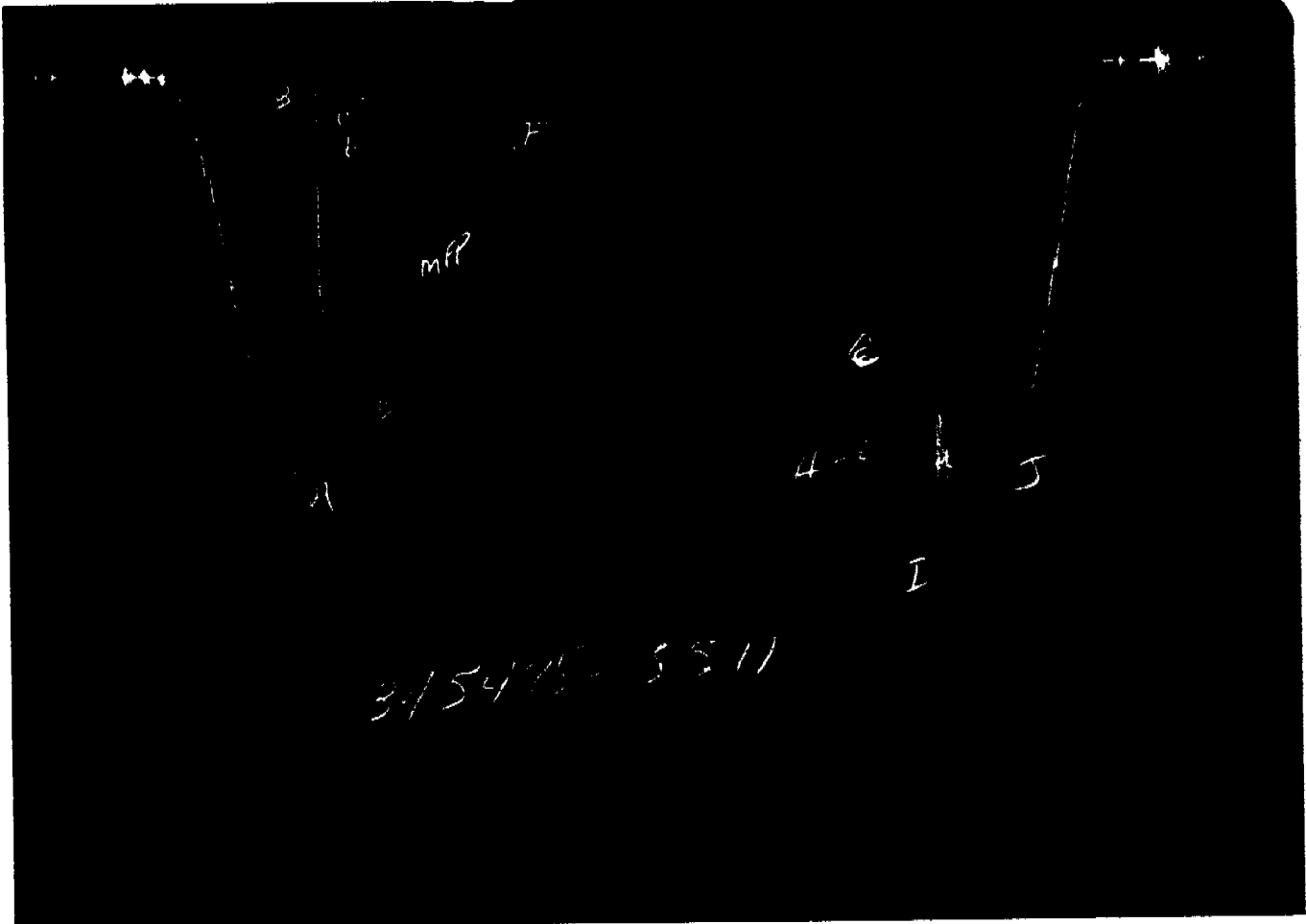
NATURE OF BLOW: INITIAL FLOW, IMMEDIATE WEAK BLOW INCREASING TO STRONG AFTER 5 MINS. GTS AFTER 8 MINS. MANIFOLD OPEN WITH CONSTANT STRONG BLOW, MAXIMUM 4 PSI PRESSURE AFTER 16 MINS. FINAL FLOW; IMMEDIATE STRONG BLOW, GAS AT SURFACE DECREASING TO VERY WEAK AFTER 28 MINS. TOTAL FLOW (OPSI). MUD TO SURFACE 89 MINS (3 PSI). OTS 96 MINS. (100 PSI) MANIFOLD PRESSURE CONSTANT 90 PSI FROM 121 MINS TO 162 MINS, 80 PSI FROM 162 TO 198 MINS (TOTAL FLOW). CHART INDICATES GOOD TEST WITH GOOD PERMEABILITY.



TICKET NO. 34547800
 02-APR-86
 ALICE SPRINGS

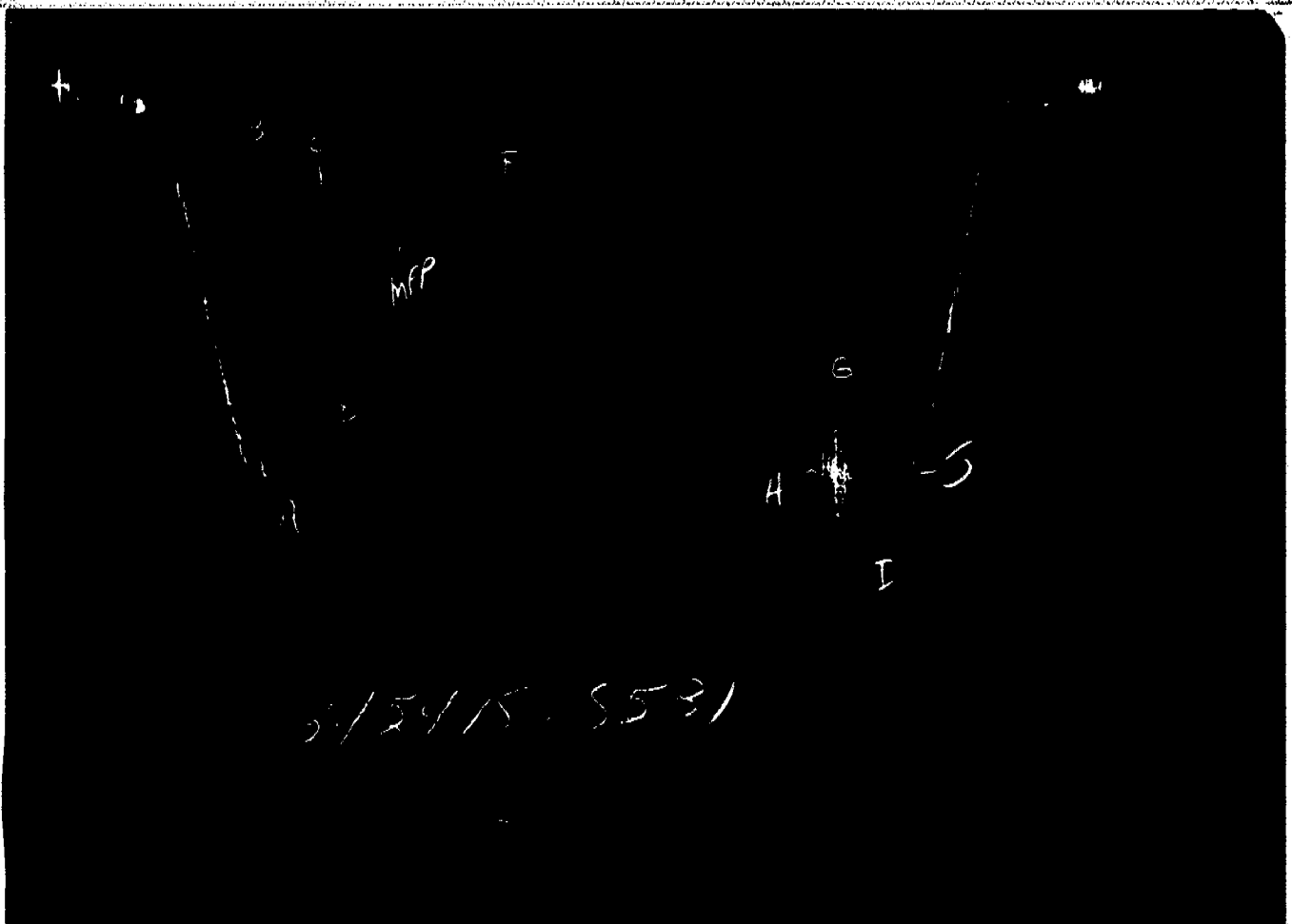
FORMATION TESTING SERVICE REPORT

LEGAL LOCATION SECT. - TWP. - RANG.	SEE REMARKS	FIELD AREA	COUNTY NO. TERRITORY	STATE AUSTRALIA	IC
EAST MERENIE					
LEASE NAME	WEILL NO.	TEST NO.	TESTED INTERVAL	LEASE OWNER/COMPANY NAME	
	28	2	4702.9 - 4910.0	MOONIE OIL COMPANY LTD.	



GAUGE NO: 8511 DEPTH: 4680.0 BLANKED OFF: NO HOUR OF CLOCK: 24

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	2110	2091.2			
B	INITIAL FIRST FLOW	31	21.8			
C	FINAL FIRST FLOW	305	303.9	20.0	18.9	F
C	INITIAL FIRST CLOSED-IN	305	303.9			
D	FINAL FIRST CLOSED-IN	1679	1675.3	40.0	37.4	C
E	INITIAL SECOND FLOW	407	385.3			
F	FINAL SECOND FLOW	413	407.0	182.0	183.8	F
F	INITIAL SECOND CLOSED-IN	413	407.0			
G	FINAL SECOND CLOSED-IN	1674	1676.6	404.0	405.9	C
H	HYDROSTATIC	2076	2077.4			
I	REVERSING		2614.4			
J	FINAL HYDROSTATIC		2102.9			



GAUGE NO: 8531 DEPTH: 4907.0 BLANKED OFF: YES HOUR OF CLOCK: 24

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	2206	2204.9			
B	INITIAL FIRST FLOW	182	123.3			
C	FINAL FIRST FLOW	382	383.8	20.0	18.9	F
C	INITIAL FIRST CLOSED-IN	382	383.8			
D	FINAL FIRST CLOSED-IN	1771	1768.0	40.0	37.4	C
E	INITIAL SECOND FLOW	488	446.6			
F	FINAL SECOND FLOW	474	472.8	182.0	183.8	F
F	INITIAL SECOND CLOSED-IN	474	472.8			
G	FINAL SECOND CLOSED-IN	1766	1763.7	404.0	405.9	C
H	HYDROSTATIC	2184	2181.3			
I	REVERSING		2727.6			
J	FINAL HYDROSTATIC		2231.6			

EQUIPMENT & HOLE DATA	TICKET NUMBER: <u>34547800</u>
FORMATION TESTED: <u>PACOOTTA P3-120/250</u>	DATE: <u>3-22-86</u> TEST NO: <u>2</u>
NET PAY (ft): _____	TYPE DST: <u>OPEN HOLE</u>
GROSS TESTED FOOTAGE: <u>207.1</u>	HALLIBURTON CAMP: _____
ALL DEPTHS MEASURED FROM: <u>KELLY BUSHING</u>	<u>ALICE SPRINGS</u>
CASING PERFS. (ft): _____	TESTER: <u>N. COWLEY</u>
HOLE OR CASING SIZE (in): <u>7.625</u>	WITNESS: <u>ROB YOUNG</u>
ELEVATION (ft): <u>2475.0</u>	DRILLING CONTRACTOR: _____
TOTAL DEPTH (ft): <u>4910.0</u>	<u>MEREENIE RIG #1</u>
PACKER DEPTH(S) (ft): <u>4695. 4703</u>	
FINAL SURFACE CHOKE (in): <u>0.50000</u>	
BOTTOM HOLE CHOKE (in): <u>0.750</u>	
MUD WEIGHT (lb/gal): <u>8.30</u>	
MUD VISCOSITY (sec): <u>45</u>	
ESTIMATED HOLE TEMP. (°F): _____	
ACTUAL HOLE TEMP. (°F): <u>150 @ 4908.0 ft</u>	

FLUID PROPERTIES FOR RECOVERED MUD & WATER		
SOURCE	RESISTIVITY	CHLORIDES
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm

SAMPLER DATA
Pstg AT SURFACE: _____
cu.ft. OF GAS: _____
cc OF OIL: _____
cc OF WATER: _____
cc OF MUD: _____
TOTAL LIQUID cc: _____

HYDROCARBON PROPERTIES
OIL GRAVITY (°API): <u>57.8</u> @ <u>60</u> °F
GAS/OIL RATIO (cu.ft. per bbl): <u>567</u>
GAS GRAVITY: <u>0.987</u>

CUSHION DATA		
TYPE	AMOUNT	WEIGHT
_____	_____	_____
_____	_____	_____

RECOVERED:

FULL STRING OF OIL

NOTE: WELL PRODUCED AT A RATE OF 418 BARRELS OF OIL PER DAY WITH GOR OF 567 CUBIC FEET PER BARREL FROM FLOW PROVER.

MEASURED FROM TESTER VALVE

REMARKS:

LEGAL LOCATION: LAT. 24 DEG., 01', 33"S; LONG. 131 DEG., 36', 58"E.

TYPE & SIZE MEASURING DEVICE: 6" CERAMIC SURFACE CHOKE				TICKET NO: 34547800	
TIME	CHOKE SIZE	SURFACE PRESSURE PSI	GAS RATE MCF	LIQUID RATE BPD	REMARKS
3-22-86					
0930					MADE UP TOOL
1111					RAN IN HOLE
1418					HEAD UP
1424					SET PACKERS WITH 30000#
1428	.50				OPENED TOOL WITH WEAK BLOW
1430					MODERATE BLOW
1432					MODERATE TO STRONG BLOW
1433		1			STRONG BLOW
1436		2			GAS TO SURFACE
1440		1			MODERATE BLOW
1443		2			STRONG BLOW
1444		4			VERY STRONG BLOW
1445		4			
1446		3			
1447		3			STRONG BLOW
1448		2			CLOSED TOOL
1528	.50	1			OPENED TOOL WITH STRONG BLOW
1529		2			
1531		1			MODERATE BLOW
1533		1			MODERATE TO WEAK BLOW
1534					WEAK BLOW
1536					VERY WEAK BLOW
1544					EXTREMELY WEAK BLOW
1637		3			RAT HOLE MUD TO SURFACE
1639		10			
1641		32			
1644		70			OIL TO SURFACE
1645		90			
1647		100			
1649		115			
1652		118			
1653		120			
1655		115			
1700		105			
1709		90			
1717		90			CHANGED LINES AND WENT THROUGH

TICKET NO: 34547800
 CLOCK NO: 29491 HOUR: 24



GAUGE NO: 8511
 DEPTH: 4680.0

REF	MINUTES	PRESSURE	AP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	21.8			
2	2.0	63.8	42.0		
3	4.0	145.0	81.2		
4	6.0	229.7	84.7		
5	8.0	267.4	37.6		
6	10.0	247.2	-20.1		
7	12.0	252.6	5.4		
8	14.0	261.3	8.7		
9	16.0	273.2	11.8		
10	18.0	296.1	22.9		
C 11	18.9	303.9	7.9		
FIRST CLOSED-IN					
C 1	0.0	303.9			
2	1.0	437.9	133.9	1.0	1.293
3	2.0	600.9	297.0	1.8	1.014
4	3.0	865.1	561.2	2.6	0.862
5	4.0	1311.4	1007.4	3.3	0.756
6	5.0	1545.1	1241.2	4.0	0.679
7	6.0	1592.8	1288.8	4.6	0.617
8	7.0	1610.0	1306.0	5.1	0.569
9	8.0	1620.1	1316.1	5.6	0.528
10	9.0	1629.4	1325.4	6.1	0.491
11	10.0	1636.7	1332.8	6.5	0.461
12	12.0	1645.9	1342.0	7.3	0.410
13	14.0	1651.6	1347.6	8.1	0.370
14	16.0	1656.8	1352.9	8.7	0.338
15	18.0	1660.0	1356.0	9.2	0.312
16	20.0	1663.5	1359.6	9.7	0.289
17	22.0	1666.7	1362.7	10.2	0.269
18	24.0	1668.2	1364.3	10.6	0.252
19	26.0	1669.6	1365.6	10.9	0.237
20	28.0	1670.7	1366.8	11.3	0.224
21	30.0	1671.8	1367.8	11.6	0.212
22	35.0	1674.3	1370.3	12.3	0.187
D 23	37.4	1675.3	1371.4	12.6	0.177
SECOND FLOW					
E 1	0.0	385.3			
2	10.0	410.4	25.1		
3	20.0	484.9	74.5		
4	30.0	555.5	70.7		
5	40.0	624.7	69.2		
6	50.0	683.7	58.9		
7	60.0	737.6	53.9		
8	70.0	793.6	55.9		
<input type="checkbox"/> 9	77.1	816.1	22.5		

REF	MINUTES	PRESSURE	AP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND FLOW - CONTINUED					
10	80.0	804.3	-11.7		
11	90.0	715.8	-88.6		
12	100.0	635.0	-80.8		
13	110.0	576.4	-58.6		
14	120.0	534.2	-42.2		
15	130.0	504.7	-29.5		
16	140.0	475.8	-28.9		
17	150.0	453.3	-22.5		
18	160.0	436.3	-17.0		
19	170.0	422.5	-13.8		
20	180.0	412.1	-10.4		
F 21	183.8	407.0	-5.1		
SECOND CLOSED-IN					
F 1	0.0	407.0			
2	1.0	563.7	156.7	1.0	2.308
3	2.0	700.8	293.8	2.0	2.016
4	3.0	874.2	467.2	3.0	1.835
5	4.0	1333.7	926.7	3.9	1.712
6	5.0	1411.4	1004.4	4.9	1.615
7	6.0	1481.6	1074.6	5.8	1.543
8	7.0	1525.6	1118.6	6.7	1.479
9	8.0	1550.1	1143.2	7.7	1.420
10	9.1	1565.4	1158.4	8.7	1.368
11	10.0	1574.4	1167.4	9.5	1.328
12	12.0	1586.1	1179.1	11.3	1.254
13	14.0	1595.3	1188.3	13.1	1.189
14	16.0	1601.0	1194.1	14.9	1.135
15	18.0	1606.4	1199.5	16.5	1.088
16	20.0	1612.5	1205.5	18.2	1.047
17	22.0	1617.1	1210.1	19.9	1.008
18	24.0	1620.2	1213.2	21.5	0.975
19	26.0	1621.5	1214.5	23.0	0.945
20	28.0	1624.0	1217.0	24.6	0.916
21	30.0	1626.1	1219.1	26.1	0.890
22	35.0	1629.4	1222.4	29.8	0.832
23	40.0	1632.0	1225.0	33.4	0.783
24	45.0	1634.6	1227.7	36.8	0.740
25	50.0	1636.9	1229.9	40.1	0.704
26	55.0	1639.8	1232.8	43.3	0.671
27	60.0	1641.1	1234.1	46.3	0.641
28	70.0	1644.1	1237.1	52.0	0.591
29	80.0	1647.8	1240.8	57.4	0.548
30	90.0	1650.0	1243.0	62.3	0.512
31	100.0	1652.0	1245.0	67.0	0.481
32	110.0	1654.6	1247.6	71.3	0.454
33	120.0	1657.0	1250.0	75.4	0.430
34	135.0	1659.2	1252.2	81.0	0.398
35	150.0	1660.9	1253.9	86.2	0.371
36	165.0	1663.5	1256.5	91.0	0.348
37	180.0	1665.1	1258.1	95.4	0.328

LEGEND:
 MAXIMUM FLOW PRESSURE
 REMARKS:

TICKET NO: 34547800

CLOCK NO: 29491 HOUR: 24



GAUGE NO: 8511

DEPTH: 4680.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND CLOSED-IN - CONTINUED					
38	195.0	1665.7	1258.8	99.4	0.309
39	210.0	1666.9	1260.0	103.1	0.293
40	225.0	1668.1	1261.1	106.6	0.279
41	240.0	1669.2	1262.2	109.9	0.266
42	255.0	1670.3	1263.4	112.9	0.254
43	270.0	1670.5	1263.5	115.8	0.243
44	285.0	1671.4	1264.4	118.4	0.233
45	300.0	1672.0	1265.1	121.0	0.224
46	315.0	1673.0	1266.0	123.3	0.216
47	330.0	1673.5	1266.5	125.6	0.208
48	345.0	1673.9	1266.9	127.7	0.201
49	360.0	1674.7	1267.7	129.7	0.194
50	375.0	1675.2	1268.2	131.6	0.188
51	390.0	1675.3	1268.4	133.4	0.182
G 52	405.9	1676.6	1269.7	135.2	0.176

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$

LEGEND:

 MAXIMUM FLOW PRESSURE

REMARKS:

TICKET NO: 34547800
 CLOCK NO: 29475 HOUR: 24



GAUGE NO: 8531
 DEPTH: 4907.0

REF	MINUTES	PRESSURE	AP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	123.3			
2	2.0	232.0	108.7		
3	4.0	317.7	85.7		
4	6.0	366.9	49.2		
5	8.0	338.3	-28.5		
6	10.0	322.1	-16.3		
7	12.0	332.4	10.4		
8	14.0	338.6	6.2		
9	16.0	352.2	13.6		
10	18.0	373.9	21.6		
C 11	18.9	383.8	10.0		
FIRST CLOSED-IN					
C 1	0.0	383.8			
2	1.0	503.6	119.8	1.0	1.287
3	2.0	638.4	254.6	1.8	1.020
4	3.0	832.5	448.6	2.6	0.860
5	4.0	1264.9	881.0	3.3	0.753
6	5.0	1608.0	1224.2	3.9	0.680
7	6.0	1673.0	1289.1	4.6	0.617
8	7.0	1693.9	1310.1	5.1	0.570
9	8.0	1710.8	1327.0	5.6	0.526
10	9.0	1717.3	1333.5	6.1	0.492
11	10.0	1725.4	1341.5	6.5	0.461
12	12.0	1736.3	1352.5	7.3	0.411
13	14.0	1742.7	1358.8	8.0	0.372
14	16.0	1748.3	1364.5	8.7	0.338
15	18.0	1752.7	1368.8	9.2	0.312
16	20.0	1755.4	1371.5	9.7	0.289
17	22.0	1757.7	1373.9	10.2	0.269
18	24.0	1760.0	1376.2	10.6	0.252
19	26.0	1761.5	1377.7	10.9	0.237
20	28.0	1763.5	1379.7	11.3	0.224
21	30.0	1764.9	1381.1	11.6	0.212
22	35.0	1768.0	1384.2	12.3	0.187
D 23	37.4	1768.0	1384.2	12.6	0.177
SECOND FLOW					
E 1	0.0	446.6			
2	10.0	489.2	42.6		
3	20.0	564.1	74.9		
4	30.0	633.7	69.6		
5	40.0	697.1	63.4		
6	50.0	753.8	56.7		
7	60.0	811.0	57.2		
8	70.0	864.8	53.8		
<input type="checkbox"/> 9	77.1	891.9	27.2		

REF	MINUTES	PRESSURE	AP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND FLOW - CONTINUED					
10	80.0	882.3	-9.6		
11	90.0	792.9	-89.4		
12	100.0	703.6	-89.3		
13	110.0	642.1	-61.6		
14	120.0	605.8	-36.2		
15	130.0	576.9	-29.0		
16	140.0	550.1	-26.7		
17	150.0	523.8	-26.3		
18	160.0	505.0	-18.8		
19	170.0	489.0	-16.0		
20	180.0	476.0	-13.1		
F 21	183.8	472.8	-3.2		
SECOND CLOSED-IN					
F 1	0.0	472.8			
2	1.0	595.3	122.5	1.0	2.297
3	2.0	719.4	246.6	1.9	2.018
4	3.0	867.0	394.2	2.9	1.842
5	4.0	1156.5	683.8	3.9	1.711
6	5.0	1417.5	944.7	4.8	1.622
7	6.0	1515.6	1042.9	5.8	1.545
8	7.0	1587.7	1115.0	6.8	1.474
9	8.0	1622.7	1149.9	7.7	1.422
10	9.0	1641.1	1168.4	8.7	1.370
11	10.0	1651.8	1179.1	9.5	1.329
12	12.0	1668.9	1196.1	11.3	1.253
13	14.0	1680.1	1207.4	13.1	1.190
14	16.0	1686.1	1213.3	14.8	1.136
15	18.0	1691.8	1219.1	16.5	1.089
16	20.0	1696.8	1224.0	18.2	1.046
17	22.0	1699.7	1227.0	19.9	1.009
18	24.0	1701.7	1228.9	21.5	0.975
19	26.0	1704.2	1231.5	23.0	0.945
20	28.0	1706.2	1233.4	24.6	0.916
21	30.1	1708.3	1235.6	26.2	0.889
22	35.0	1712.3	1239.5	29.8	0.832
23	40.0	1715.8	1243.0	33.4	0.783
24	45.0	1718.2	1245.4	36.8	0.741
25	50.0	1720.4	1247.7	40.1	0.704
26	55.0	1722.0	1249.2	43.3	0.671
27	60.0	1724.1	1251.3	46.3	0.641
28	70.1	1728.3	1255.6	52.1	0.590
29	80.0	1731.5	1258.8	57.4	0.548
30	90.0	1734.5	1261.8	62.3	0.512
31	100.0	1736.5	1263.7	67.0	0.481
32	110.0	1740.0	1267.2	71.3	0.454
33	120.0	1742.0	1269.2	75.4	0.430
34	135.0	1743.9	1271.2	81.0	0.398
35	150.0	1745.5	1272.7	86.2	0.371
36	165.0	1747.6	1274.9	90.9	0.348
37	180.0	1749.4	1276.7	95.3	0.328

LEGEND: MAXIMUM FLOW PRESSURE
 REMARKS:


























TICKET NO: 34547800
 CLOCK NO: 29475 HOUR: 24



GAUGE NO: 8531
 DEPTH: 4907.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$	REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND CLOSED-IN - CONTINUED											
38	195.0	1750.8	1278.1	99.4	0.310						
39	210.0	1752.1	1279.4	103.2	0.293						
40	225.0	1753.1	1280.3	106.6	0.279						
41	240.0	1753.7	1280.9	109.9	0.266						
42	254.9	1754.9	1282.2	112.9	0.254						
43	270.0	1755.8	1283.0	115.8	0.243						
44	285.0	1757.2	1284.4	118.5	0.233						
45	300.0	1757.9	1285.1	121.0	0.224						
46	315.0	1758.7	1286.0	123.3	0.216						
47	330.0	1759.4	1286.7	125.6	0.208						
48	345.0	1760.1	1287.4	127.7	0.201						
49	360.0	1760.8	1288.1	129.7	0.194						
50	375.0	1761.4	1288.7	131.6	0.188						
51	390.0	1762.0	1289.2	133.4	0.182						
G 52	405.9	1763.7	1290.9	135.2	0.176						

LEGEND:
 MAXIMUM FLOW PRESSURE
 REMARKS:

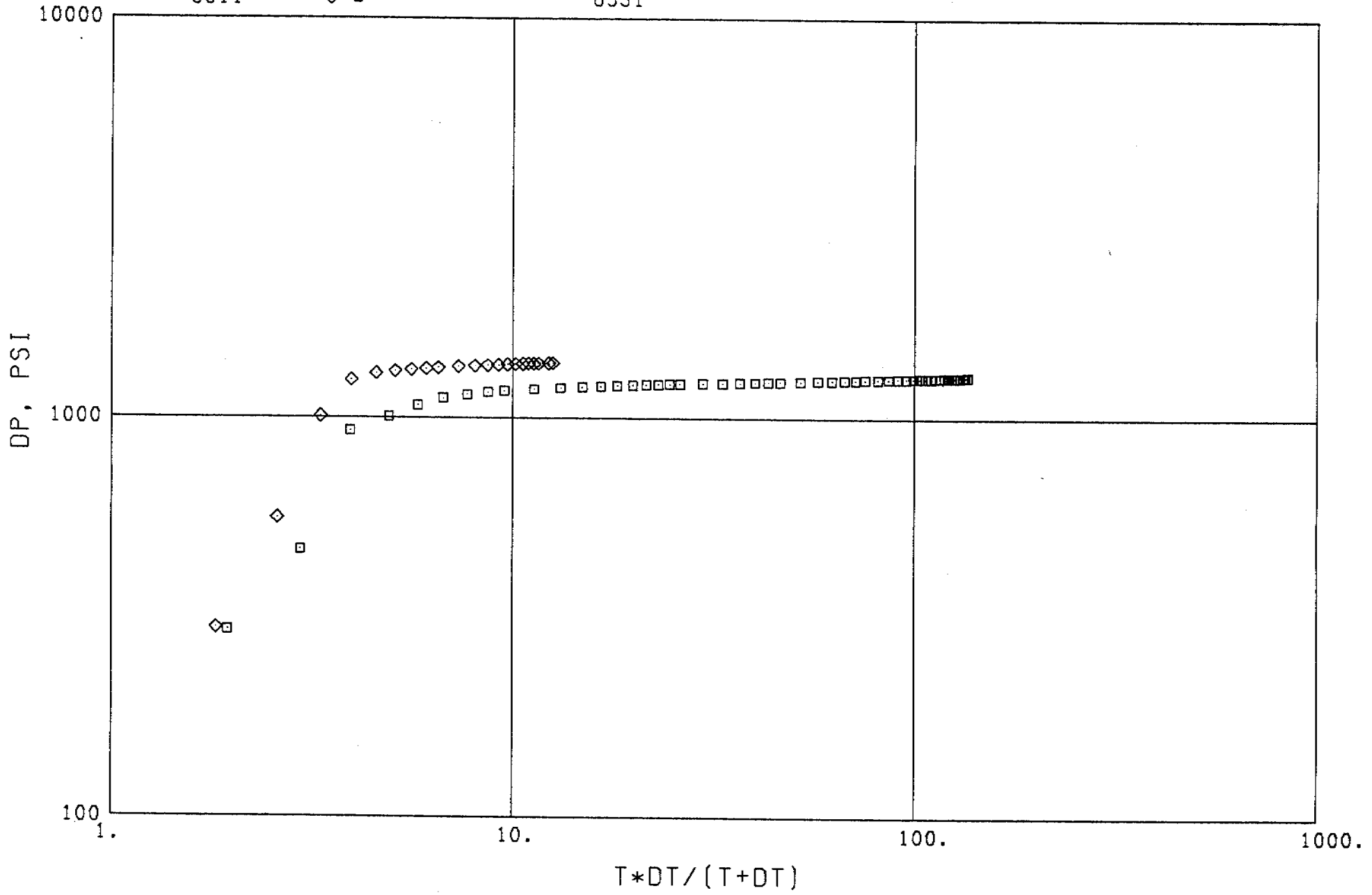
		O.D.	I.D.	LENGTH	DEPTH	
1		DRILL PIPE.....	4.500	3.826	4070.1	
4		FLEX WEIGHT.....	4.500	2.764	182.3	
3		DRILL COLLARS.....	6.250	2.375	335.9	
9		STABILIZER.....	6.438	2.375	6.5	
3		DRILL COLLARS.....	6.250	2.375	29.6	
50		IMPACT REVERSING SUB.....	6.250	3.000	1.0	4624.4
3		DRILL COLLARS.....	6.250	2.375	31.2	
9		STABILIZER.....	6.438	2.313	6.6	
258		BAR CATCHER SUB	6.250	1.000	1.0	4664.0
12		DUAL CIP VALVE.....	5.000	0.870	4.9	
202		SAMPLE CHAMBER.....	5.000	2.250	4.1	
60		HYDROSPRING TESTER.....	5.000	0.750	5.3	4678.0
80		AP RUNNING CASE.....	5.000	2.250	4.1	4680.0
15		JAR.....	5.000	1.750	5.0	
16		VR SAFETY JOINT.....	5.000	1.000	2.8	
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	4695.1
18		DISTRIBUTOR VALVE.....	5.000	1.680	2.0	
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	4702.9
19		ANCHOR PIPE SAFETY JOINT.....	5.000	1.500	4.3	
5		CROSSOVER.....	6.250	2.200	1.0	
47		PUP JOINT.....	4.500	3.000	10.0	
9		DRILL COLLARS.....	6.250	2.375	152.5	
5		CROSSOVER.....	6.250	2.250	1.0	
20		FLUSH JOINT ANCHOR.....	5.000	2.370	33.0	
81		BLANKED-OFF RUNNING CASE.....	5.000		4.1	4907.0
TOTAL DEPTH						4910.0

EQUIPMENT DATA

TICKET NO 34547800

GAUGE NO CIP 1 2
8511 ◇ □

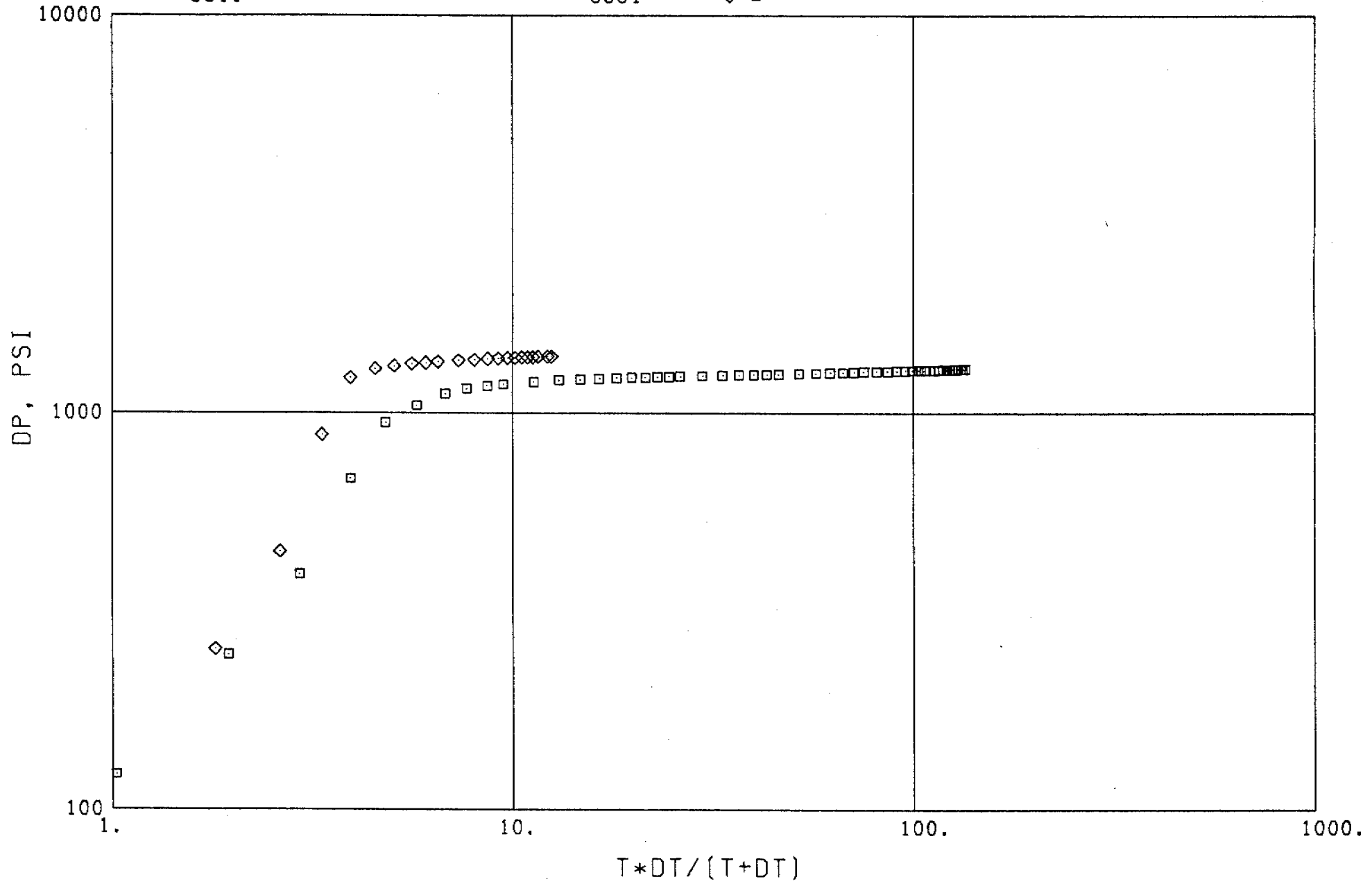
GAUGE NO CIP 1 2
8531



TICKET NO 34547800

GAUGE NO CIP 1 2
8511

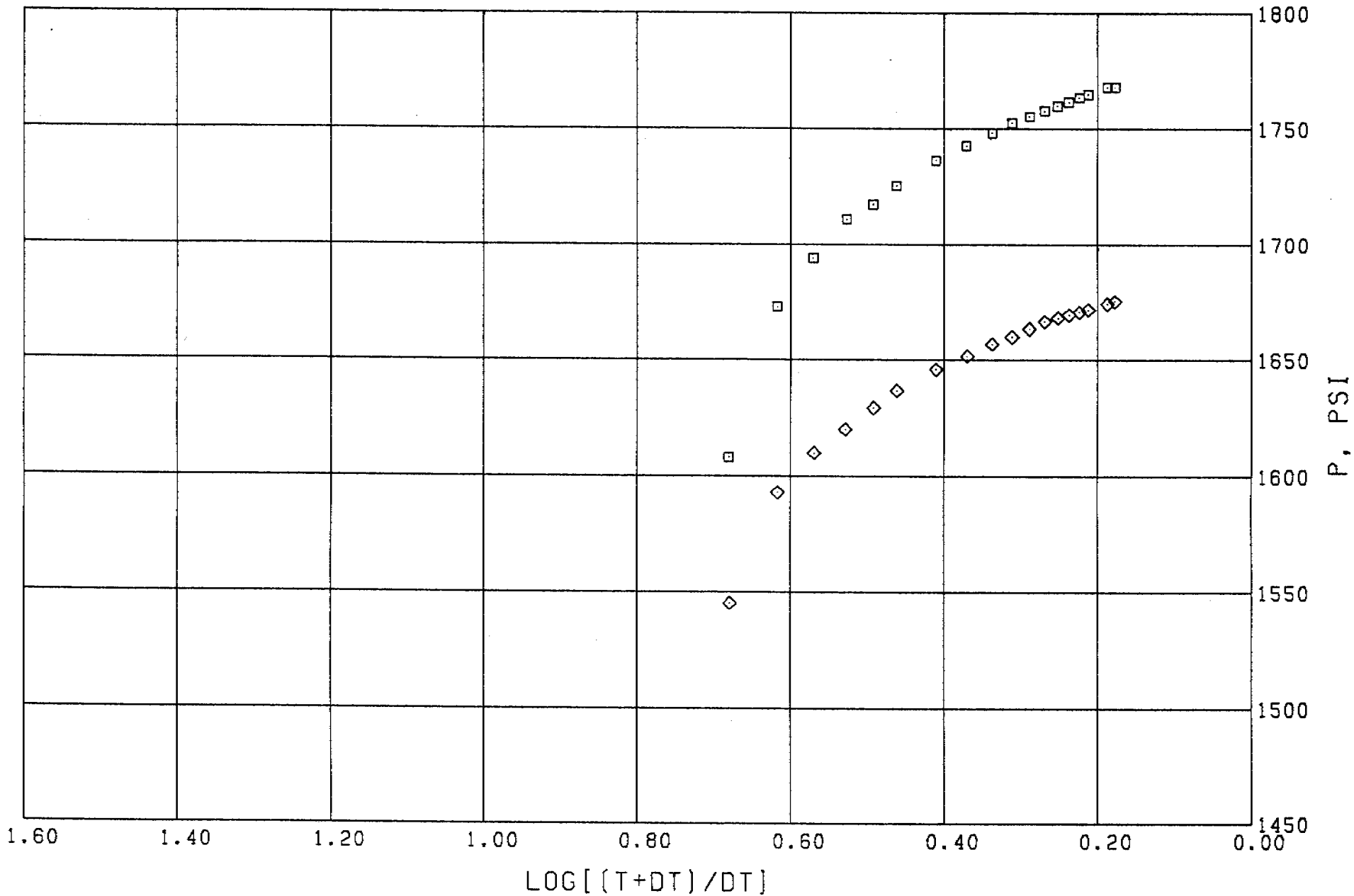
GAUGE NO CIP 1 2
8531 \diamond \square



GAUGE NO 8511 CIP 1 2
◇

GAUGE NO 8531 CIP 1 2
□

TICKET NO 34547800

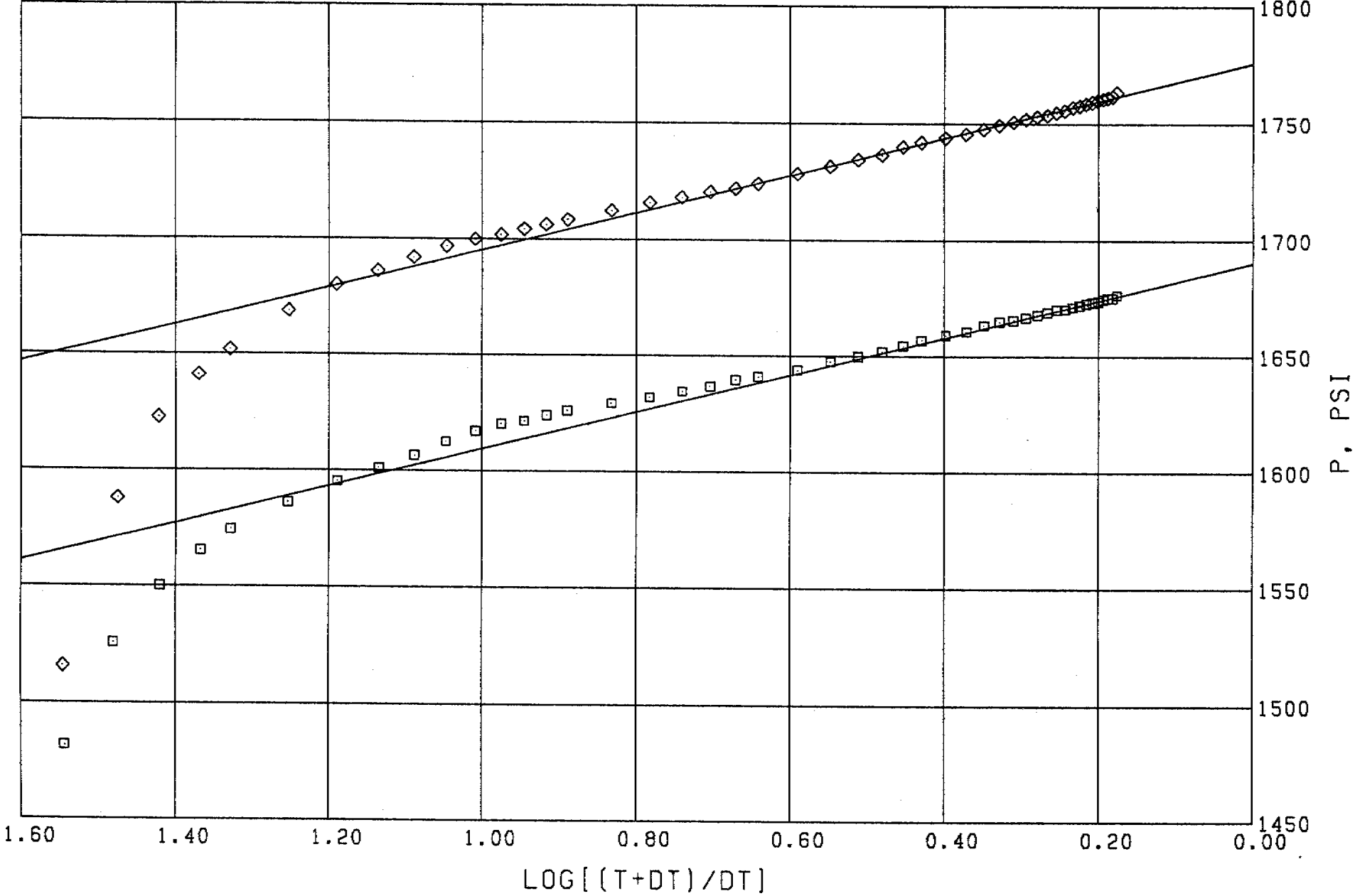


02
03
00

TICKET NO 34547800

GAUGE NO CIP 1 2
8511 □

GAUGE NO CIP 1 2
8531 ◇



0.93

TICKET NUMBER 34547800

SUMMARY OF RESERVOIR PARAMETERS USING HORNER METHOD FOR LIQUID WELLS

OIL GRAVITY	57.8	°API@60°F	WATER SALINITY	0.0	% SALT
GAS GRAVITY	0.987		FLUID GRADIENT	0.3239	psi/ft
GAS/OIL RATIO	567.0	SCF/STB	FLUID PROPERTIES AT	1776.1	psig
TEMPERATURE	150.0	°F	VISCOSITY	0.321	cp
NET PAY	0.0	ft	FMT VOL FACTOR	1.305	Rvol/Svol
POROSITY	10.0	%	SYSTEM COMPRESSIBILITY	13.38	$\times 10^{-6}$ vol/vol/psi
PIPE CAPACITY FACTORS					bbl/ft

GAUGE NUMBER	8511	8531					
GAUGE DEPTH	4680.0	4907.0					
FLOW AND CIP PERIOD	2	2					UNITS
FINAL FLOW PRESSURE P_f	407.0	472.8					psig
TOTAL FLOW TIME t	202.7	202.7					min
EXTRAPOLATED PRESSURE P^*	1690.3	1776.1					psig
ONE CYCLE PRESSURE	1609.4	1695.1					psig
PRODUCTION RATE Q	418.0	418.0					BPD
TRANSMISSIBILITY kh/μ	1095.5	1095.5					$\frac{md-ft}{cp}$
FLOW CAPACITY kh	351.515	351.515					md-ft
PERMEABILITY k	1.69732	1.69732					md
SKIN FACTOR S	12.6	12.9					
DAMAGE RATIO DR	3.3	3.3					
POTENTIAL RATE Q_1	1364.5	1386.0					BPD
RADIUS OF INVESTIGATION r_t	117.0	117.0					ft

REMARKS: ANALYSIS WAS PERFORMED BY USING THE REPORTED PRODUCTION RATE OF 418 BBL./DAY AND REPORTED GAS/OIL RATIO OF 567 CU. FT. PER BBL.
 THE ENTIRE TESTED INTERVAL OF 207 FEET WAS USED AS FORMATION THICKNESS DUE TO THE LACK OF A REPORTED NET PAY.
 THE PLOTS INDICATE THE POSSIBILITY OF A PERMEABILITY ANOMALY WITHIN THE TESTED INTERVAL.

NOTICE: THESE CALCULATIONS ARE BASED UPON INFORMATION FURNISHED BY YOU AND TAKEN FROM DRILL STEM PRESSURE CHARTS, AND ARE FURNISHED YOU FOR YOUR INFORMATION. IN FURNISHING SUCH CALCULATIONS AND EVALUATIONS BASED THEREON, HALLIBURTON IS MERELY EXPRESSING ITS OPINION. YOU AGREE THAT HALLIBURTON MAKES NO WARRANTY EXPRESS OR IMPLIED AS TO THE ACCURACY OF SUCH CALCULATIONS OR OPINIONS, AND THAT HALLIBURTON SHALL NOT BE LIABLE FOR ANY LOSS OR DAMAGE, WHETHER DUE TO NEGLIGENCE OR OTHERWISE, IN CONNECTION WITH SUCH OPINIONS.

EQUATIONS FOR DST LIQUID WELL ANALYSIS

Transmissibility	$\frac{kh}{\mu} = \frac{162.6 QB}{m}$	$\frac{\text{md-ft}}{\text{cp}}$
Indicated Flow Capacity	$kh = \frac{kh}{\mu} \mu$	md-ft
Average Effective Permeability	$k = \frac{kh}{h}$	md
Skin Factor	$S = 1.151 \left[\frac{P^* - P_f}{m} \cdot \text{LOG} \left(\frac{k(t/60)}{\phi \mu c_f r_w^2} \right) + 3.23 \right] -$	—
Damage Ratio	$DR = \frac{P^* - P_f}{P^* - P_f - 0.87 mS}$	—
Theoretical Potential w / Damage Removed	$Q_1 = Q DR$	BPD
Approx. Radius of Investigation	$r_i = 0.032 \sqrt{\frac{k(t/60)}{\phi \mu c_i}}$	ft

EQUATIONS FOR DST GAS WELL ANALYSIS

Indicated Flow Capacity	$kh = \frac{1637 Q_g T}{m}$	md-ft
Average Effective Permeability	$k = \frac{kh}{h}$	md
Skin Factor	$S = 1.151 \left[\frac{m(P^*) - m(P_f)}{m} \cdot \text{LOG} \left(\frac{k(t/60)}{\phi \mu c_f r_w^2} \right) + 3.23 \right] -$	—
Damage Ratio	$DR = \frac{m(P^*) - m(P_f)}{m(P^*) - m(P_f) - 0.87 mS}$	—
Indicated Flow Rate (Maximum)	$AOF_1 = \frac{Q_g m(P^*)}{m(P^*) - m(P_f)}$	MCFD
Indicated Flow Rate (Minimum)	$AOF_2 = Q_g \sqrt{\frac{m(P^*)}{m(P^*) - m(P_f)}}$	MCFD
Approx. Radius of Investigation	$r_i = 0.032 \sqrt{\frac{k(t/60)}{\phi \mu c_i}}$	ft