

Burdo 1 Interpretive Summary Kyalla Interval

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McArthur Basin Integrated Petroleum Geochemistry, 2016

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PETROLEUM GEOCHEMISTRY

INTRODUCTORY NOTE

A geochemical investigation has been conducted to assess hydrocarbon prospectivity of the Kyalla, Formation in the Burdo 1 well located in the Beetaloo Sub-Basin, Northern Territories, Australia. Twenty-seven (27) core chip samples from this well were analyzed by a variety of geochemical techniques, including total organic carbon (TOC, LECO $^{\otimes}$), programmed pyrolysis (SRA) and organic petrology with measured maceral reflectance (R_{o}). In addition, client supplied published geochemical data for 38 samples were also incorporated into the interpretive evaluation. The complete results of these analyses are documented in this report along with an integrated geochemical interpretation that is summarized in the following table.

Well Name	Formation	Main Product	Thermal Maturity	Source Rock Richness	Organic Matter Type	Shale Oil Risk
Burdo 1	Kyalla	Estimated O	riginal —	Good (1.09% TOC)	Oil-prone Type II	High
Measured Curr	ently \longrightarrow	Oil	Peak Oil N	Fair (0.85% TOC)	√ Gas-prone Type III	

Current TOC averages represent all data available; Original TOC averages are only high graded samples that have PPy data

Table 1. Geochemical Summary

KYALLA

Twenty-seven (27) samples from the Kyalla Formation were analyzed for LECO TOC content and programmed pyrolysis, with the remaining data set (38 samples) composed of client supplied public data (Fig. 1). TOC contents ranged from 0.27 to 1.39 wt.% and averaged 0.85 wt.% (fair). Twenty-three (23) samples have TOC content above the minimum requirement of 1 wt.% for *effective* petroleum source rocks, none of these samples have TOC content above the minimum requirement of 2 wt.% for *economic* petroleum source rocks. Highest TOC content was found near the top of the designated Kyalla interval (801 m depth) (Fig. 1), although the basal portion of the Kyalla in this well has a much thicker zone of elevated TOC and reaches a secondary maximum at 1116 m depth (Fig. 1).

The S1 values of the Kyalla source rock samples average 0.25 mg HC/g rock (5 bbl oil/acre-ft) and the S2 values average 1.02 mg HC/g rock (22 bbl oil/acre-ft). The S1 and S2 values imply poor in-situ hydrocarbon saturation and poor remaining generative potential (Fig. 1). The normalized oil contents (NOC) in the Kyalla samples, (S1/TOC) x 100, average 29 (Fig. 1). NOC values of 20 to 50 are typical of low maturity source rocks, whereas values of 50 to 100 indicate possible oil staining or shows in thermally mature, tight petroleum source rocks. NOC > 100 are often associated with conventional oil reservoirs and indicate good prospectivity in unconventional shale oil plays. Jarvie (2012) has utilized a depth comparison of TOC versus programmed pyrolysis S1 yields as a potential indicator of producible hydrocarbon saturation in unconventional source rocks. When the S1 yields (reported as mg HC/g rock) exceed or "cross-over" the measured TOC content (reported as wt.%), this would be interpreted to represent zones with good potential for containing producible hydrocarbon saturation (or zones of possible contamination). In the present study, there is no S1 cross over TOC in any of the Kyalla samples analyzed (Fig. 1).



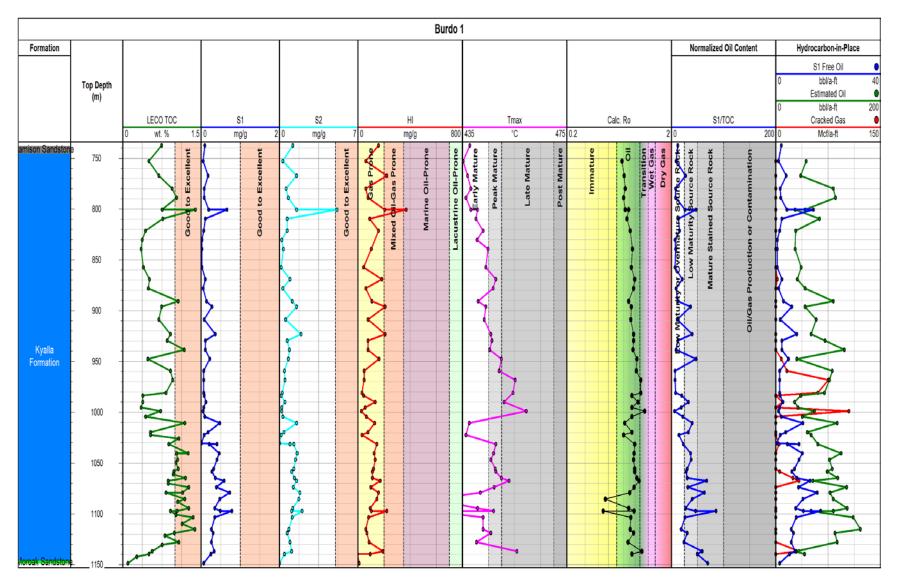


Figure 1. Geochemical depth plots for the Burdo 1 well.



The measured Hydrogen Index (HI) values in the Kyalla average 115 mg HC/g TOC, indicating gas-prone Type III kerogen quality in these source rocks at present day. Original HI $_{o}$ of these samples are estimated to average 450 mg HC/g rock, which indicate oil-prone Type II kerogen. Transformation Ratios (TR) based upon HI are average 82%, which suggest peak oil window thermal maturity. The T_{max} values in the Kyalla samples average is 444°C. T_{max} between 425 and 435°C typically indicate early oil window, while values between 435 and 445°C typically indicate peak oil window (Type II kerogen). On the basis of these guidelines, the average Kyalla T_{max} values in this well would be interpreted to be in the peak oil window. Using the formula published by Jarvie et al. (2007) for Type II kerogen (Calculated R $_{o}$ = (0.0180)(T_{max}) – 7.16), the measured T_{max} value of 444°C is equivalent to a Calc. %R $_{o}$ value of 0.84%. It is important to note that T_{max} is only a crude measure of thermal maturation (Peters, 1986) and it can be compromised by a variety of pyrolysis artifacts and caveats.

The Production Index (PI) values in the Kyalla samples average 0.19. These elevated PI values are consistent with source rocks in the peak oil window, which typically have PI values in the range of 0.15 to 0.25, while samples in the late oil to condensate window tend to have values in the range of 0.25 to 0.40.

Organic petrology was performed on one sample from the Kyalla interval (939 m). The results from this analysis show a distribution that consists of macerals identified as either fluorescing Alginite, low reflectance solid bitumen or high reflectance solid bitumens (Fig. 2). The fluorescing Alginite has a mean reflectance of 0.58% R_o. The low reflectance solid bitumen population has relatively higher reflectance values that average 1.03% R_o and are considered the most representative indigenous kerogen population for thermal maturity assessment. The high reflecting solid bitumen population has reflectance values that average 1.24% R_o. The solid bitumens are thought to possibly represent fine grained migrabitumen, although they could also represent preserved original cyanobacterial kerogen that has subsequently undergone thermal conversion to form a dispersed solid bitumen network within these Kyalla Formation source rocks. Published solid bitumen conversions were applied to these reflectance values. The conversion formula published by Landis and Castaño (1995) for bitumen in lenses/layers (Eq. R_o = (Bitumen R_o +0.41)/1.09) was applied to the low reflectance bitumen population and resulted in a 1.32% Eq. R_o. The conversion formula published by Jacob (1985) equation (Eq. R_o = (Bitumen R_o \times 0.618) + 0.4) for 'angular-like' pyrobitumen trapped in mineral pore spaces was applied to the high reflecting population and resulted in a 1.16% Eq. R_o. The Landis and Castaño (1995) conversion would suggest a maturity within the condensate/wet gas window and does not appear to be applicable for these solid bitumen reflectance readings. However, the Jacob (1985) conversion does appear to provide a possible correction back to a more suitable thermal maturity that is in general agreement with the average value from the population of low reflectance solid bitumens. Comparison with other samples examined in the current study suggest that the high reflectance solid bitumen reflectance readings can be corrected using the Jacob (1985) formula and often these "corrected" values compare favorably to "uncorrected" readings from the population of low reflectance solid bitumen within the same sample. Thus, the calculated 1.16% Eq.R_o value and the measured 1.03% R_o values would both suggest the Kyalla samples in this well are within the late oil window. This interpretation is also supported by an unpublished conversion for fluorescing Alginite (Knowles, pers. comm.) that gives a 1.14% Eq. R_o for the mean reflectance readings in this sample.

The thermal maturity of the Kyalla source was also evaluated by measured Kübler Index values from XRD, which are based upon illite crystallinity. These values can be used as maturity indicator when samples contain sufficient high quality clays (Abad, 2008). Five (5) samples from the Kyalla Formation (avg. 45% clays) have an average measured Kübler Index of 0.252, which is equivalent to a measured vitrinite reflectance of > 4% (late stage metagenesis). This interpretation is inconsistent with other geochemical maturity ratios evaluated in this study and suggests the Kübler Index should be used with caution to evaluate thermal maturity in Mesoproterozoic aged source rocks.



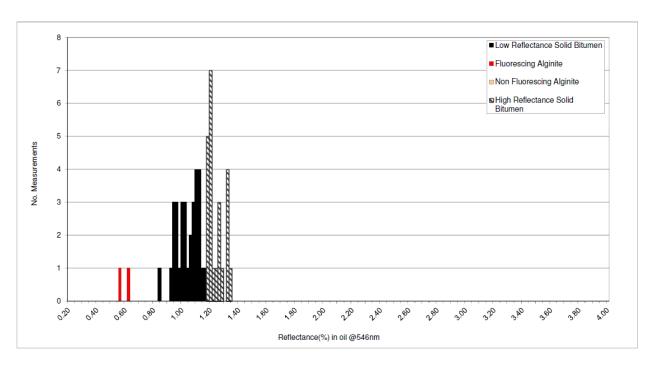


Figure 2. Organic petrology of the Kyalla (939 m) in the Burdo 1 well. Mean maceral reflectance of low reflecting solid bitumen is 1.03% R_o . The high reflecting solid bitumen has mean reflectance of 1.24% R_o , which equates to calculated Eq. R_o of 1.16% R_o using the conversion of Jacob (1985).

ORIGINAL GENERATIVE POTENTIAL AND HYDROCARBON YIELD CALCULATIONS

Petroleum generative capacity depends on the original quantity of organic matter (TOC_o) and the original type of organic matter (HI_o) (Peters et al., 2005, p. 97). The petroleum generation process has likely decreased the remaining generative potential as measured by TOC_{pd} and HI_{pd} in the Kyalla source rocks examined in this study. We can estimate the extent of the petroleum generation process, the volume of expelled oil and the expulsion efficiency by making some reasonable assumptions based on the core geochemical data and published regional information (Jarvie et al., 2007; Peters et al., 2005).

HI_o values can be computed from visual kerogen assessments and assigned kerogen-type HI_o average values using the following equation (Jarvie et al., 2007):

$$HI_{0} = \left(\frac{\% \text{ Type I}}{100} \times 750\right) + \left(\frac{\% \text{ Type II}}{100} \times 450\right) + \left(\frac{\% \text{ Type III}}{100} \times 125\right) + \left(\frac{\% \text{ Type IV}}{100} \times 50\right) \tag{1}$$

This equation requires the input of maceral percentages from visual kerogen assessment of a source rock. For the present study, only limited kerogen data were available. Where available, these kerogen data sets were used. In the absence of other measured kerogen data original kerogen type were interpreted in the context of measured present day TOC, HI and OI values to arrive at an appropriate kerogen mix for each sample examined in this investigation. All samples were modeled using appropriate kerogen mix to maintain an appropriate transformation ratio consistent with the interpreted thermal maturity. The average maceral percentage in the various formations evaluated in the current study are shown in Table 2, along with the resultant average original HI_o values calculated using equation (1) above. The kerogen estimations used in this study are generally in agreement with other published values that suggest Type II to a mixed Type I/II kerogen assemblage (Law et al., 2010; Crick et al., 1988; Taylor et al., 1994).



Formation	%Type I 750 HI。	%Type II 450 HI。	%Type III 125 HI。	%Type IV 50 HI。	НI _о
Kyalla	0	100	0	0	450

Table 2. Average Kerogen Estimations for Burdo 1 well.

The extent of the petroleum-generation process, or transformation ratio (TR) which is also called fractional conversion, is calculated as follows (Jarvie et al., 2007, p. 497):

$$TR_{HI} = 1 - \frac{HI_{pd}[1200 - HI_{o}(1 - PI_{o})]}{HI_{o}[1200 - HI_{pd}(1 - PI_{pd})]}$$
(2)

 HI_{pd} and PI_{pd} are the measured HI and PI values for the various source rock samples in this well. The average HI_{pd} and PI_{pd} for the formations evaluated in the current study are shown in Table 3. HI_o and PI_o are the original HI and PI values for immature organic matter in the rocks. For this calculation using the assumptions described previously results in an average HI_o values of 450 mg HC/g TOC (Table 2). We assume a PI_o of 0.02 (see Peters et al., 2005). Using these values in equation 2, the extent of fractional conversion of HI_o to petroleum is 0.82 (Table 3), i.e., on average an estimated 82% of the petroleum generation process has been completed.

The original TOC_o in the source rocks before burial and thermal maturation is constrained by mass balance considerations as follows (corrected from Jarvie et al., 2007):

$$TOC_{o} = \frac{HI_{pd}\left(\frac{TOC_{pd}}{1+k}\right)(83.33)}{\left[HI_{o}\left(1-TR_{HI}\right)\left(83.33-\left(\frac{TOC_{pd}}{1+k}\right)\right)\right] + \left[HI_{pd}\left(\frac{TOC_{pd}}{1+k}\right)\right]}$$
(3)

In this equation k is a correction factor based on residual organic carbon being enriched in carbon over original values at high maturity (Jarvie et al., 2007, p. 497). For Type II kerogen the increase in residual carbon C_R at high maturity is assigned a value of 15% (whereas for Type I, it is 50%, and for Type III, it is 0%) and the correction factor k is then $TR_{HI} \times C_R$. The kerogen mix for each individual sample was used in this calculation.

Using equation 3, the estimated original TOC_o for the Kyalla source rock samples in this well before petroleum generation average 1.09 wt.% (Table 3).

The original generation potential S2_o can be calculated using the following equation:

$$S2_{o} = \left(\frac{HI_{o} \times TOC_{o}}{100}\right) \tag{4}$$

For the Kyalla source rocks examined in the Burdo 1 well, the average S2_o values are 4.9 mg HC/g rock or approximately 108 bbl/acre-ft (multiply S2_o by 21.89 to calculate barrels/acre-ft, Jarvie and Tobey, 1999) (Table 3).

Knowing the measured remaining generation potential S2 from programmed pyrolysis and using the calculated original generation potential $S2_{\circ}$ enables a determination of the amounts of hydrocarbons generated. A VR_{\circ} algorithm can then be applied to estimate fractional oil cracking thereby converting yields to estimated oil and cracked gas (reported as Mcf/acre-ft or thousand cubic feet/acre-ft).



Original
$$(S2_0)$$
 – Remaining $(S2)$ = Generated HCs (5)

Using this methodology for the Kyalla samples analyzed in the current study, the estimated generated oil yields average 69 bbl/acre-ft (Table 3).

Formation	TOC _{pd}	HI _{pd}	S2 _{pd} bbl/a-ft	HI。	TR	тос。	S2。 bbl/a-ft	S1 Free Oil bbl/a-ft	Est. Oil bbl/a-ft	Cracked Gas Mcf/a-ft
Kyalla	0.85	115	22	450	0.82	1.09	108	5	84	8

Table 3. Hydrocarbon Yields average data for Burdo 1 well.

For shale oil systems, the amount of hydrocarbons (oil + gas) expelled from the rocks can be estimated as the difference between the amount of residual oil measured via programmed pyrolysis (S1) and the amount of estimated generated hydrocarbon yields determined above (equation 5). The expulsion efficiency (ExEf) can then be calculated as a direct proportion of the measured retained oil saturations and the average generated hydrocarbon yields. Thus, the resulting expulsion efficiency for the Kyalla interval is 94%, which is consistent with a source rock in the peak to late oil generation window.

The Kyalla source rock interval in the Burdo 1 well is interpreted to be in the peak oil window and hydrocarbon yield calculations suggest minor to moderate amounts of generation have occurred (predominantly oil with minor secondary cracked gas). From an exploration risk perspective, this is generally favorable. However, it is useful to relate these hydrocarbon yields to other productive unconventional US Shale plays (Table 5). In doing so, the potential critical value is not necessarily the generated oil and gas yields, but also the original (S2_o) generation potential of the source rocks. These values related to the ultimate volumes of hydrocarbon that could be generated at depth in the basin. For the Kyalla Formation, original generation potential (S2_o) averages 108 bbl oil/acre-ft, this is below all of the other formations on the list of unconventional US Shale plays shown below.

Sample Database Averages	HI°	TR	TOCº	S2º	Remaining Potential		Oil Cracked	S1 Free Oil	Estimated Oil	Cracked Gas	
TOC >1%	mg/g TOC		wt%	mg/g Rock	bbl/a-ft	bbl/a-ft	%	bbl/a-ft	bbl/a-ft	M cf/a-ft	
Barnett Shale Ft. Worth Basin	435	0.84	5.38	23.40	94	513	0.40	33	251	1005	
Barnett Shale Delaw are Basin	435	0.91	5.25	22.84	52	500	0.80	32	90	2149	
Woodford Shale Delaw are Basin	480	0.89	6.41	30.79	139	674	0.89	46	60	2854	
Haynesville Shale E. Texas Basin	400	0.98	3.93	15.73	7	344	1.00	3	0	2022	
Fayetteville Shale Arkoma Basin	435	0.95	3.34	14.53	15	318	1.00	10	0	1820	
Woodford Shale Arkoma Basin	520	0.87	5.15	26.80	12	587	0.70	87	170	2431	
Eagle Ford Shale Gulf Coast Basin	520	0.85	3.19	16.61	61	364	0.47	22	161	848	
Marcellus Shale Appalachian Basin	600	0.97	6.44	38.66	34	847	1.00	24	0	4875	
Utica Shale Appalachian Basin	450	0.98	2.74	12.32	6	270	1.00	12	0	1585	
Barnett Shale Oil	450	0.47	5.47	24.64	326	540	0.00	79	213	0	
Barnett Shale Gas	450	0.96	5.58	25.13	23	550	0.87	7	68	2751	
Kyalla	450	0.82	1.09	4.92	22	108	0.02	5	84	8	

Table 4. Geochemical Properties and Generation Potential for US Shale plays and current study.



UNCONVENTIONAL OIL & GAS RISK ASSESSMENT

The Mesoproterozoic Kyalla Formation source rocks in the Burdo 1 well have been evaluated for unconventional oil and gas potential. These source rock samples are presented in a modified geochemical risk assessment diagram (Fig. 3) based upon published results from the Barnett Shale in the Fort Worth Basin. The data illustrated in the star plot represents average values for all four of the diagnostic ratios. Also shown are the recommended areas for unconventional oil (in green) and gas (in red). Data that lies above the minimum threshold and within the shaded areas indicates samples with low geochemical risk for either thermogenic oil or gas production. Data that lie below the minimum threshold and fall in the immature region (in gray) indicate a high risk for commercial shale oil or gas production. Transformation ratios (TR) were calculated based upon HI_o estimates using measured and interpreted fractional composition of kerogen macerals.

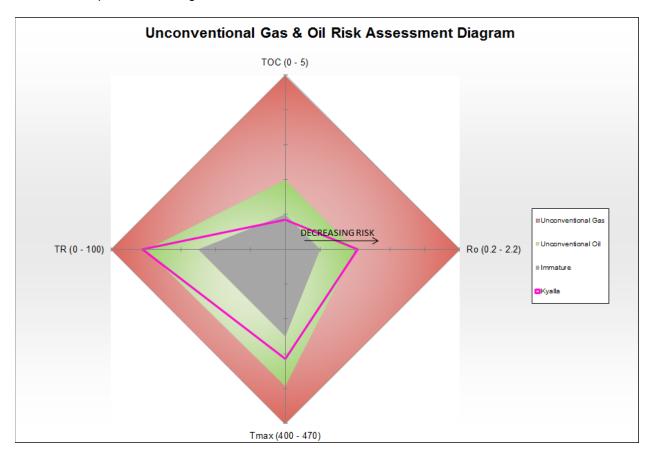


Figure 3. Geochemical Risk Assessment diagram for Mesoproterozoic Kyalla Formation source rocks in the Burdo 1 well.

The Kyalla source rock interval in the Burdo 1 well is interpreted to represent a high geochemical risk for in-situ shale oil production. The average measured TOC content of 0.85 wt.% is below the generally accepted minimum value of 1% TOC to be considered an *effective* source rock for hydrocarbon generation/expulsion (Fig. 3). Some samples do exceed this threshold, predominantly in the basal portion of the Kyalla interval, and this zone could represent a somewhat lower risk target. However, the overall average organic richness is considered marginal and thus the designation of high risk. All of these source rocks are below the minimum requirements of 2 wt.% for *economic* petroleum source rocks, which is also the minimum threshold for prospective shale gas. Original organic matter type is interpreted to be predominantly oil-prone Type II marine algal kerogen. Thermal maturity parameters from programmed pyrolysis generally place the Kyalla source interval in peak oil window. The average Tmax value of 444°C is above recommended minimum value of 435°C for shale oil and well below the minimum of 455°C for



shale gas (Fig. 3). This amount of conversion would likely be sufficient to generate/expel moderate amounts of hydrocarbons from this oil prone source facies. Transformation Ratios (TR), the least constrained risk parameter, average 82% and fall above the recommended minimum of 50% for shale oil and just above the 80% threshold for shale gas systems (Fig. 3). Measured maceral reflectance values in the Kyalla give a mean for low reflectance solid bitumen of 1.03% R_0 , which is above the recommended minimum threshold of 0.5% R_0 for shale oil and just above the minimum of 1.0% R_0 for shale gas (Fig. 3).

In the Kyalla source interval, measured in-situ oil saturation determined by programmed pyrolysis S1 yields is generally poor (avg. 5 bbl oil/acre-ft), which is a significant concern regarding risk assessment for unconventional oil (Fig. 4). Hydrocarbon yield calculations on as-received samples show estimates of average generated oil from the Kyalla at 84 bbl oil/acre-ft, along with a very minor amount (8 Mcf/acre-ft) of secondary cracked gas. As a comparison, a representative example from the core area of Barnett Shale oil production in the Fort Worth Basin has an estimated generated oil yield of 213 bbl/a-ft with a measured in-situ oil saturation of 79 bbl/a-ft (Fig.4). These values are significantly higher compared to the Kyalla, primarily due to differences in organic richness (Barnett Shale oil example has 4.70 wt. % TOC).

It is important to note that the quantity of oil generated from a potential source rock is only one geochemical factor to consider in regard to risk assessment. Equally important is the quality of the oil generated, since this factor can be a critical element in assessing the movability and ultimate recovery. The interpreted thermal maturity of the Kyalla source interval in this well is in the peak oil window and hydrocarbon saturation is likely to be fairly light and mobile. However, the presence of solid bitumen could also indicate a source interval with restricted microporosity. Such microporosity is considered necessary for recovery of in-situ oil saturation and can be better assessed using scanning electron microscopy (SEM). Source rock extract fingerprints and bulk fractional compositional analyses from select Kyalla samples would also aid in the determination of the quality of the in-situ hydrocarbon saturation and provide a better assessment of their movability and ultimate recovery potential.

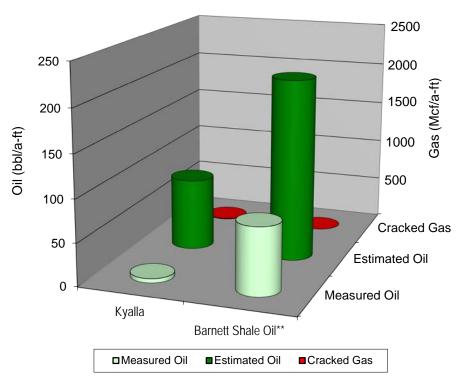


Figure 4. Hydrocarbon yield estimates for the Mesoproterozoic source rocks in the Burdo 1 well compared to Barnett Shale in the oil window.



GEOCHEMICAL SUMMARY

The Kyalla source interval in the Burdo 1 well is interpreted to represent high geochemical risk for unconventional shale oil development. The average measured TOC content of 0.85 wt.% is below the generally accepted minimum value of 1% TOC for unconventional shale oil, although the basal section of this source rock interval does have relatively higher TOC values. The Kyalla source rock is thought to contain dominantly oil-prone Type II kerogen. Thermal maturity parameters indicate that this source interval is in the late oil window, 0.84% Calc. R_o and 1.03% Eq. R_o from solid bitumen reflectance. All key thermal maturity risk ratios are above recommended minimum thresholds for shale oil systems. While the Kyalla has likely generated minor to moderate amounts of oil (avg. 84 bbl oil/acre-ft), comparison to other systems such as the Barnett Shale show in-situ oil saturations are much lower for the Kyalla. Risk criteria like the S1 versus TOC show no oil cross-over for any of the samples within this unit, also supporting a high risk assessment. Further evaluation of in-situ oil characteristics would be required to fully evaluate potential oil mobility and recovery risk.



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Appendix I

Hydrocarbon Yield Calculation Beetaloo Sub-Basin Group Burdo 1

McArthur Basin Integrated Petroleum Geochemistry, 2016 Northern Territory Geological Survey - Australia



Burdo 1 Hydrocarbon Yield Calculation

																S2 (meas)	S2 (orig)				
Sample	Top Depth	TOC*	HI*	S1*	S2*	Calc.Ro	PI*	%Type IV 50 HIP	% Type III 125 HIP	%Type II 450 HIº	%Type I 750 HI⁰	HIº	TR	TOCº	S2º	Remaining Potential	Original Potential	Oil Cracked	S1 Free Oil	Estimated Oil	Cracked Gas
Burdo 1	(m)	wt%	mg/g TOC	mg/g Rock	mg/g Rock	%		30 Hi	125 111	430 Hi	730 HI	mg/g TOC		wt%	mg/g Rock	bbl/a-ft	bbl/a-ft	%	bbl/a-ft	bbl/a-ft	Mcf/a-ft
TN14DJR072	753	0.50	64	0.05	0.32	0.68	0.14	0	0	100	0	450	0.91	0.66	2.99	7	66	0.00	1	59	0
1394668	768	0.69	223	0.19	1.54	0.71	0.11	0	0	100	0	450	0.62	0.83	3.74	34	82	0.00	4	48	0
TN14DJR074	780	0.95	62	0.08	0.59	0.73	0.12	0	0	100	0	450	0.91	1.26	5.66	13	124	0.00	2	111	0
TN14DJR075	789	1.03	79	0.09	0.81	0.70	0.10	0	0	100	0	450	0.88	1.35	6.06	18	133	0.00	2	115	0
1394669	801	1.39	371	0.66	5.16	0.78	0.11	0	0	100	0	450	0.28	1.53	6.87	113	150	0.00	14	37	0
TN14DJR076	801	0.76	206	0.20	1.56	0.73	0.11	0	0	100	0	450	0.66	0.92	4.15	34	91	0.00	4	57	0
TN14DJR077	810	0.77	92	0.11	0.71	0.76	0.13	0	0	100	0	450	0.86	1.01	4.53	16	99	0.00	2	84	0
1394670	822	0.44	159	0.07	0.70	0.81	0.09	0	0	100	0	450	0.75	0.55	2.47	15	54	0.00	2	39	0
1394671	840	0.36	106	0.03	0.38	0.85	0.07	0	0	100	0	450	0.84	0.46	2.09	8	46	0.00	1	37	0
TN14DJR079	858	0.40	45	0.03	0.18	0.83	0.14	0	0	100	0	450	0.93	0.54	2.42	4	53	0.00	1	49	0
1394672	870	0.52	185	0.11	0.96	0.90	0.10	0	0	100	0	450	0.70	0.64	2.88	21	63	0.01	2	42	3
TN14DJR080	879	0.49	61	0.05	0.30	0.88	0.14	0	0	100	0	450	0.91	0.65	2.93	7	64	0.00	1	57	0
TN14DJR081	891	1.07	110	0.14	1.18	0.78	0.11	0	0	100	0	450	0.83	1.37	6.18	26	135	0.00	3	110	0
1394673	897	0.75	209	0.28	1.57	0.83	0.15	0	0	100	0	450	0.65	0.92	4.13	34	90	0.00	6	56	0
TN14DJR083	909	0.70	78	0.08	0.54	0.82	0.13	0	0	100	0	450	0.88	0.91	4.10	12	90	0.00	2	78	0
1394674	924	0.92	211	0.37	1.94	0.87	0.16	0	0	100	0	450	0.65	1.13	5.06	42	111	0.00	8	68	0
TN14DJR084	930	0.85	81	0.11	0.69	0.88	0.14	0	0	100	0	450	0.88	1.11	5.01	15	110	0.00	2	95	0
TN14DJR085	939	1.18	78	0.11	0.92	0.86	0.11	0	0	100	0	450	0.88	1.54	6.94	20	152	0.00	2	132	0
1394675	948	0.48	165	0.23	0.79	0.94	0.23	0	0	100	0	450	0.74	0.61	2.74	17	60	0.03	5	41	8
TN14DJR086	960	0.92	51	0.07	0.47	0.93	0.13	0	0	100	0	450	0.93	1.23	5.51	10	121	0.02	2	108	16
TN14DJR087	969	0.97	51	0.07	0.49	1.03	0.13	0	0	100	0	450	0.93	1.28	5.77	11	126	0.11	2	103	76
TN14DJR088	981	0.83	34	0.07	0.28	1.02	0.20	0	0	100	0	450	0.95	1.11	5.02	6	110	0.10	2	94	61
1394676	984	0.39	44	0.08	0.17	0.84	0.32	0	0	100	0	450	0.94	0.53	2.37	4	52	0.00	2	48	0
1394070	990 996	0.39	136	0.13 0.07	0.53 0.21	0.96 0.84	0.20	0	0	100	0	450 450	0.79	0.50	2.25 2.17	12 5	49 47	0.04	<u>3</u>	36	10
TN14DJR089	990	0.36	58 27	0.07	0.21	1.11	0.20	0	0	100 100	0	450	0.91 0.96	0.48	4.44	4	97	0.00 0.19	1	43 75	105
111140311009	1005	0.73	68	0.03	0.20	0.84	0.25	0	0	100	0	450	0.90	0.59	2.63	7	58	0.19	2		0
TN14DJR091	1011	1.19	129	0.10	1.53	0.72	0.24	0	0	100	0	450	0.80	1.53	6.90	34	151	0.00	11	118	0
114142010001	1020	0.54	80	0.48	0.43	0.84	0.30	0	0	100	0	450	0.88	0.72	3.22	9	71	0.00	4	61	0
TN14DJR092	1023	0.54	33	0.08	0.18	0.70	0.31	0	0	100	0	450	0.95	0.73	3.27	4	72	0.00	2	68	0
1394677	1032	0.89	147	0.21	1.31	0.90	0.14	0	0	100	0	450	0.77	1.12	5.06	29	111	0.01	5	81	5
	1041	1.26	128	0.47	1.61	0.89	0.23	0	0	100	0	450	0.80	1.62	7.30	35	160	0.00	10	125	0
TN14DJR093	1047	1.06	135	0.41	1.43	0.87	0.22	0	0	100	0	450	0.79	1.36	6.12	31	134	0.00	9	103	0
TN14DJR094	1056	1.07	121	0.33	1.29	0.90	0.20	0	0	100	0	450	0.82		6.21	28	136	0.00	7	108	0
	1059	0.98	114	0.28	1.12	0.90	0.20	0	0	100	0	450	0.83	1.27	5.70	25	125	0.01	6	99	6
TN14DJR095	1065	1.20	113	0.37	1.36	0.94	0.21	0	0	100	0	450	0.83	1.55	6.99	30	153	0.03	8	119	25
1394678	1068	0.88	174	0.60	1.53	0.99	0.28	0	0	100	0	450	0.73	1.12	5.04	34	110	0.07	13	71	34
TN14DJR096	1074	1.27	100	0.40	1.27	0.89	0.24	0	0	100	0	450	0.85	1.66	7.46	28	163	0.00	9	136	0
	1080	1.15	161	0.73	1.85	0.80	0.28	0	0	100	0	450	0.75	1.47	6.61	41	145	0.00	16	104	0
TN14DJR097	1086	1.19	147	0.48	1.75	0.47	0.22	0	0	100	0	450	0.77	1.52	6.82	38	149	0.00	11	111	0
TN14DJR098	1095	1.27	94	0.35	1.20	0.78	0.23	0	0	100	0	450	0.86	1.66	7.47	26	164	0.00	8	137	0
1394679	1098	0.92	224	0.79	2.06	0.45	0.28	0	0	100	0	450	0.64	1.14	5.15	45	113	0.00	17	68	0
	1098	1.04	107	0.49	1.11	0.89	0.31	0	0	100	0	450	0.84	1.36	6.13	24	134	0.00	11	110	0
TN14DJR100	1104	1.35	85	0.36	1.15	0.82	0.24	0	0	100	0	450	0.87	1.77	7.98	25	175	0.00	8	149	0
TN14DJR101	1116	1.38	62	0.27	0.86	0.81	0.24	0	0	100	0	450	0.91	1.83	8.24	19	180	0.00	6	162	0
	1119	0.99	73	0.31	0.72		0.30	0	0	100	0	450	0.89	1.31	5.92	16	130	0.00	7	114	0
TN14DJR102	1128	1.08	89	0.27	0.96		0.22	0	0	100	0	450	0.87	1.42	6.37	21	140	0.00	6	118	0
1394680	1137	0.57	195	0.34	1.11	1.05	0.23	0	0	100	0	450	0.69	0.71	3.21	24	70	0.12	7	40	34
	1140	0.50	96	0.25	0.48	0.84	0.34	0	0	100	0	450	0.86	0.66	2.98	11	65	0.00	5	55	0
Kyalla (A	Avg)	0.85	115	0.25	1.02	0.84	0.19	0	0	100	0	450	0.82	1.09	4.92	22	108	0.02	5	84	8
Barnett Sha		4.70	300	3.60	14.90		0.20	0	0	100	0	450	0.47	5.47	24.64	326	540	0.00	79	213	0
Barnett Sh		4.21	26	0.33	1.07		0.24	0	0	100	0	450	0.96	5.58	25.13	23	550	0.87	7	68	2751
Notes: Calc.Ro values in	hold one coloule				d fant and intermed	ad from other a	a a a b a mi a	al matumitre data	haaanaa Tmar m	oo oomaidamad s	unualiahla All	othor Colo Do vol									

Notes: Calc.Ro values in **bold** are calculated from measured Tmax. Calc.Ro values in **red font** are intrepreted from other geochemical maturity data because Tmax was considered unreliable. All other Calc.Ro values are formation specific averages because Tmax was considered unreliable.

Kerogen Type in **bold** have visual kerogen data for estimates TR = Transformation Ratio (fractional conversion) (Original Potential - Remaining Potential) = (Estimated Oil + Cracked Gas)

Estimated Oil and Cracked Gas yield data assume complete conversion and no expulsion of hydrocarbon products and the proportion between each is based on empirical Ro calculated % cracking.

Yields do not represent recoverable products and are intended primarily for comparison purposes, yield calculations based on carbon mass balance are likely to be overestimations.

**Estimated parameters for productive Barnett Shale in the Ft. Worth Basin

Hydrocarbon yield calculations and formulas are fully documented in the appendix section of Jarvie et al. (2007)

