EAST MEREENIE NO. 26

WELL COMPLETION REPORT

PETROLEUM LEASE NO. 5, NORTHERN TERRITORY

BY

MOONIE OIL N.L.

MAY 1986



RESOLUL B NORTHERN TERRITORY GEOLOGICAL SURVEY

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S U M M A R Y

SUMMARY

East Mereenie No. 26 is the twenty seventh well in the current Mereenie Field Appraisal and Development Programme. It was designed to be completed for oil production from the P1-80 reservoir, which flowed oil in East Mereenie Nos. 6, 8 and 24.

Further information on prospective Stairway Sandstone horizons was obtained, by coring the LS-160 sand and conducting two Drill Stem Tests. An evaluation of the oil/water contact in the lower Pl was also conducted.

East Mereenie No. 26 is located 930 metres on a true bearing of 19 degrees from East Mereenie No. 8, and 1375 metres on a true bearing of 123 degrees from East Mereenie No. 9. East Mereenie No. 26 is an eastern nose, northern flank well.

The well spudded into Parke Siltstone on the 16th December 1985 using 0.D. & E. Rig No. 19, and reached TD at 5088 ft on the 19th January 1986 in the Pacoota (P2) Sandstone. The main producing reservoir horizon, the P1-80 sand, was intersected at -2462 ft MSL.

The well was drilled to 3000 ft with air foam. Returns of meteoric water began at 151 ft, with 1200 bbls/hr recorded at 1370 ft. An average rate of 2200 bbls/hr was recorded from 2000 ft to 3000 ft. After 8-5/8" casing had been set, drilling continued with air in 7-5/8" hole to 4340 ft, approximately 50 ft above the LS-160 sand interval. At this point the hole was displaced with an invert emulsion oil based mud of 10.1 ppg. The 7-5/8" hole was drilled to TD at 5088 ft with the mud weight being reduced from a maximum of 10.4 ppg at 4783 ft to 9.5 ppg at 4857 ft.

Wireline logs were run at TD 5088 ft, and 5-1/2" casing run and set at 5086 ft.

Four Drill Stem Tests were run in East Mereenie No. 26. Drill Stem Test No. 1 and No. 2 (4398 to 4426 ft, 4426 to 4459 ft, respectively), were conducted to evaluate the Lower Stairway LS-160 sand interval. Both tests produced no fluids to surface and were valid tests in a very poorly permeable formation. Drill Stem Test No. 3 (4758 to 4783 ft), tested the P1-80 sand and flowed 694 BOPD and 440 MCFD of gas through a 0.5" choke, with a G.O.R. of 635 cuft/bbl. Drill Stem Test No. 4 (5029 to 5088 ft), tested the P1-350 sand and produced no fluids to surface, with 8 bbls of oil cut rat hole mud recovered during the reverse circulation. This was a valid test in a poorly permeable formation.

Four cores were cut in East Mereenie No. 26, each cored interval being followed by a Drill Stem Test. Core No. 1 and No. 2 were cut in the Lower Stairway LS-160 sand. Core No. 3 and No. 4 were cut in the P1-80 sand and P1-350 sand, respectively. Recovery was 100% in the Lower Stairway, with 98% and 99% in the P1 intervals.

2-3/8" production tubing was run at TD, with a Guiberson packer and a Gearhart tubing conveyed perforating assembly. The packer was set at 4494 ft and the casing perforated between 4767 to 4777 ft with the well in an under-balanced condition. No immediate flow occurred to surface, and Gearhart swabbed the well in (fluid level was at 300 ft). A clean up to flow test was then conducted with a flow of 672 BOPD, and 427 MCFD through a 0.5" choke, with a G.O.R. of 635 cuft/bbl.

East Mereenie No. 26 was completed as an oil producing well from the P1-80 sand horizon. The rig was released at 1200 hrs on the 24th January 1986, having taken 40 days from spud to completion.

1. GENERAL DATA

1. GENERAL DATA:

Well Name & Number:

East Mereenie No. 26

Operator:

Moonie Oil N.L.

Beneficial Interst

<u>Holders</u>:

The Moonie Oil Company Limited

Flinders Petroleum N.L.

Magellan Petroleum Australia Limited

Petroleum Title:

Petroleum Lease No. 5

District:

Alice Springs, Northern Territory

Location:

Latitude:

24°03'12"S

Longitude:

131°40'13"E

Elevation:

Ground Level: 2293 ft MSL Not Surveyed Kelly Bushing: 2306 ft MSL Not Surveyed

Total Depth:

5088 ft (DRILLER) 5088 ft (LOGGER)

Spudded:

16th December 1985, 0230 hours

Rig Released:

24th January 1986, 1200 hours

Total Days Drilling:

40 days

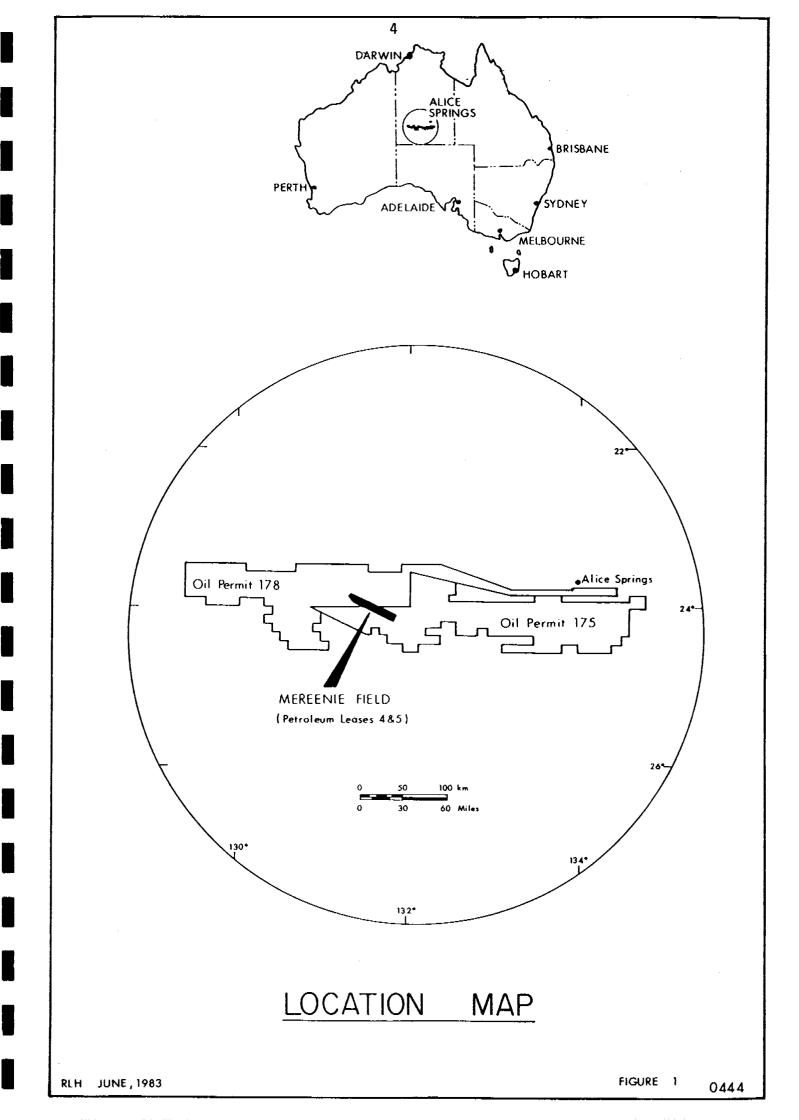
Well Status:

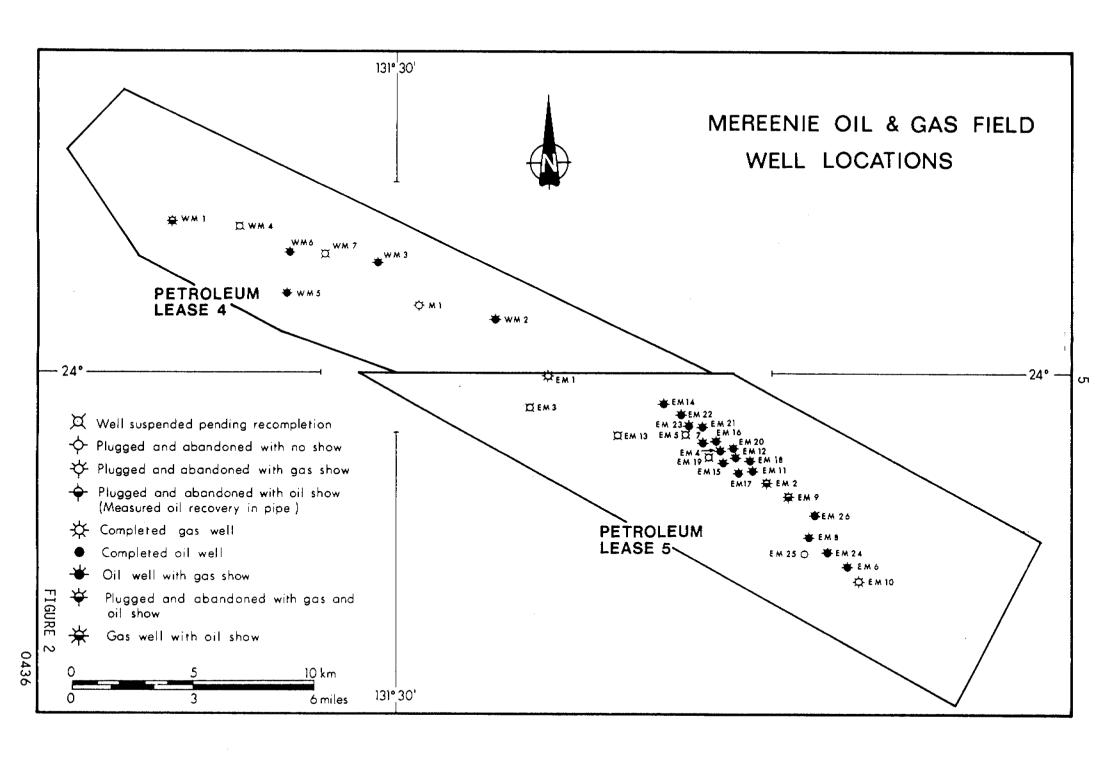
Completed Oil Well

Geological Formation

Tops:

Parke Siltstone Surface 706 ft Mereenie Sandstone 2373 ft Carmichael Sandstone Stokes Siltstone 2614 ft 3692 ft Stairway Sandstone Horn Valley Siltstone 4462 ft Pacoota Sandstone 4690 ft





2. ENGINEERING DATA

2. ENGINEERING DATA:

2.1 Rig Data:

Drilling Contractor: 0.D. & E. Drilling Contractor Rig: Rig 19

Drilling Plant: Ma

Make: KREMCO

Type:

K600H

Rated

Capacity: 7500 ft

Motors:

GM 8V92TA

Mast:

Make:

KREMCO

Type:

109 FT

Rated

Capacity:

270000 1bs

Pumps:

Make 1: Gardner Denver PZ-7/550HP

Make 2: Gardner Denver PAHBFC/275HP

Type:

TRIPLEX

Size 1:

 $7'' \times 5-1/2''$

Size 2:

8" x 5"

Rotary Table:

Make:

IDECO SR-175

Capacity:

325 Tons

Blowout preventors:

Make 1:

NL Shaffer Spherical

Make 2:

11" 5000 psi NL Shaffer LWS

11" 5000 psi

Size:

11"

Rating (psi)

5000

Choke Manifold:

Make:

0 w n

Size & Type:

5000 psi with 1×3 " positive and 1×3 "

adjustable choke

Mud Tanks:

Size & Capacity: Suction Tank - 317 BBL Shaker Tank - 271 BBL

- 33 BBL Trip Tank

Shale Shaker:

Make:

Harrisburg

Type:

Single Dual Deck

Mud Mixers:

Make:

Harrisburg

Type:

8" x 6" Centrifugal

Desander:

Make:

DSN-1000

Capacity:

800 GPM

Mud Cleaner:

Make

Harrisburg

Model:

MC800

Capacity: 800 GFM

Drill pipe:

7000 16.6 lbs/ft 'E' 4-1/2" OD W/- 4"

IF Conx.

Drill collars:

6 x 8"

 $24 \times 6 - 1/2$ "

Air drilling equipment:

Air compressors:

Make 1:

Gardner Denver

Make 2:

Sullair

Model 1:

WEN

Model 2:

900/350

Capacity 1:

860 CFM/350 PSI

Capacity 2:

900 CFM/350 PSI

Air compressor

booster:

Make:

Gardner Denver

Model:

RLD

Capacity:

To 1000 PSI

Diverter: Make:

ke: Grant

Model:

70685

Injection pumps:(1)

Make:

Gardner Denver P.A.H.

Model:

Triplex HP

Capacity:

300 GPM

(2) Make:

Gardner Denver PZ7

Model:

PZ7 Triplex

Capacity:

300 GPM

2.2 Drilling Data:

The following is a summary of relevant drilling activities on a day by day basis. Figure 3 is the annotated time/depth curve.

DATE	E.T.D. (FT)	DETAILS OF OPERATIONS, DESCRIPTIONS AND RESULTS
16/12/85	97	Move rig to new lease and rig up. Dig rat hole, spud 17.5" hole @ 0230 hours and drill with air to 47 ft. Pick up square drill collar, drill 17-1/2" hole to 97 ft.
17/12/75	151	Drill 17-1/2" hole to 151 ft with air and foam. POH, run 15" conductor pipe to 144 ft and cement with 46 sacks of class A cement. Install rotating BOP, rig up Blooey line.
18/12/85	623	Lay out hammer and square drill collar. Make up new bit No. 2, hammer, 3 X 8" drill collars. Tag cement @ 139 ft, drill out cement and ream to 151 ft. Air drill with 11" bit to 169 ft, change to air and foam. Drill 11" hole to 600 ft, loss of returns, work pipe and break up bridge @ 590 ft. Drill 11" hole to 623 ft. Foam injection rate 12 to 15 bbls/hr.
19/12/85	1105	Mist drill 11" hole to 872 ft, pull rotating head rubber. POH. Lay out hammer and make up New Bit No. 3 and shock sub. RIH and mist drill 11" hole to 1105 ft. Foam injection rate 12 to 15 bbls/hr.
20/12/85	1628	Drill 11" hole with air and foam to 1628 ft. Foam injection rate 8 to 10 bbls/hr.
21/12/85	1877	Mist drill 11" hole to 1854 ft. Blow hole clean and POH. Lay out 6 X 6-1/2" drill collars. Change bit and gauge stabilizers. RIH and pick up 3 x 6-1/2" drill collars and 6 x heavy weight drill pipe. RIH to shoe, slip and cut drilling line. RIH with new bit No. 4 and ream from 1817 to 1854 ft. Drill 11" hole with air and foam to 1877 ft. Foam injection rate 10 bbls/hr.
22/12/85	2145	Mist drill ll" hole to 2145 ft. Foam injection rate 8 bbls/hr.

23/12/85	2240	Drill 11" hole with air and foam to 2179 ft. Blow hole clean and POH. Lay out 5 x 6-1/2" drill collars. Change stabilizer rubbers and bit. Pick up 5 x 6-1/2" drill collars, lay out 3 joints drill pipe. RIH with new bit No. 5 to 2088 ft, unload hole and ream from 2088 ft to 2179 ft. Drill 11" hole to 2240 ft. Foam injection rate 8 bbls/hr.
24/12/85	2379	Mist drill 11" hole to 2379 ft. Blow hole clean and POH. Make up new bit No. 6 and RIH to 2307 ft. Slip 15 ft drilling line, unload hole and ream to 2379 ft.
25/12/85	2622	Drill 11" hole to 2622 ft. Blow hole clean and POH. Make up new bit No. 7, check float and service bit sub. Change bottom stabilizer and RIH.
26/12/85	3000	Unload hole and mist drill 11" hole from 2622 ft to 3000 ft. Blow hole clean. Pump pill, and chase with water. Strap out of the hole.
27/12/85	3000	Run 8-5/8" casing to 2988 ft circulate through casing and cement with 161 sacks of Class A cement plus 0.2% HR-4. Displace cement and bump plug to 1000 psi. Weld conductor to casing, slack off and cut casing. Install BOPs, pressure test blind rams and choke manifold. RIH with new bit No. 8.
28/12/85	3300	Tag plug at 2954 ft, drill out cement plug and float to 2980 ft, pressure test hydril and pipe rams. Drill to 3010 ft drying hole, drill 7-5/8" hole to 3300 ft with air.
29/12/85	3776	Drill 7-5/8" hole to 3776 ft. POH to change bit. RIH with Bit No. 9, air drill $7-5/8$ " hole to 3776 ft.
30/12/85	4288	Air drill $7-5/8$ " hole to 4340 feet. Displace hole with oil based mud. Drill $7-5/8$ " hole to 4288 ft.
31/12/85	4401	Drill 7-5/8" hole to 4401 ft. Circulate, pump pill, POH, remove rotating head and nipple up flow line. Pick up core barrel and RIH.
1/1/86	4412	Run in hole with core barrel, wash to bottom (27 ft), space out and cut Core No. 1. from 4401 ft to 4412 ft.
2/1/86	4426	Cut Core No. 1, from 4412 ft to 4426 ft. POH to recover core, 100% recovery. Pick up tools for DST No. 1.

3/1/86	4426	Pick up tools for DST No. 1, RIH to shoe, make up head and conduct test between 4397.6 ft to 4426 ft, over LS-160 sand. Open tool initially for 40 mins due to drill pipe slips failure, and close for 80 mins. Open tool for second flow 133 mins and close for 269 mins. No gas or oil to surface. Field chart readings:- IHP IFP ISIP FFP FSIP FHP BHT 2339 45.5 68.2 55.2 81.2 2336 139°F Drop bar, reverse circulate. POH, break head and
		surface lines, POH with tools and lay out. Make up junk sub and near bit reamer due to the loss of a tong die down the hole. RIH to shoe.
4/1/86	4429	RIH with re-run bit No. 9, junk sub and near bit reamer, wash and ream from 4377 ft to 4426 ft. Drill and work junk sub to 4429 ft. POH, and make up core barrel. RIH.
5/1/86	4445	Cut Core No. 2 from 4429 ft to 4445 ft.
6/1/86	4459	Cut Core No. 2 from 4445 ft to 4459 ft, pump pill POH and recover core, 100% recovery, make up DST tools.
7/1/86	4459	Make up tools for DST No. 2. RIH. Make up test head and conduct test over interval 4425.6 ft to 4459 ft in the LS-160 sand. Open tool initially for 20 mins and close for 40 mins. Open tool for second flow 90 mins and close for 220 mins. No oil or gas to surface. Field chart readings:-
		IHP IFP ISIP FFP FSIP FHP BHT 2447.5 35.7 55.2 45.2 77.9 2431.5 139°F
	•	Pull free, drop bar, reverse circulate for 1 hour, pump pill, lay out test head and POH.
8/1/86	4550	Lay out test tools. Make up new bit No. 10 and near bit reamer. RIH to shoe, slip 15 ft drilling line. RIH to 4399 ft, ream to 7-5/8" hole from 4399 ft to 4459 ft. Drill 7-5/8" hole to 4550 ft.
9/1/86	46 47	Drill 7-5/8" hole to 4647 ft. Drop survey, pump pill, POH.
10/1/86	4763	POH. Retrieve survey, break out bit and make up new bit No. 11 and near bit reamer. RIH. Wash from 4590 ft to 4647 ft. Drill 7-5/8" hole to 4763 ft.

		-1 DON
11/1/86	4772	Circulate bottoms up, drop survey, pump pill, POH. Break out bit and retrieve survey. Service and make up core barrel. RIH. Cut Core No. 3 with 7-19/32" core head from 4763 ft to 4772 ft.
12/1/86	4783	Cut Core No. 3 from 4772 ft to 4783 ft. Break off, pump pill and POH. Break out core, 98% recovery. Pick up DST tools.
13/1/86	4783	Make up and RIH with test tools for DST No. 3. Rig up test head. Tool opened with immediate strong blow for 20 minutes. (GTS in 15 min), and shut in for 40 minutes. Final flow 120 minutes and final shut in 280 min. OTS after 28 min, clean up and direct to separator for 75 min. Flow rate 694 BOPD, gas flow rate 440 MCFD through a 1/2" choke, GOR of 635 cu ft/bbl. Field chart readings:
		IHP IFP ISIP FFP FSIP FHP BHT 2631.7 649.7 1805.4 872.6 1821.2 2590.5 141°F
		Drop bar, reverse circulate, POH. Lay out test tools, make up new bit No. 13 and RIH.
14/1/86	4834	RIH with $7-5/8$ " bit, pick up kelly, circulate and ream 30 ft to 4783 ft. Circulate gas bubble out. Drill $7-5/8$ " from 4783 ft to 4834 ft.
15/1/86	4902	Drill 7-5/8" hole from 4834 ft to 4879 ft with oil base mud. Circulate and drop survey, POH. Retrieve survey, make up new bit No. 13 and near bit reamer. RIH, breaking circulation at shoe. Tag bottom and drill 7-5/8" hole from 4879 ft to 4902 ft.
16/1/86	5003	Drill 7-5/8" hole from 4902 ft to 5003 ft with oil base mud.
17/1/86	5028	Drill 7-5/8" hole from 5003 ft to 5028 ft. Pump pill and drop survey. POH, retrieve survey. Make up new bit No. 14 and junk sub, previous bit had broken teeth and 3/16" undergauge. RIH to shoe and break circulation. RIH and ream 20 ft to bottom, pump pill, POH. Make up core bit and barrel and RIH.
18/1/86	5057	RIH with core barrel. Slip and cut line at shoe, RIH. Pick up kelly and tag bottom. Cut Core No. 4 from 5028 ft to 5057 ft.

19/1/86 5088 Cut Core No. 4 from 5057 ft to 5058 ft. Break off, pump pill and POH. Recover core (99%) and lay out jars and subs. Make up re-run bit No. 14 and near bit reamer. RIH, slip 15 ft drilling line at shoe. Break circulation at shoe and RIH. Ream 30 ft rat hole and tag bottom. Drill 7-5/8" hole from 5058 ft to 5088 ft. Circulate bottoms up, pump pill and drop survey. POH. Rig up and run electric logs with Gearhart.

20/1/86

22/1/86

23/1/86

5088

5088

Run logs with Gearhart, pick up and make up Howco test tools, and run DST No. 4 over interval 5028.6 ft to 5088 ft in Pl-350 sand. Tool opened with immediate very weak blow. No gas to surface. Tool closed in after 20 minutes, re-opened after 40 minutes. No gas or oil to surface in final flow of 90 minutes. Final shut in for 220 mins. Field chart readings:

IHP IFP ISIP FFP FSIP FHP BHT 2606.4 55.2 165.6 58.4 185.1 2606.4 105°F

Drop bar and reverse circulate. Recovered 7.8 bbls of oil cut rat hole mud POH, make-up bit and bit sub, RIH.

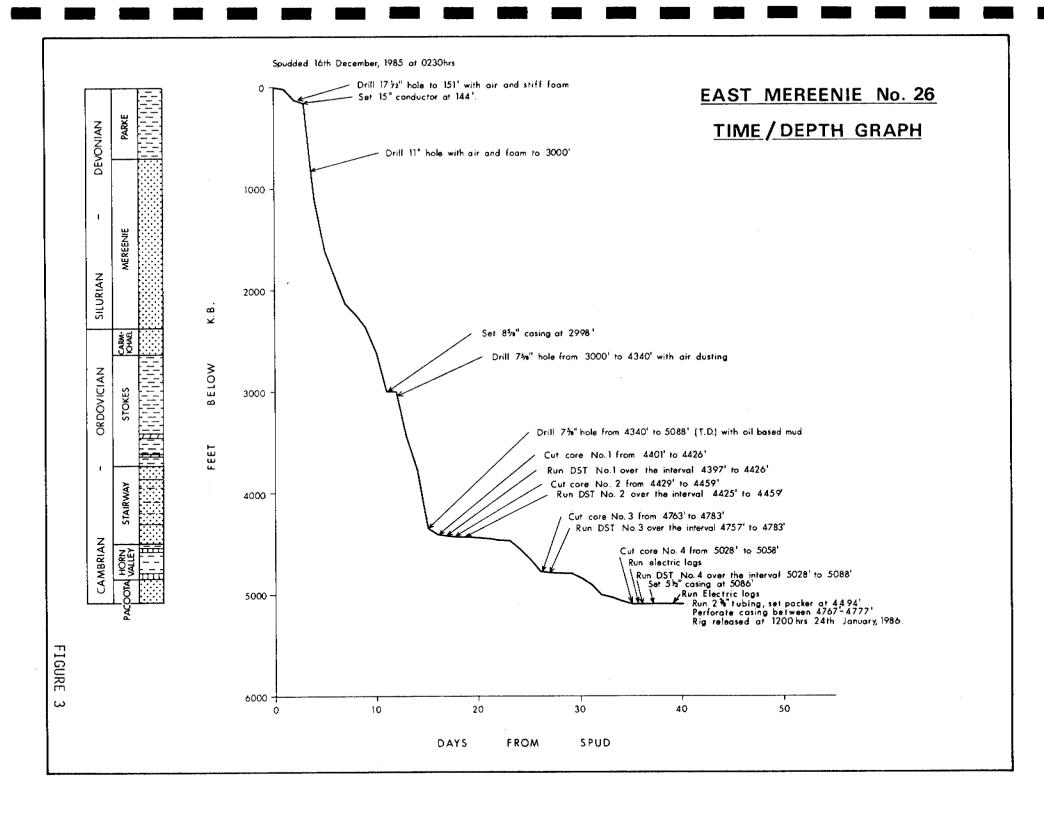
21/1/86 5088 RIH, circ and condition hole, pump pill, POH. Run 5-1/2" casing to 5085 ft and cement with 230 sacks of Class G cement with 0.75% CFR-2 plus 0.5% HALLAD 22A.

Cement 5-1/2" casing with float collar at 5046 ft, nipple down BOPs, energise tubing head seals to 2,000 psi and pressure test tubing head. RIH with 4-1/2" bit, and casing scraper, picking up 2-3/8" tubing. Tag plug at 5017 ft, POH, lay out BHA & bit.

Run CBL log, RIH with perforating gun and Guiberson packer assembly, on 2-3/8" tubing. Run correlation log (CCL/GR). Set packer, land do-nut with 18,000 lbs tension, pressure test annulus to 500 psi, nipple up Xmas tree, pressure test same to 1500 psi, drop detonation bar and perforate 4767 to 4777 ft. Wait on well to flow. Rig up Gearhart and swab from 300 ft

24/1/86 5088

Swab well, rig down Gearhart, flow well to clean for 1 hour 20 minutes. Flow well to test for 1 hour. Oil flow rate at 672 BOPD. Gas flow rate at 427 MCFD, GOR 635 cu ft/bbl, through a 1/2" choke. Rig released at 1200 hours.



2.3 Hole Sizes and Depths:

17-1/2" to 151 ft

11" to 3000 ft

7-5/8" to 5088 ft

2.4 Casing and Cementing Record:

15" conductor:

Weight:

1/4" Wall ERW

Grade/

Connections:

1/4" Wall ERW/welded

Shoe Depth:

144 ft

Cement Used:

46 sacks Class A

Additives:

Nil

Slurry Weight:

15.6 ppg

8-5/8" casing:

Weight:

1. 32 1b/ft

2. 36 lb/ft

Grade/

Connections:

1. J55/N80

2. K55/8 RND

No. of Joints:

80

Total Length:

2998.6 ft

Shoe Depth:

2998 ft

Cement Used:

161 sacks Class A

Additives:

0.2% HR4

Slurry Weight:

15.5 ppg

5-1/2" casing:

Weight:

14 1b/ft

Grade/

Connections:

J55/8 rnd

Total Length:

5088 ft

No. of Joints:

130

Shoe Depth:

5085 ft

Cement Used:

230 sacks Class G

Additives:

0.75% CFR-2 + 0.5% HALLAD

22A

Slurry Weight: 15.5 ppg

2.5 Drilling Fluids:

A summary of the daily drilling fluid properties is listed below in Table 1.

32 142 1659 1787	DAYS FROM SPUD	AIR AIR AIR AIR AIR	FOAM FOAM PAOLITIVE	1NJECTION RATE (BBLS/HR)	MUD WEIGHT (PPG)	FUNNEL VISCOSITY (SEC/QRT)	PLASTIC VISCOSITY (CP)	YIELD POINT (LBS/100FT2)	CAKE THICKNESS (32nd of in)	NIW CEL STRENGTH	WATER LOSS	OIL/WATER RATIO	SOLIOS CONTENT %	SAND CONTENT %	H C.	SALINITY x 1000 PPM	ELECT. STABILITY (VOLTS)	+ FLUID LOSS (+) or GAIN (+) to FORMATION + (b)s - hr)	PARKE SILTSTONE PARKE SILTSTONE PARKE SILTSTONE PARKE ST/MEREENIE SS MEREENIE SANDSTONE MEREENIE SANDSTONE MEREENIE SS	
12	78 90 11 12 14 15 166 178 120 122 223 24 256 27 28 29 33 13 33 35 6 3	AIR AIR AIR AIR AIR AIR AIR AIR OMUD OMUD OMUD OMUD OMUD OMUD OMUD OMUD	FOAM FOAM FOAM FOAM FOAM FOAM	10 8 8 8 8	10.1 10.1 10.1 10.1 10.1 10.2 10.2 10.3 10.3 10.3 9.3 9.3 9.5	4045565364333575857857 56666555555555544444	23 25 27 28 24 26 26 27 30 29 35 21 21 21 26	30 36 38 38 32 32 32 33 32 33 30 23 22 22 22	1 1 1 2 1 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1	5/12 8/15 10/15 10/15 12/17 10/15 10/14 8/12 10/12 10/12 10/11 10/11 10/11 10/11 5/7 5/7 5/6 5/6 5/7		70/30 70/30 71-29 73-17 73-17 75-25 77-21 80-20 79-21 79-21 79-21 79-21 79-21 79-21 79-21 79-21 79-21 79-21 79-21 79-21 79-21	1434555566666656455354 1155566666656455354	.25 .25 .25 .25 TR TR TR TR TR TR TR TR TR TR TR TR TR			580 520 610 710 780 900 930 930 980 990 940 900 910 920		MEREENIE QUARTZITE MEREENIE QUARTZITE L.MEREENIE/CARMICHAEL CARMICHAEL/U.STOKES UPPER STOKES UPPER STOKES UPL STOKES/U.STWY U-L STAIRWAY LOWER STAIRWAY HORN VALLEY PACOOTA P1	TABLE 1

EAST MEREENIE NO. 26 - DRILLING FLUID SUMMARY

2.6 Bit Record:

A summary of the drilling bits used is listed below in Table ?

HES)			32.13	; 4	•		82	00TAGE		1334	iours	7 FBS		EVIATION ()	URE	FLUID	SP	*	H	DO DAT		811	r con	HÖLTIG	
512E (INCH	HAKE	TYPE	1	2	_	SERIAL NO	DEPTH 00.T (FT)	סאורדנס על	HOURS	AVERAGE FE PER HOUR	ACCUMULATED DRITLING HOURS	₩08 x 1000	RPII	VERTICAL DEVI	PUNP PRESSURE (PSI)	DRILLING F TYPE	PUNSP NO. 1	PHIMP NO. 2	MUD WEIGHT (LBS/GAL)	V1SC0S1TY (SEC)	WATER LOSS (CC)	TEETH	BEARINGS	(SKI)	FORMATION
7.625 7.625 7.625 7.625 7.625 7.625 7.625 7.625 7.625	VAREL SMITH SMITH DB SMITH DB SMITH SMITH SMITH	Y537 Y537 Y537 Y537 Y537 F4 CB403 F5 F3 CB403 F4 CB403	14 14	18		174211 20768 15702 15363 15439 15701 16945 15701 16947 9509005 £19041 19509005 £19041 £19041 £19041 £19041 £19041 £19041 £19041 £19041 £19041 £19041 £19041	151 872 1854 2177 2379 2622 3000 3776 4301 4426 4459 4647 4783 4879 5028 5088	151 721 982 325 202 243 376 564 25 3 30 188 116 20 96 149 30 30	25.0 23.5 41.5 20.5 20.5 20.5 20.5 20.6 35.0 45.5 31.5 35.0 35.0 35.0 35.0 36.0 36.0 36.0 36.0 36.0 36.0 36.0 36	6.04 30.7 23.7 10.8 9.9 11.5 27.5 27.6 3.0 66.37 5.95 0.74 4.62	25.0 48.5 120.0 120.5 140.5 162.5 214.5 2234.5 2234.5 2290.5 3371.0 3390.5 420.5 450.5 512.1 518.5	10 22 23 18 12 21 22 23 23 23 23 23 23 23 23 23 23 23 23	900 355 935 3108 575 600 600 555 900 600 555 955	0.0 0.75 1.0 1.25 1.75 2.13 4.5 4.5 5.25 5.25 6.0 6.5 7.25 7.25 7.25	470 500 500 500 100 1000 1000 1000 1000 1	AIR	100 100 120 110 123 120 124 77 100 80	50 50 50 50				3 2 6 6 6 5 2 5 6 5 2 5 6 5 2 5 6 5 2 5 7 3 5 8 5 8	3 × 3 × 3 × 3 × 3 × 3 × 3 × 3 × 3 × 3 ×	IM IM 0.25 0.5 0.5 0.13 IM 0.06 0.06 0.06 VEAR IM VEAR IN 0.06 VEAR IN 0.19 VEAR	PARKE SILTSTONE PARKE/MERENIE SS PARKE/MERENIE SS MEREWIE SANDSTONE MEREWIE SANDSTONE MEREWIE OMATZITE MERECHIE OUATZITE MERECHIE OTZ.CARMICHAEL CARMICHAEL. U. STOKES UPP LOW STOKES, U. STWAY UPP/MID/LOW STAIRWAY LOWER STAIRWAY LOW

EAST MEREENIE NO. 26 BIT RECORD

DAYS FROM SPUD

BIT NO.

RR1 NB2 NB3 NB4 NB5 NB6 NB6 NB9 CB1 RR10 NB11 CB1 CB1 RB12 RB13

DEPTH IN KB (FT)

7 Deviation Record:

A list of deviation surveys and relevant computations is listed below in Table 3.

TABLE 3

DEPTH KB FT.	URVEY NO.	DEV. ANGLE	DEPTH INERVAL	MEAN DEV.	DEPTH CORRECTION	CUM. CORRECTION	TVD FT.	LATERAL DRIFT FT.	CUM. LATERAL	DIRECTION (EXAMPLE) W320.96N
210 459 709 964 1246 1497 1535 1823 2058 2141 22593 2962 3086 33495 3683 3872 4050 4410 4535 4753 4847 5025 5068	1 23 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 22 22 27	0.0 0.755 0.755 0.755 1.0 0.755 1.0 1.335 1.755 2.5 2.5 3.0 4.25 4.5 5.0 6.0 7.25 7.75 8.0	210 249 255 282 2582 2582 2588 2835 2002 3694 218 1889 1899 160 1889 160 1889 160 1889 1783	0.0 0.375 0.75 0.75 0.875 0.875 0.875 1.17 1.29 1.75 2.125 2.75 3.0 3.5 4.1375 4.875 5.625 6.5 7.875 7.875	0.0 0.005 0.021 0.022 0.033 0.029 0.004 0.034 0.049 0.021 0.068 0.118 0.254 0.143 0.254 0.143 0.299 0.262 0.351 0.490 0.582 0.579 0.582 0.579 0.582 0.579 0.582 0.726 1.523 0.4055	0.0 0.005 0.026 0.048 0.081 0.110 0.114 0.197 0.218 0.287 0.405 0.659 0.802 1.101 1.363 1.714 2.204 2.755 3.337 3.916 4.508 4.995 8.499	210 459 709 964 1246 1497 1535 2058 2141 2393 2961 3085 33494 3681 3870 4058 4510 4747 4840 4510 4747 5059	0.0 1.63 3.27 3.34 4.31 3.83 0.63 4.40 4.80 1.87 5.70 13.68 5.95 11.48 13.602 14.83 13.60 12.06 85.57 11.66 23.23 5.892	0.0 1.63 4.90 8.24 12.558 17.41 26.21 28.08 331.02 54.70 60.66 93.94 107.96 136.39 150.39 150.39 150.39 150.39 150.39 150.40 136.53 17.64 198.30 198.	

EAST MEREENIE NO. 26

DEVIATION RECORD

2.8 Formation Testing:

Four drill stem tests were run during the drilling of the well. A summary of results is presented below with full details included as Appendix 4.

Drill Stem Test No. 1

Interval:

4397.6 to 4426.3 ft (28.7 ft)

Date:

3rd January, 1986

Tester:

Halliburton

Formation:

Lower Stairway LS -160 sand

Test Type:

Open hole conventional

Water cushion:

Nil.

Times:

First flow:	40	mins
First shut-in:	80	mins
Second flow:	90	mins
Second shut-in:	269	mins

Bottom Bourdon Recorder Pressures (Field Results)

2339 PSIG Initial hydrostatic: PSIG 45.5 First flow: 68.2 PSIG Initial shut-in: 55.2 PSIG Second flow 81.2 PSIG Second shut-in: 2336 PSIG Final hydrostatic:

Results:

Immediate very weak blow remaining constant, initial flow 40 minutes due to drill pipe slips failure. Final flow had very weak blow decreasing intermittently to nil after 85 minutes of total flow. No fluids to surface. Gas cut mud from rat hole during reverse circulation.

Conclusions:

Valid test with the LS -160 sand having very poor permeability.

Drill Stem Test No. 2

4425.6 to 4459.3 ft (33.7 ft) Interval:

Date: 7th January, 1986

Tester: Halliburton

Formation: Lower Stairway LS -160 sand

Test Type: Open hole conventional

Water cushion: Nil.

Times: First flow: 20 mins First shut-in: 40 mins 90 Second flow: mins Second shut-in: 220 mins

> Bourdon Recorder Pressures (Field Bottom

Results)

Initial hydrostatic: 2447.5 PSIG First flow: 35.7 PSIG Initial shut-in: PSIG 55.2 Second flow PSIG 45.2 Second shut-in: PSIG 77.9 Final hydrostatic: 2431.5

Results: Immediate very weak blow remaining constant initial flow. Final flow died through

completely after a few bubbles with the manifold closed. No fluids to surface.

recovery on reverse circulation.

Valid Test. The LS -160 sand has very poor Conclusions:

permeability.

Drill Stem Test No. 3

Interval: 4757.6 to 4783 ft (25.4)

Date: 12th January, 1986

Tester: Halliburton

Formation: Pacoota P1-80 sand

Test Type: Open hole conventional

Water cushion: Nil.

Times: First flow: 20 mins First shut-in: 40 mins Second flow: 120 mins Second shut-in: 280 mins

Bottom Bourdon Recorder Pressures (Field Results)

2631.7 PSIG Initial hydrostatic: PSIG 649.7 First flow: PSIG 1805.4 Initial shut-in: PSIG 872.6 Second flow PSIG 1821.2 Second shut-in: PSIG 2590.5 Final hydrostatic:

Immediate strong blow, open manifold to flowline, gas to surface in 15 minutes with a maximum wellhead pressure of 120 psi. Final flow, oil to surface in 28 minutes of total flow time, maximum wellhead pressure 237 psi. Oil flowed at 694 BOPD, gas at 440 MCFD with a GOR of 635 cu ft/bbl, through a

0.5" choke.

Valid test with the P1-80 sand having good

permeability.

Results:

Conclusions:

Drill Stem Test No. 4

Interval: 5028.6 to 5088 ft (59.4 ft)

Date: 20th January, 1986

Tester: Halliburton

Pacoota P1-350 sand Formation:

Test Type: Open hole conventional

Water cushion: Nil.

Times: First flow: 20 mins First shut-in: 40 mins Second flow: 90 mins Second shut-in: 220 mins

> Bottom Bourdon Recorder Pressures (Field

Results)

Initial hydrostatic: 2606.4 PSIG First flow: 55.2 PSIG Initial shut-in: 165.6 PSIG Second flow 58.4 PSIG Second shut-in: 185.1 PSIG Final hydrostatic: 2606.4 PSIG

Results:

Immediate very weak blow remaining constant through initial flow. Instant very weak blow during final flow decreasing gradually and dead after 75 minutes of final flow No fluid to surface, recovery of period. 7.8 bbls oil cut rat hole mud on reverse

circulation.

Conclusions:

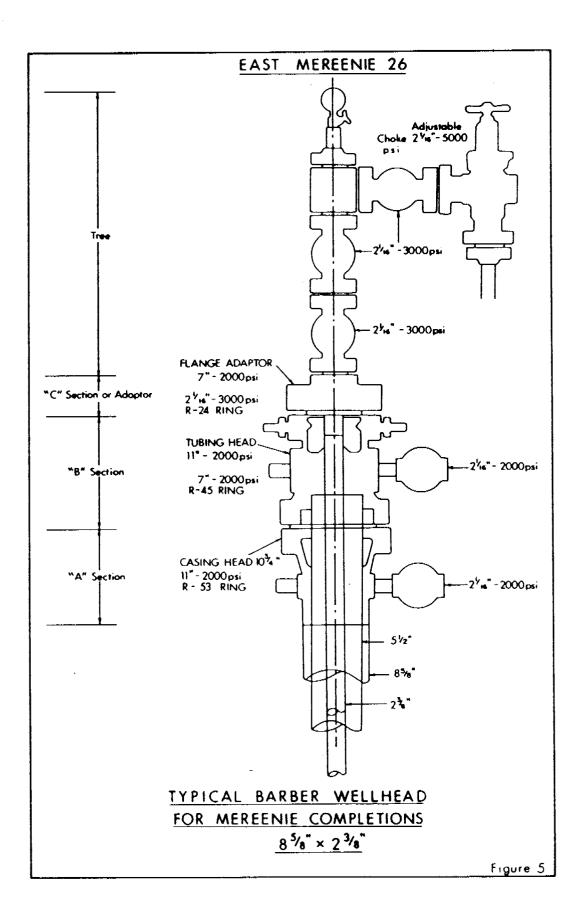
Valid test and the P1-350 sand has very poor permeability.

2.9 Completion Data:

East Mereenie No. 26 was completed as an oil producing well over the P1-80 sand horizon. 5-1/2" casing was perforated over the interval 4767 to 4777 ft using a Gearhart tubing conveyed perforating gun. The 5-1/2" casing shoe was set at 5086 ft and plugged back to approximately 5017 ft. 2-3/8" tubing was run to 4777 ft with the packer being set at 4494 ft. The rig was released at 1200 hrs on the 24th January 1986.

MOONIE OIL N.L. WELL COMPLETION SUMMARY

		WE	LL F	RC	FILE	:	_					DATE:	DAY MONTH YEAR	
-	- -	-	4											
15"						-			WELL NAME EAST MEREENI					
									WELL LOCATION LAT 24° 03'					
144	<u>- -</u>	+	+	1:					K.B. ELEVATION					•
							: :	;	size (0.0.) Weight CASING 15" 52LB/	ĖT	14	4	INTERVAL DEPTH	
		1	1				1 1		casing 8-5/8" 32/36			8,56		
					-	\Box			-PERFS: 5-1/2" 14.0L					
	-	1		:	1	•			DIAMETER OPEN HOLE					
					-				TUBING: SIZE 2.375" O.D.					
		1	-	-	-				TYPE/CLASS E.U.E.					
		1	-	1:	-				No. OF JOINTS ON LOCATION					
8-8	5	1		1:					PERMANENTLY IN WELL					
		1	-	1.	-			- · · · · ·	FINAL TUBING S	TRING FF	_		VARD	
 - 	.	-	_ -		- -			· · ·	DESCRIPTION	ft		SET AT TOP	REMARKS	
	_ -	_	- -	Ŀ	_		:: 		GEARHART 3.5" GUNS	10	00			
		1			- -				GEARHART FIRING HEAD	2	46			
		1.		1:					GEARHART NO-GO		67	_		
		_		<u> </u>					1 JT TUBING	31	58	<u> </u>		
		1			- :				GEARHART SHATTER DISC		84			
		- -	_ -						GEARHART SAFETY SUB		84			
2998	2	1	- -	-	-		· .		1 JT TUBING	31		·		
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		-	- :	1:					1 x 2-3/8" SLIDING SLEEVE		87	<u>T</u>	YPE - OTIS	
		4	4	1.		,			1 JT TUBING	31				
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			- -	-					146 JTS TUBING	4567		-		
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	51/2					· ·· ·			1 PUP JOINT	1	23			
		-	- .						1 JT TUBING	31	[
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44	94	1	\geq	\leq	<u> </u>	(PA	CK	R	SETTING DEPTH K.B.	4777.		TIME ON BOTTO! CASING INTERNA	NL 5017 FT	
			- -	ŀ					WEGGLE			DEPTH BY TUBIN		
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			- -	1:			 		MASTER VALVE TYPE FLANGED M				2" - 3,000 P\$I	
PERFOI	RATIN		۲.	ጘ	10	RFO	471 RA-1		CASING VALVES. TYPE FLANGED M		BAR	TON SIZE	2" - 3,000 PSI	
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		1	<u></u>		+		475	¥ '₹'	REMARKS (Note Additional Equipment)					
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3. GEOLOGICAL DATA

3. GEOLOGICAL DATA:

3.1 Stratigraphy:

See Stratigraphic Table (Table 4).

3.2 Formation Sampling:

(1) Ditch Cuttings:

Samples were taken at 30 ft intervals from 220 to 4660 ft with closer spaced sampling undertaken adjacent to predicted formation tops. From 4660 to 5088 ft (TD) samples were taken at 10 ft intervals.

Throughout the drilling operation two unwashed bagged samples were obtained for each sample interval. For each interval a washed and dried portion was produced from which a three-way sample split was made.

The samples were distributed as follows:

Moonie: 1 set washed & dried; 1 set unwashed

Magellan: 1 set washed & dried

NT Dept of Mines: 1 set washed & dried; 1 set unwashed

Sample descriptions are presented in Appendix 1.

(2) Coring:

A total of 105 ft of core was cut over four coring runs with 99.5% recovery.

The depths of all cores have been corrected to correlatable electric log depths. Descriptions are given in Appendix 2.

CORE NO.	INTERVAL DRILLER FT	INTERVAL CORRECTED FT	CUT FT	REC FT	REC %	BIT TYPE (7-5/8%)
1	4401-4426.3	4403-4428.3	25.3	25.3	100	DB CB403
2	4429-4459.3	NO CORRECTION	30.3	30.3	100	DB CB403
3	4763-4783	4762-4782	20	19.7	98	DB CB403
4	5028-5058	NO CORRECTION	30	29.8	99	DB CB403
TOTAL	, , , , , , , , , , , , , , , , , , ,		105.6	105.1	99.5	

TABLE 4 EAST MEREENIE NO. 26 STRATIGRAPHIC TABLE

SYSTEM & SERIES	FORMATION	SUB UNIT		DEPTH (FT	')	TRUE	AVERAGE	AVERAGE WELL DEVIATION
			KB.	TVD	MSL	THICKNESS	FORMATION DIP	
MIDDLE TO LATE DEVONIAN	PARKE SILTSTONE		13	13	+2293	693+	8	0
MIDDLE DEVONIAN TO LATE SILURIAN	MEREENIE SANDSTONE		706	706	+1600	1667	8	0.8
LATE ORDOVICIAN	CARMICHAEL SANDSTONE		2373	2373	-67	241	8	1.8
MIDDLE ORDOVICIAN	STOKES SILTSTONE	UPPER	2614	2614	-308	819	8	1.8
		LOWER	3434	3433	-1127	257	8	3.0
	STAIRWAY SANDSTONE	UPPER	3692	3690	-1384	139	8	4.0
		MIDDLE	3831	3829	-1523	421	8	4.1
		LOWER	4253	4250	-1944	208	-	4.5
EARLY ORDOVICIAN	HORN VALLEY SILTSTONE		4462	4458	-2152	227	9	5.5
		P1	4690	4685	-2379	349	9	6.5
EARLY ORDOVICIAN TO LATE CAMBRIAN	PACOOTA SANDSTONE	P2	5042	5034	-2728	45+	9	8.0
		Р3	_	-	_	_	-	-
		P4	_	_	_	_	-	-
LATE CAMBRIAN	GOYDER FORMATION		_	_	_	-	-	-
	TOTAL DEPTH		5088	5079	-2773	-	-	-

(3) Sidewall Coring:

No sidewall cores were taken.

3.3 Core Analysis:

The core analysis programme for East Mereenie No. 26 was designed to provide data on three intervals, the Lower Stairway LS-160 sand, and the Pacoota PI-80 and P1-350 sands.

Conventional core analysis was carried out on 21 samples within the Lower Stairway Sandstone and on 14 samples in the Pacoota Pl Sandstone.

Two cores were cut in the Lower Stairway LS-160 sand interval and samples sent for analysis showed average porosities of 3%, with a maximum porosity of 6%. Permeabilities averaged 0.5 md. An improvement of porosity and permeability was noted in the top seven foot of the LS-160 sand interval (4404 ft to 4411 ft KB). This 7 ft exhibits porosity in the range of 3 to 6% and permeabilities in the range of 1 to 2.3 md. The LS-160 sand below this has porosities of less than 3% and permeabilities of less than 1 md. Evidence of considerable vuggy porosity was seen throughout the core of the LS-160 sand predominantly between 4404 ft and 4427 ft.

One core (Core No. 3) sampled the P1-80 sand. The sand interval showed an average porosity of 13% and average permeability of 40 md.

Core No. 4 from 5028 ft to 5058 ft sampled the P1-350 sand. Core porosities averaged 5% and permeabilities 0.3 md. As this core was cut below the estimated oil/water contact at -2450 ft MSL the average oil saturation of 11% measured by fluid summation techniques is considered significant. Although the well was drilled at this point with an oil based mud that level of oil saturation would appear consistent with other reservoir horizons of similar porosity and permeability within the oil column. The results of Drill Stem Test No. 4 indicate that the P1-350 sand contains in-place hydrocarbons.

The following table summerizes the core analysis results for the 3 sands cored in this well.

SAND INTERVAL	AV HOR KA-MD	MAX HOR KA MD	AV HE INJ Ø%	MAX HE INJ ØZ	<u>AV SO</u> %	AV STW
LS -160	0.5	15	3	6	15	20
P1-80	40	87	13	15	45	28
P1-350	0.3	3.1	5	9.5	11	3 5

3.4 Logging and Surveys:

1. Electric Logging:

The following logs were run using a Gearhart DDL logging unit.

LOG	RUN	INTERVAL	DATE
GR	1	16-5087	19/1/86
CDL	1	3592-5087	19/1/86
CNS	1	3554-5087	19/1/86
CAL	1	2990-5087	19/1/86
DIL	1	3599-5081	20/1/86
WEL LOG	1	4200-5080	20/1/86
CBL/VDL/GR/CCL	1	3393-4682	23/1/86
CCL/GR	1	4445-4682	23/1/86

Prints of all wireline logs are included as Enclosure 4.

2. Velocity Survey:

No velocity survey was run.

3. Penetration Rate and Gas Logs:

The penetration rate was recorded continuously from spud to total depth. Gas was monitored continuously by a conventional hotwire detector during the air dusting and mud drilling phase.

A mud log showing penetration rate, gas, lithological and other pertinent data was prepared at the well site on a daily basis and is included as Enclosure 3.

A composite log is included as Enclosure 2.

4. Deviation Survey:

Deviation surveys were taken at regular intervals during the drilling of the well. The drift and true vertical depth corrections are shown in Table 3.

5. Temperature Surveys:

Temperature surveys were not carried out, however the following temperatures were recorded:

141° F at 4783 ft; Halliburton

139° F at 5088 ft; Gearhart

3.5 Formation Dips:

A structural dip of approximately 8 degrees east northeast was prognosed for this well.

Based on formation tops as compared with surrounding wells, the figure of 8 degrees appears to be the true formation dip.

3.6 Formation Evaluation:

See Stairway and Pacoota Sandstone Sand Data Sheets. (Tables 5 and 6).

Two cores were cut in Lower Stairway Sandstone interval in the LS-160 sand. Core analysis showed average porosities of 3% and a maximum porosity of 6% in the cored interval. Permeabilities averaged 0.5 md. The porosity data from the cores correlates well with that shown on the density log. The data shows that the top 7 ft of the LS-160 sand from 4404 ft to 4411 ft shows the best reservoir potential in this well. Core analysis shows porosities ranging from 3 to 6% and permeabilities from 1 to 2.3 md in this interval. Below porosities are generally less than 3% and permeabilities less than 1 md.

From the core descriptions it would appear that at least some of the porosity present in the cored interval is vuggy porosity. This is distributed irregularly throughout the core, being more concentrated in the sandy sections. Some of the vugs evident on the surface of the core may be due to more friable sections of the lithology being washed out during the drilling process. The poor drill stem test results combined with what would appear to be reasonable porosity from the logs would support the presence of vuggy porosity with very little interconnection between the pores.

Minor fracturing is evident throughout the core, however no large or open fractures are evident. Drill stem test results show that effective fracture permeability is not present in this well in the LS-160 sand interval.

Evidence of hydrocarbons occurs throughout the cores in the LS-160 sand, ranging from gas bubbling to good fluorescence and oily sweats. Noticeably most evidence of hydrocarbons occur within the zones showing vuggy porosity and/or fractures.

The P1-80 net sand interval exhibited good porosity (average 13%) and good permeability (average 40 md) from core analysis. This was reflected in the visible examination of the core chips and the presence of oil sweat in Core No. 3. Drill Stem Test No. 3 confirmed the good permeability of this interval and flowed 694 BOPD through a 0.5" choke.

STRATIGRAPHIC GROSS SAI CORRELATION GR < 80						NET SAND & CDL ≥ 6%					
SAND NAME	INTERVAL KB - FT	INTERVAL KB - FT	t FT	INTERVAL KB - FT	t FT	A V ø	MAX ø	INTERVAL KB - FT	t FT	A V	MAX O
U. STAIR US-10 US-10 MISC US-40 US-80 US-100 US-100 US-100 US-100 US-100	3692-3720 3692-3720 3720-3723 3728-3735 3740-3768 3774-3831 3774-3831 3774-3831 3774-3831	3701-3707 3710-3719 3730-3734 3774-3788 3794-3806 3808-3822 3826-3832	6 9 4 14 12 14 6	3720-3723 3728-3730 3786-3790 3797-3803 3808-3811 3814-3816 3817-3826	3 2 4 6 3 2 9	4.5 4.5 4 5 5 7.5	5 5 7 6 6 12.5	3799-3802 3818-3826	3 8	6.5	7
		:	65		29				11		
M. STAIR MISC MISC MISC MISC MISC	3831-3835 3836-3844 3856-3862 4238-4244	3856-3858 4242-4243	2	3831-3835 3836-3844 3856-3862 4240-4242	4 8 10 2	6.5 5 5.5 4.5	9 7 8.5 5.5	3831-3834 3837-3839 3857-3862	3 2 5	7.5 6.5 7	9 7 8.5
			3		24				10		
L. STAIR LS-10 MISC LS-50 LS-50 LS-50 MISC LS-80 LS-150 MISC LS-160 LS-160 LS-160	4262-4270 4280-4282 4290-4322 4290-4322 4290-4322 4326-4330 4333-4347 4388-4396 4400-4462 4404-4462 4404-4462	4262-4264 4291-4301 4311-4314 4315-4322 4388-4393 4404-4438 4440-4457 4460-4462	2 10 3 7 5 34 17 2	4280-4282 4290-4300 4302-4305 4318-4320 4325-4330 4334-4337 4400-4402 4405-4407	2 10 3 2 5 3 2 2 2	5 6.5 4.5 4.5 4.5	6 12 6 4.5 8.5 5.5 6.5	4291-4297 4326-4330 4401-4402	6 4	8.5 6.5	8.5 6.5
			80		29				11		
STAI	STAIRWAY SANDSTONE TOTAL		148		82		L	<u> </u>	32		

STRATIGRAPHIC GROSS SA CORRELATION GR < 80		ND NET SAND Ø CDL > 4% API			L <u>></u> 4%	NET SAND & CDL			<u>></u> 6%	·	
SAND NAME	INTERVAL KB - FT	INTERVAL KB - FT	t FT	INTERVAL KB - FT	t FT	% AV Ø	% MAX Ø	INTERVAL KB - FT	t FT	% AV O	MAX O
P1 MISC P1-40 P1-80 P1-110 P1-120 P1-140 MISC P1-190 P1-210 P1-240 MISC MISC P1-280 P1-130 P1-350 P1-350	4728-4732 4734-4749 4734-4749 4768-4779 4766-4804 4811-4817 4836-4840 4847-4849 4879-4887 4901-4910 4921-4939 4944-4946 4949-4952 4975-4979 4992-5021 5030-5042	4768-4774 4786-4804 4879-4884 4922-4939 4950-4952 4976-4978 4993-5020 5030-5037	6 18 5 17 2 27 7	4728-4732 4734-4742 4746-4749 4768-4775 4793-4800 4847-4849 4881-4887 4903-4910 4944-4946 4950-4952 5004-5010 5030-5044	4 8 3 7 7 2 6 7 2 2 14	4.5 4.8 4.5 5.5 4.5 4.4 4.4 4.5	- 6.5 7.5 15 7 56 4 4.5 5.5	4728-4730 4746-4748 4770-4774 4793-4795 5035-5039 5040-5042	2 2 4 2	6 6.5 10.5 6.5	6.5 7.5 15 7
P2 MISC MISC	5046-5051 5068-5072		84	5047-5052 5068-5072	68 5 4	5 5	7.5 7	5048-5050 5069-5071	2 2 4	7 6.5	7.5 7
PACOOTA SANDSTONE TOTAL		84		77		***************************************		20		1	

The P1-350 sand was cored and tested as well as logged. These data show that although porosities of up to 7% are present, permeabilities are poor throughout ranging from 0.06 to a maximum of 3.1 md. The low permeabilities were confirmed by Drill Stem Test No. 4.

It must be noted that the core cut in the P1-350 sand from 5028 ft to 5058 ft KB below the estimated oil/water contact at 4756 ft KB (-2450 ft MSL), exhibited oil fluorescence and cut, together with minor sections of visible oil sweat. Core analyses from this zone show water saturations in the range of 39% above 5054 ft and from 54 to 72% in the interval 5054 ft to 5058 ft. Further examination of the core analysis results show that permeabilities in the lower interval are very low in the range of .04 to .06 md. Thus the higher water saturations are a result of overall lower permeabilities rather than an oil/water transition zone occurring at this level.

The P1-350 sand in East Mereenie No. 26 contains hydrocarbons some 284 ft below the estimated oil/water contact at -2450 ft MSL.

3.7 Relevance to Appraisal Programme:

A comprehensive evaluation of the LS-160 sand in this well showed that although porosity was present some at least was vuggy porosity and permeabilities were low throughout the sand despite the presence of minor fractures. This well is some 930 meters from East Mereenie No. 8 which produced 7.29 MMCFD from the LS-160 Sandstone.

Obviously the permeabilities in the LS-160 Sandstone in this area of the field are extremely variable over relatively short distances and the high flow rates from the sand interval in East Mereenie No. 8 are most likely due to fracture permeability.

The productive capacity of the Pacoota P1-80 Sand has been confirmed in this well with a flow of 694 BOPD.

The Pacoota P1-350 sand was extensively evaluated and showed that oil, and possibly moveable oil, exists at a considerable depth below previously anticipated oil/water contact at -2450 ft.

Formation dips were as prognosed, being approximately 8 degrees in a east northeast direction.