

SEISMIC DATA PROCESSING REPORT

FOR

PACIFIC OIL AND GAS PTY. LTD.

**1990 SCARLET HILL SEISMIC SURVEY
McARTHUR BASIN**

**1990 ELSEY SEISMIC SURVEY
McARTHUR BASIN**

OPEN FILE

OPEN FILE

**LOCATION : NORTHERN TERRITORY
COMPILED BY : SIMON-HORIZON AUSTRALIA
PTY. LTD.**

OCTOBER 1991

ONSHORE

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1. INTRODUCTION

The Field Survey was undertaken by GEOSYSTEMS PTY LTD in August 1990

The lines recorded in the whole survey comprised of :

Mcarthur basin

| | |
|----------|----------|
| SH90-100 | 40.0 km |
| SH90-102 | 46.4 km |
| SH90-103 | 100.0 km |
| SH90-105 | 30.0 km |
| SH90-107 | 20.0 km |
| SH90-109 | 10.0 km |
| EL90-201 | 60.0 km |

For a total of 306.4 kilometres.

Processing was conducted by Simon-Horizon Australia, at their Perth office. Final filming was completed by July 1990.

2. FIELD SURVEY INFORMATION

ACQUISITION PARAMETERS - Scarlet Hill / Elsey

| | |
|------------------------------|-----------------------------------------------------------------------------------------------------------------------|
| Source | Vibroseis |
| Source pattern | 4 Vibrators in line 36m (12m Pad to Pad) stacked array |
| Sweep Frequency | 7 Varisweeps per VP 10 - 30 Hz 20 - 66 Hz 12 - 48 Hz 13 - 52 Hz 24 - 66 Hz 10 - 36 Hz 28 - 66 Hz |
| Sweep Emphasis | linear - 250 msec taper |
| Sweep Length | 6.0 Seconds |
| VP Interval | 45 metres |
| Number of data channels | 500 |
| Spread configuration offsets | 3742.5-7.5-X-7.5-3742.5 m |
| Group interval | 15 m |
| Geophone configuration | 6 geophones in line with 2.5m spacing over 12.5m |
| Geophone type | MARK L21A (10 Hz) |
| Recording instrument | GEOCOR IV (16 SIGN-BIT) |
| Record length | 4 seconds (correlated) |
| Sample period | 2 msec |
| Tape format | Geosystems (correlated) 1600 bpi |
| COVERAGE | 8333 % |
| Polarity | Upward movement of geophone recorded with negative value on tape. |

FIELD DATA SUPPORT MATERIAL

The following support information was provided

- a) Observers Reports.
- b) Vibrator Parameter Reports.
- c) Receiver Parameter Reports.
- d) Elevations listing.
- e) Intersection Diagrams.
- g) Uphole plots.

DATA PROCESSING PARAMETERS

- 1) DEMULTIPLEX Transcribe Geosystems format field tapes to HORIZON'S internal format
Resample from 2 to 4 msec sample period.
- 2) GAIN RECOVERY 0.0t + 10.0Log(t) (Scarlet Hill)
1.0t + 10.0Log(t) (Elsley)
- 3) DISPLAY Display of shot records for quality control monitoring and for edit of noise contaminated traces.
- 4) TRACE SUMMING Receiver array simulation. 1:2:1 trace weights. No trace summing for Elsey.
- 5) LINE GEOMETRY CREATION
- 6) FK FILTER Lozenge type FK filter applied to attenuate ground roll.
- 7) CDP SORT Reorder traces from common shot record gathers into common depth point gathers.
- 8) DECONVOLUTION Predictive Deconvolution. 20 msec gap 120 msec operator, 1% white noise.

 Design windows (Scarlet Hill)
 200-2100 msec @ near offset
 1100-2600 msec @ far offset

 Design windows (Elsley)
 100-1500 1400-3200 msec @ near offset
 1100-2500 1800-3200 msec @ far offset
- 9) STATICS - (1) The mean datum static is calculated for each CDP, and the relative static (the difference between the CDP mean static and the individual traces' total static) applied.

- 10) RESIDUAL STATICS Surface consistent solution where the maximum allowable shift was +/- 20 msec. NMO corrections were performed using velocities chosen from preliminary CVS velocity analyses performed at 2.0 Km intervals Kmintervals.
- 11) DIP MOVEOUT Kirchoff summation implementation on 31 equal migration offset ranges.
- 12) VELOCITY ANALYSES CVS velocity analyses were performed over 21 cdp's at approximately 1.0 Km intervals. The velocity functions are referenced to surface.
- 13) NMO CORRECTIONS
- 14) MUTE Each line has its own mute/mutes.
- 15) SCALING 800msec AGC.
- 16) STATICS - (2) The cdp mean static was applied, correcting from floating datum to datum.

DATUM: 200 m above sea level. New time origin of -200 msec.
- 17) RESIDUAL STATICS A CDP trim solution calculated on a 7 trace pilot with a maximum allowable shift of +/- 12 msec.
- 18) STACK CDP stack using a square root compensation.

- 19) ZERO PHASE 1 Operator averaged over 11 traces:
- DECONVOLUTION Design Desired output
- (Scarlet Hill) 0 - 1500 msec 12 - 48 Hz
- (Elsey) 0 - 1500 msec 12 - 60 Hz
-
- 20) BAND-PASS FILTER 12 - 45 Hz -200 to 1000 msec
- (Scarlet Hill) 10 - 45 Hz 1300 to 1700 msec
- 10 - 40 Hz 2000 to 2800 msec
- (Elsey) 14 - 55 Hz -200 to 700 msec
- 12 - 50 Hz 1200 msec
- 10 - 50 Hz 1700 msec
- 10 - 45 Hz 2700 msec
-
- 21) SCALING 800 msec fixed length window
-
- 22) TAU-P FILTER Time variant dip and coherency filter.
- 70% of original data (Scarlet Hill)
- 75% of original data (Elsey)
-
- 23) MIGRATION Wave equation migration using 95% of smoothed stacking velocities - second order Finite Difference solution.

NOTE : Q-DECON AND F-X PREDICTIVE NOISE REDUCTION WERE USED
 INSTEAD OF ZERO PHASE DECON FOR LINES SH90-100 AND
 SH90-103

4. DATA PROCESSING TESTS

Mute tests were conducted on each line

| | |
|----------|-----------------------------------------------------------------|
| SH90-107 | FK TRIALS |
| SH90-107 | DECON BEFORE STACK TRIALS |
| SH90-107 | PRE-STACK FILTER TRIALS |
| SH90-107 | SPECTRAL WHITENING TRIALS |
| SH90-107 | POST SPECTRAL WHITENING FILTER TRIALS |
| SH90-107 | MIGRATION TRIALS OF 100% TO 85% VELOCITIES |
| SH90-103 | DAS TRIALS |
| SH90-103 | MULTI-CHANNEL RANDOM NOISE ATTENUATION BY SIGNAL PREDICTION. |
| SH90-103 | QDECON - INVERSE-Q COMPENSATION. |

5. STATICS COMPUTATION

Refraction breaks were picked by hand from the production breaks and statics derived using the Gardner/Layat method (see below). Breaks were picked in both the forward and reverse directions, and intercept times converted to one way statics. The refraction statics were compared with the uphole statics and differences computed at each uphole location.

A difference profile was then produced by linear interpolation. Final uphole "calibrated" statics were derived by combining the difference and refraction profiles.

GARDNER/LAYAT WEATHERING STATICS METHOD

The weathering statics method used has its development in the procedures established by Gardner and Layat. Trace by trace shot and receiver corrections are derived by establishing a continuous intercept curve from refraction breaks picked from the acquired data.

Intercept time is essentially the difference between the actual travel time of the refracted wave and the time if the wave had travelled a straight line between shot and receiver at the subweathering velocity, or $I = T - X/V_m$. With the redundancy in multi-fold coverage, intercept curves are developed which are the accumulated differences of the variations in time between traces encountering the velocity marker at the base of marker velocity, as described in the above equation. These curves are possible errors in the estimation of the marker velocity.

Intercept times are reduced to one way statics by the equation $S = K1$, where $K = 1/2 \cos \theta (V_w/V_c - 1)$, resulting in a profile which gives a static at every surface position.

Details on the theoretical background for the method may be found in the paper "Modified Gardner Delay Time and Constant Distance Correlation Interpretation" by C. Layat, printed in the S.E.G. publication "Seismic Refraction Prospecting".

6. FINAL DISPLAY

Final display were produced on films using a GEOSPACE 6400 plotter.

DISPLAY SCALES

Scarlet Hill / Elsey

| | | | |
|----------------|---------|-----------------|------------|
| FINAL STACK | 1:25000 | 42.33 tr/in and | 5.0 in/sec |
| MIGRATED STACK | 1:12500 | 21.16 tr/in and | 5.0 in/sec |
| | 1:25000 | 42.33 tr/in and | 5.0 in/sec |
| | 1:50000 | 84.66 tr/in and | 5.0 in/sec |

APPENDIX A

LIST OF FIELD TAPES

| LINE | TAPES | VP RANGE |
|----------|-----------------|------------|
| SH90-100 | 90A200 - 90A235 | 100 - 2767 |
| SH90-102 | 90A063 - 90A108 | 100 - 3196 |
| SH90-103 | 90A109 - 90A199 | 6769 - 100 |
| SH90-105 | 90A033 - 90A062 | 2101 - 100 |
| SH90-107 | 90A002 - 90A022 | 1435 - 100 |
| SH90-109 | 90A023 - 90A032 | 100 - 769 |
| EL90-201 | 90A236 - 90A289 | 4099 - 100 |

APPENDIX B

PURCHASE TAPES

Two archive tapes were produced containing the Raw Stacks and the Migration Stacks. There is a description block separating each data set which contains the line number and a description of the data which follows.

All tapes were produced in SEG Y 32 bit IBM Floating Point format.

The time of first sample is -200 msec.

Reel number MC-100 - Raw Stack Archive of lines:
SH90-100,102,103,105,107,109
EL90-201 and 89-203

Reel number MC-200 - Migrated Stack Archive of lines:
SH90-100,102,103,105,107,109
EL90-201 and 89-203

A velocity tape was created for Mcarthur Basin.

APPENDIX C

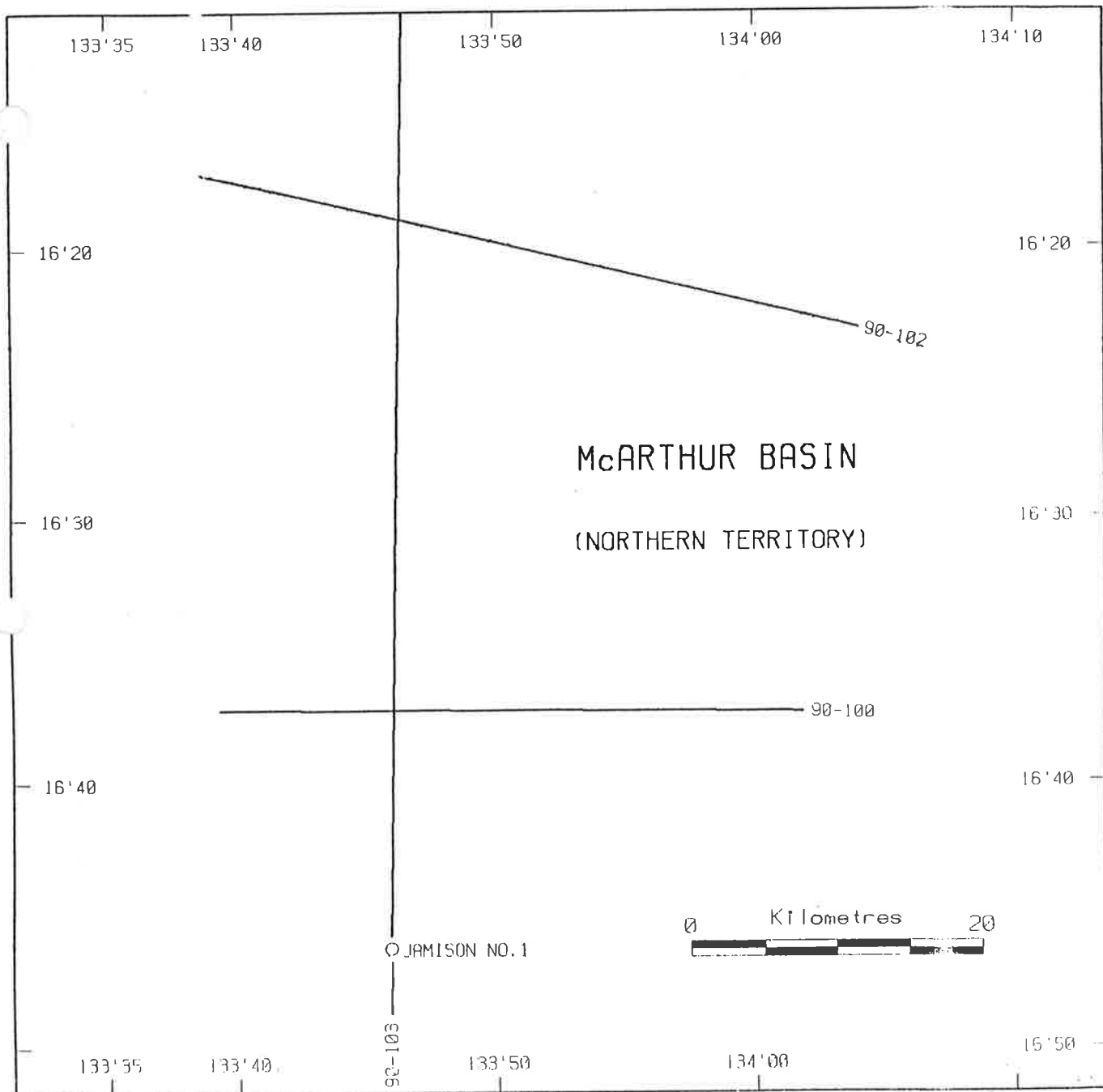
DATA DISPOSAL

| DATA | DISPOSAL | DATE |
|---------------------------------|-------------------------------------------------------------------------|----------|
| Field Tapes | Encom Technology 24 Queen Parade, North Fitzroy, Victoria 3065 | 29/07/91 |
| Archive Tapes | Pacific Oil And Gas 826 Whitehorse Road Boxhill Victoria 3128 | 04/06/91 |
| Film Display | Pacific Oil And Gas 826 Whitehorse Road Boxhill Victoria 3128 | 01/10/91 |
| Shot Record Display | Pacific Oil And Gas 826 Whitehorse Road Boxhill Victoria 3128 | 01/10/91 |
| Observer's Logs Uphole Plots | Pacific Oil And Gas 826 Whitehorse Road Boxhill Victoria 3128 | 01/10/91 |

NOTE: Velocity analyses displays were destroyed after the velocity tape was created

APPENDIX D

LINE LOCATION MAP



APPENDIX D

LINE LOCATION MAP

