

**A LOGISTICS REPORT FOR A
GRAVITY AND MAGNETICS SURVEY
CONDUCTED AT THE ANTRIMS JV
BIRRINDUDU, NT
FOR
BHP BILLITON**

FUGRO GROUND GEOPHYSICS PROJECT NUMBER G2052

**August, 2002
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1. INTRODUCTION

1.1 GENERAL

Between Thursday 4th July and Tuesday 22nd July 2002, Fugro Ground Geophysics Pty Ltd conducted a Gravity and Magnetism survey for BHP Billiton, near Birrindudu Station in the Northern Territory.

The survey was conducted on ten (10) individual locations, with a gravity crosshair done over eight of the locations, and magnetism on all locations. A total of 444 gravity stations were observed, together with 88.1km of magnetism traverses.

1.2 EQUIPMENT AND PERSONNEL

A Garmin GPS2+ handheld GPS was used to navigate to each point for the gravity acquisition and to flag the line positions for the magnetism traverses. A geodetic-grade GPS (Ashtech Z-12) was used to record all pseudo range and phase information simultaneously with the acquisition of the gravity data. The On The Fly (OTF) processing of this GPS data generated positional information used in the gravity processing. Gravity data was acquired using a LaCoste & Romberg Model G gravimeter, with magnetism data acquired using a Geometrics G-856 proton precession magnetometer. While repeatable, the magnetism data exhibited high gradients and rapid station to station changes as could be expected over basalts.

Fugro Ground Geophysics supplied a complete camp and food for the crew, together with all geophysical equipment and a Toyota 4x4 vehicle. BHPB supplied fuel and water from Birrindudu Station.

The following Fugro Ground Geophysics personnel acquired and processed the gravity/GPS data:

GRAVITY/MAGNETICS PERSONNEL

PERSONNEL	POSITION
Doug Hall	Crew Chief
Morris Wallace	Geophysical Technician

The following equipment was supplied on site by FUGRO GROUND GEOPHYSICS for magnetics, gravity and GPS data acquisition and processing.

Num	HARDWARE
1	Lacoste and Romberg Model G gravity meter.
3	Ashtech Z-12 geodetic grade-GPS receivers.
4	Geometrics G-856 Proton Magnetometers
1	Garmin GPS 2+ navigation GPS
1	Pentium II laptop computer for GPS processing
1	HP 320 Deskjet Printer
1	Four wheel drive vehicles
1	Inmarsat Satellite telephone
	Safety equipment - survival/first aid kits, EPIRB
	Tripods, Wild Optical level, compasses etc.
	SOFTWARE
	GRAVI Gravity Processing software
	Ashtech PNAV GPS processing software
	Geometrics MAGMAP 2000 for magnetics processing

2. SURVEY PROCEDURE AND SPECIFICATIONS

2.1 DATA ACQUISITION

The gravity/GPS survey consisted of a total of 444 stations which were acquired at a 40m spacing in a crosshair over the centre of each target. Line length varied between 1000 and 1200m. The GPS data was processed with OTF to calculate elevation and position to sub-decimetre accuracy. Repeat readings were taken at the cross over of each line.

Magnetics data was acquired at a 10m station spacing on lines 200m apart. A base magnetometer was established at the camp to provide diurnal corrections.

The following table summarises the specifications for this survey.

PARAMETERS	All Grids - Gravity	Magnetics
Line Spacing	Crosshair	200m
Station Spacing	40 m	10m
Line Direction	E-W, N-S	N-S
Number of Stations	444	
Number of Lines	16	
Number of Repeats	12	
Navigation	Garmin GPS2+	
Surveying	OTF	
Loops	101-108	

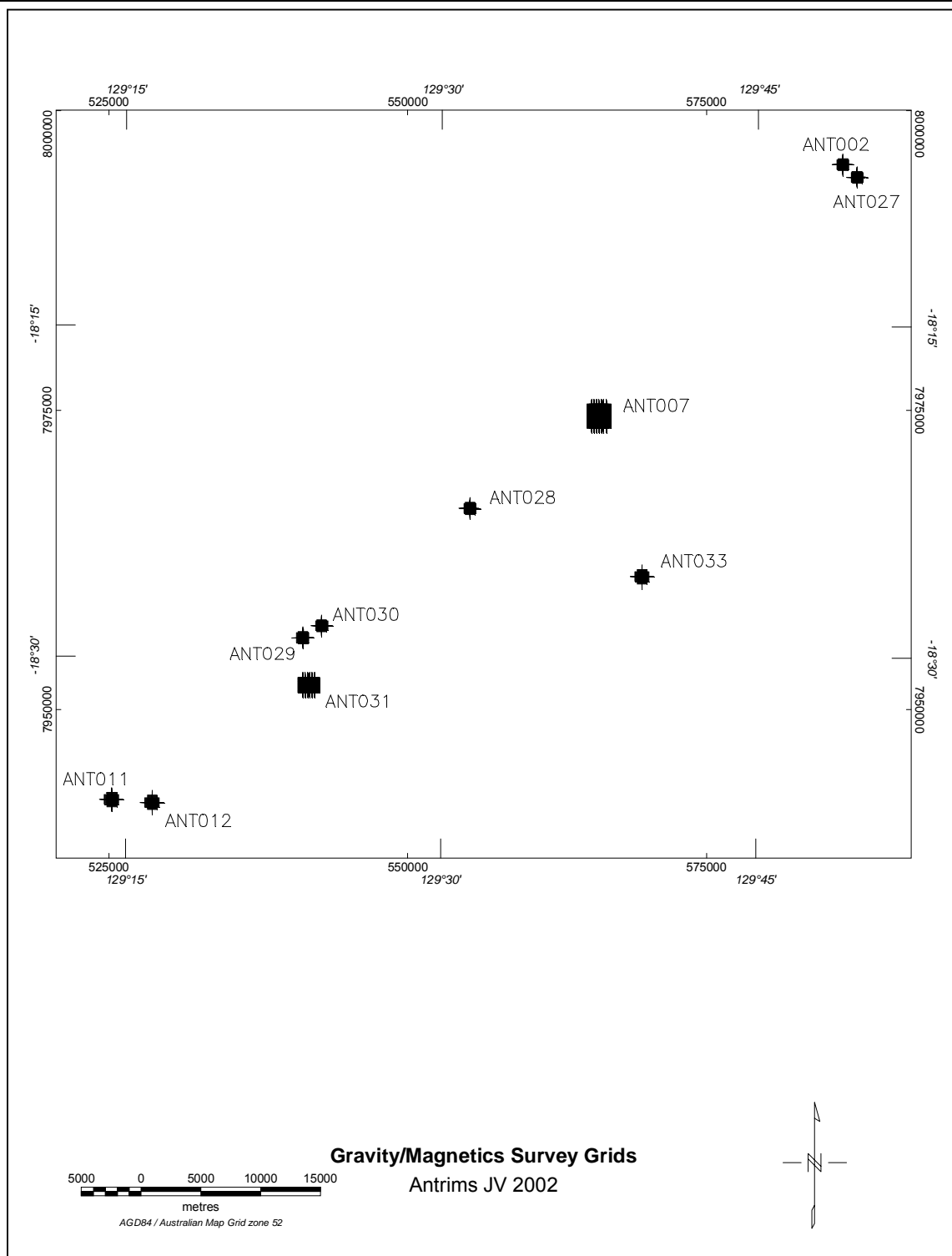


Figure 1. Antrims JV survey area.

2.2 NAVIGATION

Cross country station to station navigation was accomplished using a stand alone Garmin GPS2+ GPS receiver. This GPS unit was mounted on the dashboard of the vehicle and connected to a roll cage mounted external antenna. After entering the desired waypoint, it displayed the vehicle's track and bearing and range to the destination in real time.

2.3 BASE STATION ESTABLISHMENT

There are two reasons for the establishment of gravity base stations: Datum control and drift control.

2.3.1 Datum Control

The gravity meter measures only the relative changes in gravity and not the absolute value of gravity. Giving each station an absolute value of gravity is not critical if the survey is small and independent from all other past and planned surveys. Surveys forming part of an on-going exploration program and/or covering large areas need to be tied into a base with a known absolute gravity value to allow merging of different survey data sets and for correct application of latitude corrections (latitude correction is a non-linear function of latitude, so relative corrections should only be applied to small survey areas).

To facilitate datum control, the Bureau of Mineral Resources (now Geoscience Australia or GA) has established a national gravity base station network consisting of 200 equidistant bases throughout Australia. Of these, 60 bases were subsequently tied directly to at least one of the five absolute gravity measurement sites in Australia that were measured in 1979. These measurement sites are compatible with the International Gravity Standardisation Net 1971 (IGSN71) and referred to as Isogal84 values. It is important that the 1967 International Gravity Formula is used in reducing observations on the IGSN71 datum (the 1930 formula only applies to observations on the Potsdam datum).

One permanent gravity base was established roughly in the centre of the project area, along the road into Birrindudu Station, which served as a starting and ending point for the gravity loops. The gravity base, called DUDU, was tied to a GA base in Halls Creek located at the airport (6491.0129). For DUDU a observed gravity value of 978438.43 milligals was registered. The location of DUDU is shown in Figure 2 on the following pages together with gravity loop details for the ties.

64910129

Loop 0001 Ip Time 6.2hrs Drift -0.02 VALUE: 978447.30
 Parent Base Out 64910129 Value: 978447.30 Time: 11.10
 Parent Base In CAMP Value: 978439.35 Time: 17.28

Loop 0002 Ip Time 8.2hrs Drift 0.01 VALUE: 978447.29
 Parent Base Out CAMP Value: 978439.35 Time: 6.23
 Parent Base In CAMP Value: 978439.35 Time: 14.40

Loop 0002 Ip Time 8.2hrs Drift 0.01 VALUE: 978447.30
 Parent Base Out CAMP Value: 978439.35 Time: 6.23
 Parent Base In CAMP Value: 978439.35 Time: 14.40

CAMP

Loop 0001 Ip Time 6.2hrs Drift -0.02 VALUE: 978439.34
 Parent Base Out 64910129 Value: 978447.30 Time: 11.10
 Parent Base In CAMP Value: 978439.35 Time: 17.28

DUDU

Loop 0003 Ip Time 8.3hrs Drift 0.00 VALUE: 978438.42
 Parent Base Out CAMP Value: 978439.35 Time: 8.49
 Parent Base In DUDU Value: 978439.35 Time: 17.20

Loop 0004 Ip Time 4.2hrs Drift 0.04 VALUE: 978438.43
 Parent Base Out CAMP Value: 978439.35 Time: 7.07
 Parent Base In CAMP Value: 978439.35 Time: 11.31

Loop 0005 Ip Time 11.1hrs Drift 0.00 VALUE: 978438.44
 Parent Base Out CAMP Value: 978439.35 Time: 6.51
 Parent Base In CAMP Value: 978439.35 Time: 18.04

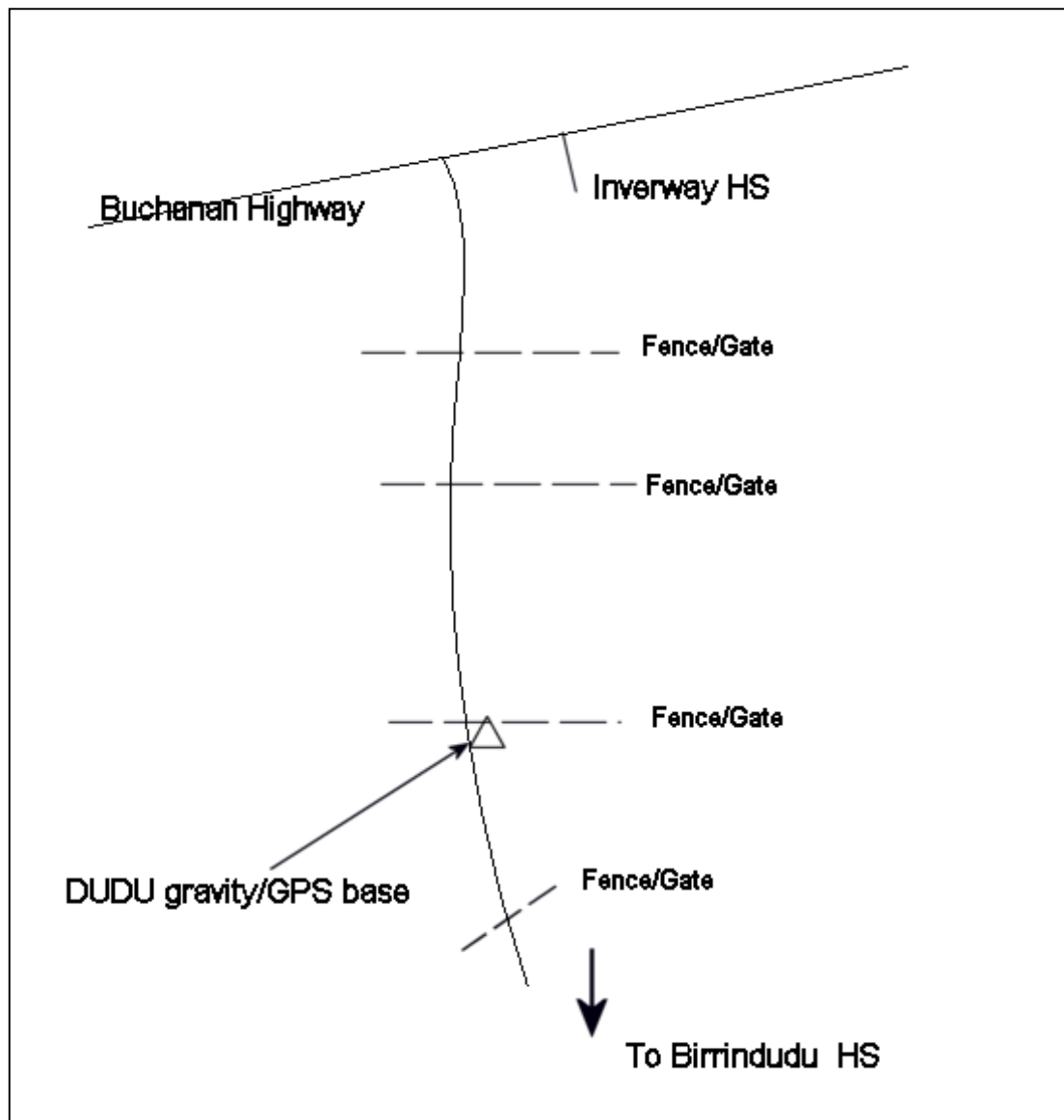


Figure 2. GPS and gravity base DUDU. (schematic only)

2.3.2 Drift Control

Drift has two components, a cyclic component due to the time varying gravitational effects of the sun and moon, and an approximately linear component due to instrumental drift. The tidal effects are removed using Longman's algorithm which calculates the tidal correction to a resolution of 0.01 mgals. As the remaining drift is predominantly linear, gravity loop times can be extended to cover the full day.

This offers a number of advantages :

- Most loops are directly tied to primary bases reducing accumulated errors generated from tying secondary bases to other secondary bases.
- Removes the need to set up a series of temporary bases along the survey line.
- Instrument drift rate is often less than reading error, even for long duration loops.

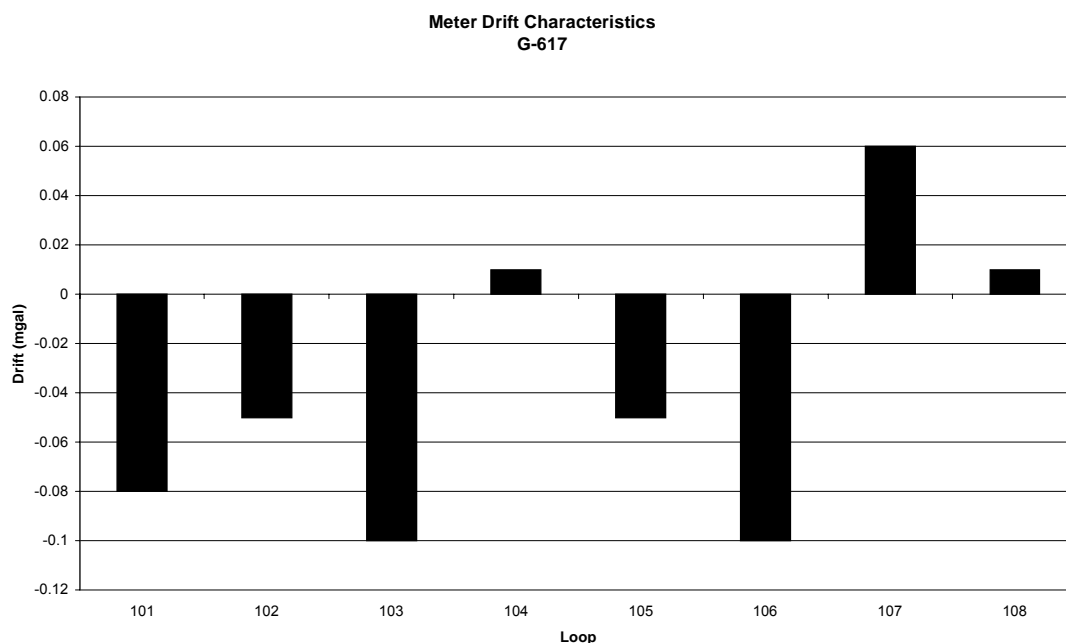


Figure 3. Instrument drift for meter G617

The gravity meter, being a mechanical instrument consisting of beams, weights and springs, suffers from drift due to minute stretching of the spring mechanism. This drift can be removed provided each survey loop starts and ends at the same gravity station or at two different stations each of known value of gravity. For this survey, gravity loops are tied into the gravity base station DUDU. Drift values for G-617 are shown above.

2.4 GRAVITY REPEATS

An operational procedure that includes 5% repeats provides both quality control and confirmation of the linearity of the mechanical drift. The repeats are used as secondary bases to isolate and reduce the amount of field data recovery in the instances where excessive tares have occurred. On this survey, the layout of the gravity lines and grids made this repeat level impractical to achieve. Repeats were observed at the line crossovers and generally at the start and end of the grid with the GPS base station located beside the first station.

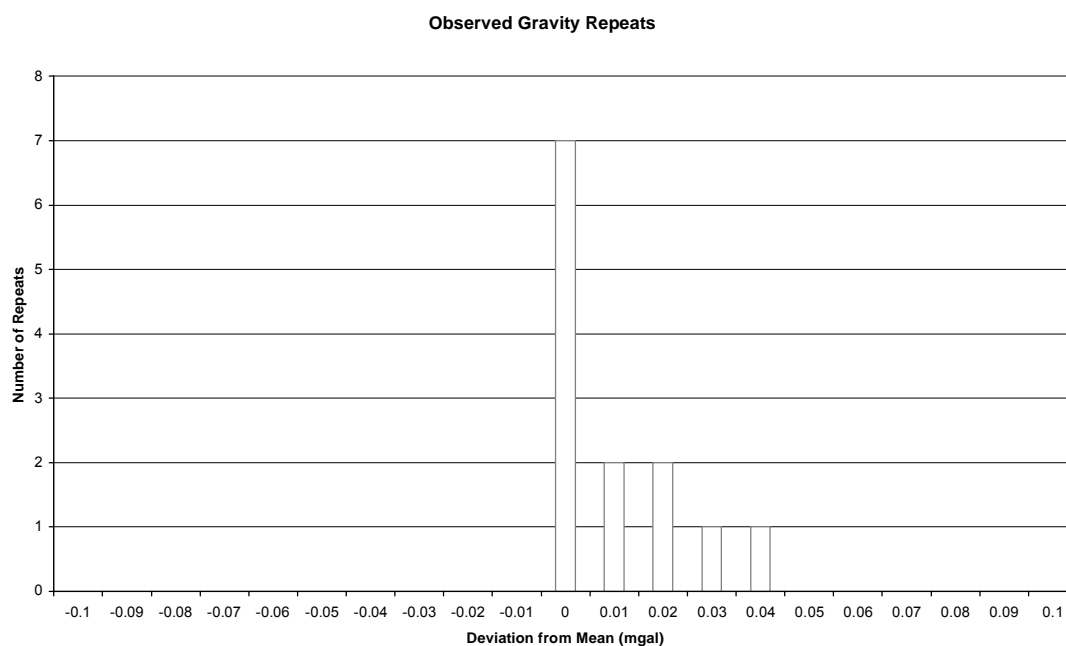


Figure 4. Statistical distribution of gravity repeats

For this survey a total of 13 stations were reoccupied for drift control. Figure 6 demonstrates the distribution of the repeats.

2.5 GPS SURVEYING

Unlike most other geophysical methods, observed gravity requires accurate survey information before the technique can usefully be used in sub-surface mapping. The gravity response to elevation and position can far exceed sub-surface anomaly amplitudes. The effects are approximately 0.20 mgals per meter of elevation and 0.5 mgals per kilometre of north-south position. Therefore real-time GPS (± 20 metres) is totally inadequate while real-time differential GPS (± 5 metres) would produce ± 1 mgal errors. There are three GPS methods that can provide adequate quality survey data for gravity reductions. These are:

METHOD	DESCRIPTION	ELEV ERROR	GRAV ERROR
Rapid Static	Relies on the mobile receiver remaining stationary for 5 to 30 minutes depending on the distance between the base and mobile receivers. Very accurate but slow.	$\pm 2\text{cm}$	$< .01$ mgals
Real Time Kinematic (RTK)	Tracks satellites continuously and relies on a radio telemetry link with the GPS base station. Observations at the base are transmitted to the rover receiver together with the position of the base receiver, allowing it to calculate the vector from base to rover and apply it to the base station position. Observation times at each station is only a few seconds. Maintenance of the radio link is the limiting factor with RTK surveys generally limiting them to smaller grids.	$\pm 5\text{cm}$	$\pm .01$ mgals
On The Fly Ambiguity resolution (OTF)	Tracks satellites continuously and stores information for post processing. Observation time at each station is only a few seconds. Able to recover from interruption of the satellite signals with no loss of accuracy through advanced ambiguity resolution algorithms which eliminate the need for a static initialisation or antenna swap.	$\pm 5\text{cm}$	$\pm .01$ mgals

All methods require a base GPS receiver to be located at a station with known elevation and horizontal coordinates. This base receiver allows post processing of the data to remove ionospheric effects and accurately calculate the vector from the base to the rover receiver using carrier phase processing. The most appropriate method is generally a compromise between cost and accuracy, though the accuracy should be kept in-line with other sources of gravity noise (eg geological noise, terrain correction errors, meter reading resolution)

Fugro Ground Geophysics surveyed all gravity stations with GPS utilising Ashtech Z-12 geodetic receivers. Data processing was performed using PNAV, Ashtech's On The Fly (OTF) ambiguity resolution software.

2.5.1 Control Point Establishment

Because of the scattered locations of the survey grids, a central base (DUDU) was established, with a temporary base on each survey grid tied to the DUDU base. provided location and elevation for the GPS base stations. The location of DUDU is shown as a schematic in the appendices to this report together with a photograph of the base. The quality of the GPS data is partially dependent on a well selected location for the GPS base receiver. Some of the criteria used for selecting a base station site include:

- Restrict the maximum base receiver to mobile receiver distance (baseline) to 20 km
- Minimise daily access time for installation/de-installation
- Minimal obstruction to satellite signals (trees, hills, culture)
- Avoid areas with potential multi-path reflections (metal culture, saline water etc).

The base station DUDU was positioned using Auslig's AUSPOS long baseline processing service. While a number of benchmarks and trig stations were shown in the area, none were able to be located. Refer to the appendices for a picture of the DUDU base and a location schematic.

2.5.2 On The Fly (OTF) GPS

The OTF kinematic method of processing data is done using Ashtech's proprietary PNAVTM baseline processing algorithm. PNAV is a Kalman-filter based real-time baseline processing engine which processes the time-tag matched double difference pseudo range and carrier phase measurements to generate optimal position and velocity solutions. Its ambiguity search algorithm fixes the carrier phase integer cycle ambiguities on-the-fly and enables PNAV to generate centimetre level epoch by epoch solutions. One of its major advantages over the other kinematic techniques is the elimination of initialisation requirements. This means that if the receiver loses lock completely because of trees, the crew does not have to stop and reinitialise the receiver. The PNAV software automatically recomputes the integer ambiguities even while the roving receiver is moving.

Repeats fell into a similar situation to the gravity repeats due to the programme layout. A total of 5 elevation repeats were observed with the largest error being 5cm.

2.5.3 GPS Window

The GPS window was good during the period of the survey, although some periods in the middle of the day had only 6-7 satellites available at an elevation mask of 10 degrees, as can be seen on the Geometric Dilution Of Precision (GDOP) graph below. This was only a problem on grids with substantial tree cover where some stations required a longer observation time after breaks in satellite lock. Figures 13 and 14 graph the Geometric Dilution Of Precision (GDOP) and number of satellites in view typical for a day in July 2002

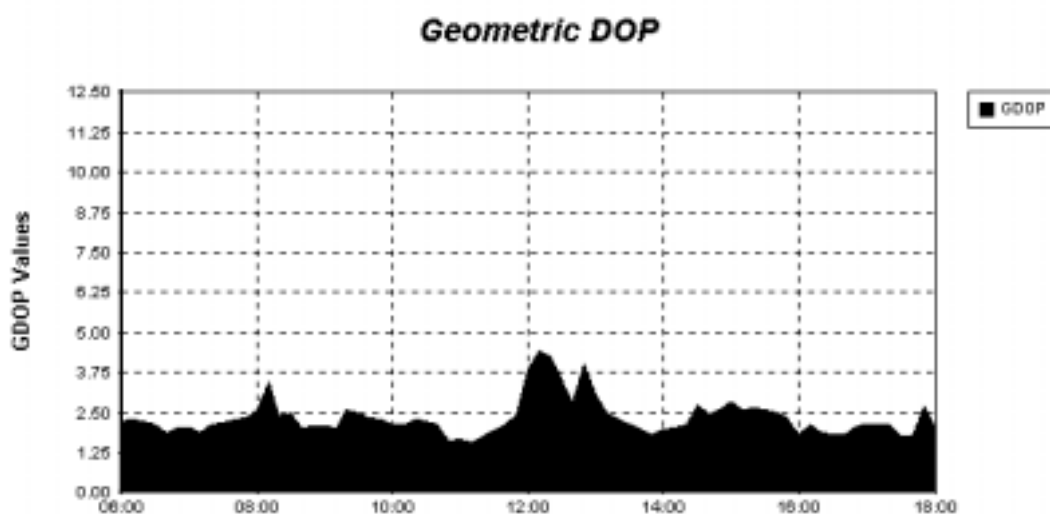


Figure 5. GDOP at a mask angle of 10° (July 2002)

GDOP is a measure of the quality of the solution based on satellite geometry and is the single most important factor effecting data quality. An absolute minimum of four satellites are required to solve for the receiver's position in 3-D space (ie. there are four unknowns to solve: X,Y,Z and receiver synchro-timing errors). GDOP can be considered as being inversely proportional to the volume of the hexahedron formed between the receiver and the four satellites (ie small volume \Rightarrow high GDOP \Rightarrow poor solution). GDOP is good when it is less than 3, acceptable when it lies between 3 and 5 and unacceptable if it exceeds 5.

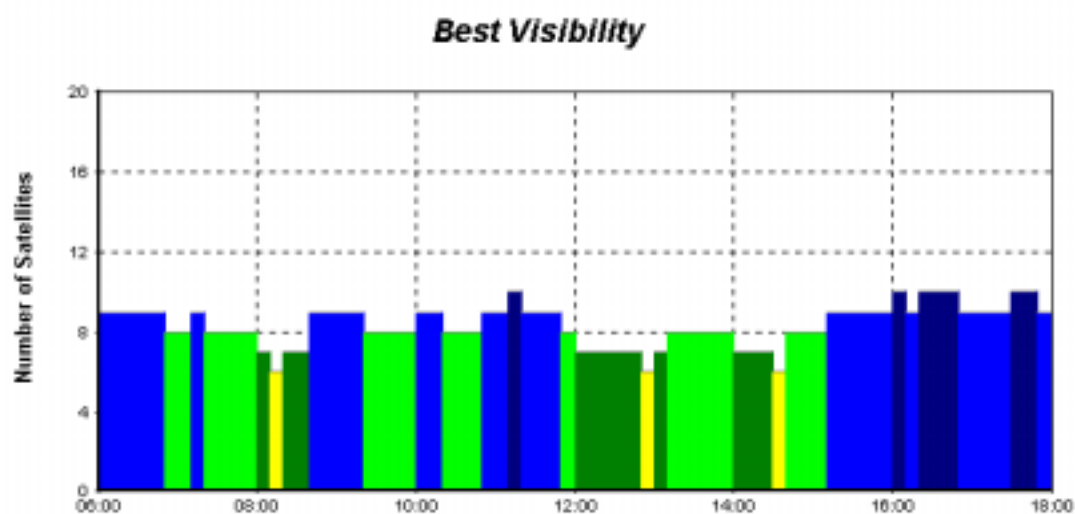


Figure 6. Satellites in view above 10° for survey area during July 2002

3. DATA PROCESSING

3.1 OBSERVED GRAVITY

The following corrections are applied to the raw gravity data to obtain observed gravity (g_o):

Instrument correction: to correct for the scaling factor between machine units and milligals, as listed in the manufacturer's calibration tables (see Appendix A).

Tidal correction: To correct for the differential gravitational effects of the moon and sun. Longman's polynomial approximation of tidal effect is applied to the base-out, base-in readings before the loop drift rate is calculated and is also applied to each station within the loop. The Longman's formulae are published in the Journal of Geophysical Research, Vol 64, No 12.

Mechanic drift: removed with the assumption that the drift between base-out and base-in is linear. This is a valid assumption when the non-linear components (tidal) have been removed before the drift rate is calculated and the meter has not suffered significant tares during the course of the loop.

The following equation summarises these corrections to obtain observed gravity:

$$g_o = g_{\text{stn}} + C_{\text{tide}} - C_{\text{drift}} - g_{\text{base-out}} + g_{0(\text{base})}$$

where:

g_o	observed gravity in milligals
g_{stn}	raw gravity reading at each station
C_{tide}	tidal effect (in milligals)
$g_{0(\text{base})}$	absolute value of gravity at the base
$C_{\text{drift}} = (g_{\text{base-out}} - g_{\text{base-in}}) / (t_{\text{base-out}} - t_{\text{base-in}}) \times t_{\text{stn}}$	
$g_{\text{base-out}}, g_{\text{base-in}}$	are base readings at start and end of loops
$t_{\text{base-out}}, t_{\text{base-in}}$	are base times at start and end of loops

3.2 BOUGUER GRAVITY

Bouguer gravity is calculated using equation:

$$G_b = G_o - G_t + C_{fa} - C_b + C_t$$

where

G_o = observed gravity described above

G_t = theoretical gravity calculated from the station's latitude.

C_{fa} = free air correction

$C_b = 2\pi G \rho h$ bouguer correction, G =universal gravity constant, ρ =density

C_t = terrain correction

Latitude Correction - To correct observed gravity for the effects of the differential centrifugal acceleration due to the reduction in angular velocity at the surface of the earth with latitude (this acceleration is at its maximum at the equator where the observed gravity will be at its minimum). This correction is solely a function of latitude (ϕ) obtained from survey co-ordinates.

For this survey the 1967 gravity formula is used to calculate the theoretical gravity g_t .

$$g_t = -978031.80 \times (1 + 0.0053024 \times \sin^2(\phi) - 0.0000059 \times \sin^2(2\phi))$$

Free Air Correction - To correct for the fact that gravity decreases (as the square of the distance) from the elevation datum. This correction is a function of station elevation above the datum and is approximately 0.3085958 mgals/metre.

Bouguer Correction - Corrects for the gravitational attraction of the rock between the station and elevation datum. This correction is dependent on elevation and the rock density and is approximately $2\pi G \rho h = 0.041896325\rho$ mgal/meter. For this survey, densities of 2.2, 2.4 and 2.67 gms/cc were used for the Bouguer corrections.

Terrain Correction - Corrects for the effects of surrounding topographic features which deviates from the infinite slab that is implicit in the bouguer correction. Quite small hills close to the reading site can have significant effects on gravity. Major features can have effects in excess of 20 km from the reading site. No terrain corrections were required for the grids covered during this survey.

3.3 GPS

3.3.1 Static Differential GPS

The temporary GPS bases established at each grid within the survey area were processed using Ashtech's 'Prism' software for the static ties.

3.3.2 On The Fly (OTF) GPS

Ashtech "PNAV" software was used in processing all GPS loops acquired on this survey. PNAV uses a recursive Kalman filter parameter estimation technique that resolves ambiguities while the roving receiver is in motion. PNAV initially uses the linear combination of the L1 and L2 frequencies (called widelane), which gives an 86cm carrier wave. The widelane carrier wave, being 86cm long is easier to solve ambiguities for than the L1 or L2 (<19cm) carrier waves individually. Once the widelane ambiguity is solved, L1 and L2 ambiguities are easily computed. The OTF method gives results comparable to normal kinematic methods, while eliminating the need to carry out static initialisation's or antenna swaps after breaks in the satellite data.

3.4 SPHEROID TRANSFORMATION

GPS uses the World Geodetic System 1984 (WGS84) spheroid for both its broadcast and precise ephemerides. The WGS84 (World Geodetic System) is a geocentric reference system which attempts a best fit of the whole earth using the latest information. The Australian National Spheroid (ANS) is a non geocentric local spheroid and is the basis for the Australian co-ordinate set (AGD66 & 84) and its UTM projection. An accurate 7 parameter shift is available to convert between WGS84 and AGD84, however because coordinates were required in the older AGD66 values, a block shift (supplied by AUSLIG) must then be applied to the AGD84 values. This shift was 4.48m East and - 3.3m North from AGD84 values. It should be noted that conversion to AGD66 can generate an error in position of up to 3m, as the AUSLIG values are simply a mean value for each 1:250,000 map sheet. This is a result of the non homogenous nature of the AGD66 projection.

All GPS data are processed on the WGS84 datum, and must then be converted to AGD, to reflect the shift between the datum origins. Fugro Ground Geophysics used the following datum transformation values.

Defining parameters for the ANS Spheroid:

Semi-Major Axis (a)	6378160m	Inverse Flattening ($1/f$)	298.25
<i>Transformation Parameters From WGS84 to AGD84</i>		(From Higgins, 1987)	
Shifts		Rotations (seconds)	
Tx	116m	Rx	0.23
Ty	50.47m	Ry	0.39
Tz	-141.69m	Rz	0.344
Scale change K	0 ppm		

The data is also presented as UTM co-ordinates (Zone 52) using Redfearn's (1948) formulae to convert geographic co-ordinates to easting and northing values.

3.5 SPHEROID-GEOID SEPARATION

The Australian Height Datum (AHD) is a national vertical datum based on mean sea level measured at 30 locations around the Australian coastline. The geoid is an equipotential surface which best approximates mean sea level over the whole earth. AHD, true local mean sea level and geoid surfaces invariably do not coincide and certainly differ from the WGS84 and AGD84 spheroid surfaces.

Fugro Ground Geophysics processes all heights to the WGS84 spheroid which differs by up to 50 meters from the AHD height. This height difference is referred to as spheroid separation or n-value. The calculation of the height difference between the WGS84 spheroid and the non-uniform Australian Height Datum depends on the GPS method, area and accuracy. The possible methods include:

- 1 Global Geo-potential Model (eg OSU91) which utilises a satellite orbit perturbation, terrestrial gravity and satellite altimetry to produce a high degree expansion model of the geoid. This method provides absolute accuracies of 2 metres and relative errors at the decimetre level. Given that relative errors of over 20ppm (20mm/km) can occur when exclusively using a geo-potential model this method should only be applied in areas where there no better geoid model.
- 2 In Australia, AUSLIG (Australian Surveying & Land Information Group - Dept. of Administrative Services) maintains a data base of n values over a regular 2 minute grid calculated from a combination of the Global model (EGM96) and Geoscience Australia's gravity database. This method can provide relative accuracy of 2-3 parts per million. Fugro Ground Geophysics uses a bi-cubic interpolation routine provided by AUSLIG to calculate n-values for each control point from this regular grid of calculated values. The interpolation errors are less than 10 cm when compared with rigorously calculated n values.
- 3 For surveys requiring high accuracy in areas with good gravity coverage, the n-values may be rigorously calculated using a combination of Global model EGM96 and GA gravity data for each station. This method will therefore have no interpolation errors.

For this survey method 2 has been applied to the WGS84 co-ordinates to give AHD heights.

3.6 OFFICE REPROCESSING

As a standard procedure, all data is routinely checked throughout the survey, and undergoes a final checking process via a complete reprocessing sequence subsequent to the completion of the survey.

The following data integrity checks were made:

- All data entry of raw gravity are checked against field books
- WGS84 to AGD66 to AMG conversions checked
- Spheroid to geoid separation checked for both control and each gravity station
- GPS and Gravity Base station ties are checked and reprocessed
- Re-process OTF data where necessary

The final data accompanying this report has been shifted to reflect the accurate position of the DUDU base station which was computed after completion of the survey.

4. ERROR ANALYSIS

The total probable error in the final Bouguer Gravity data, e_{bg} , is calculated using: (from Appendix D)

$$e_{bg}^2 = e_g^2 + e_{gt}^2 + (c \cdot e_h)^2$$

where

e_g is the error in the observed gravity

e_{gt} is the error in the theoretical gravity value used

e_h is the error in the elevation value

$$c = (0.3086 - 2\pi\rho G)$$

where $G = 6.67 \times 10^{-8}$ (dyne cm²)/g Universal Gravity Constant

$$\rho = 2.67 \text{ g/cc}$$

$$c = 0.1967 \text{ mgal/metre}$$

From preceding sections

$$e_g = 0.019 \times 0.707 = 0.013 \text{ mgals}$$

$$e_h = 0.05 \times 0.707 = 0.035 \text{ metres}$$

$$\begin{aligned} e_{gt} &= 0.00081 \sin(2 \times \text{latitude}) \text{ mgals/metre} \times \text{northing error} \\ &= 0.0001 \text{ mgal} \end{aligned}$$

It follows that the probable Bouguer error for the survey

$$e_{bg}^2 = 0.013^2 + 0.0001^2 + (0.035 \times 0.1967)^2$$

$$e_{bg} = 0.014 \text{ mgals}$$

5. DATA PRODUCTS

5.1 FIELD DATA PRODUCTS

The following data presentation products were presented to BHP Billiton.

- Field data via email.

5.2 FINAL DATA PRODUCTS

The following data presentation products were presented to BHP Billiton.

- Logistics Report
- Final data on CD-ROM.

5.2.1 FINAL DATA FORMAT

The final data is supplied to BHP in a standard Geosoft ASCII format including a header line detailing column assignments. This disk is located at the rear of the report.

APPENDIX A

GRAVITY METER CALIBRATION TABLE

MILLIGAL VALUES FOR LACOSTE & ROMBERG
MODEL G GRAVITY METER # G-617

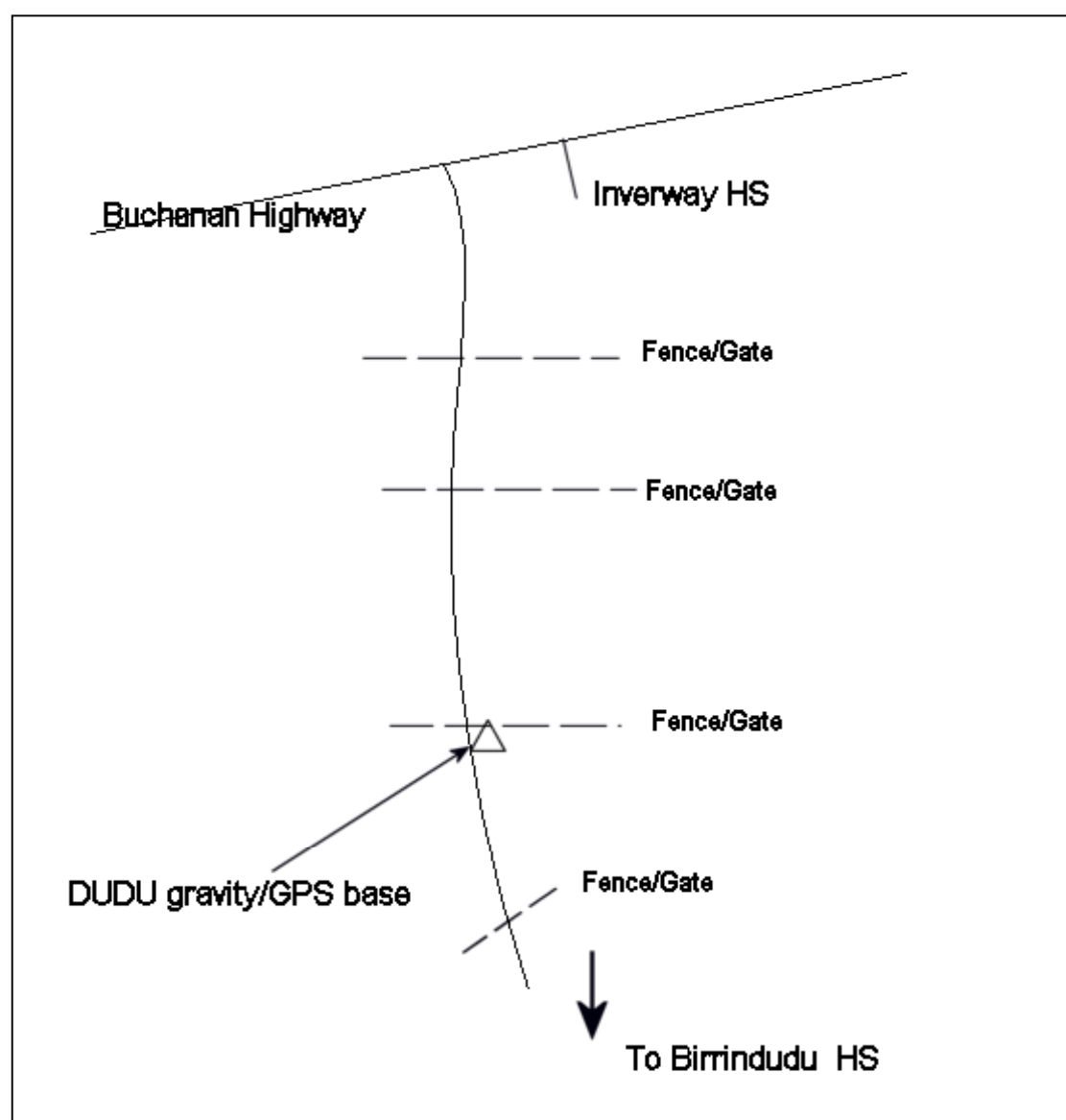
COUNTER READING	VALUE IN MILLIGALS	FACTOR FOR INTERVAL
2000	2032.28	1.01678
2100	2133.95	1.01686
2200	2235.64	1.01696
2300	2337.34	1.01706
2400	2439.04	1.01717
2500	2540.76	1.01729

APPENDIX B

GPS CONTROL DESCRIPTIONS



DUDU	GDA94
Latitude (ϕ)	18°09'10".1701 S
Longitude (λ)	129°30'49".3905 E
MGA East (Zone 52)	554,337.252
MGA North (Zone 52)	7,992,830.462
Spheroidal Height	433.529
Geoid Separation (n)	30.881
AHD Elevation (Auspos Derived)	402.648
Observed Gravity (Isogal84 milligals)	978438.43



APPENDIX C

GRAVITY LOOP STATISTICS

GRAVITY LOOP STATISTICS

Loop	Date	Stations	Drift	G #	G Fact	Base Out	Base In
101	20020707	54	-0.08	617	1.01678	DUDU	DUDU
102	20020708	54	-0.05	617	1.01678	DUDU	DUDU
103	20020711	64	-0.1	617	1.01678	DUDU	DUDU
104	20020716	52	0.01	617	1.01678	DUDU	DUDU
105	20020717	53	-0.05	617	1.01678	DUDU	DUDU
106	20020719	63	-0.1	617	1.01678	DUDU	DUDU
107	20020720	64	0.06	617	1.01678	DUDU	DUDU
108	20020721	53	0.01	617	1.01678	DUDU	DUDU

APPENDIX D

STATISTICAL ANALYSIS AND ERROR CALCULATION

STATISTICAL ANALYSIS AND ERROR CALCULATION

Assuming all of the factors contributing to the final Bouguer gravity are mutually independent, then the expected error in the final Bouguer gravity is the square root of the sum of the squares of the error in each factor, ie

$$E_{BG} = E_{OBS} + E_{gv} + (C \times E_h) + E_{gT}$$

This assumption is not absolutely valid, since a small amount of cross-correlation does exist (for instance, an error in the vertical will affect the terrain correction if measured elevations rather than grid elevations are used to calculate the terrain correction). These cross-correlations will, however, be generally small, so the above error calculation will yield results that are very close to the true values.

In order to quantitatively measure the so-called expected error, it is necessary to define the confidence limit. This gives some meaning to the term expected error (or, put more positively, expected accuracy) by making the following statement possible:

X percent of the measured values will be accurate to within $\pm Y$

For our purposes, we have defined the confidence limit to be 1 sigma, or roughly 67%, hence, we are after the error range (ie ± 0.3 mgal) that will allow us to confidently state that 67% of the data satisfies this criterion. We could have chosen a 2 sigma limit, in which our expected error would have been larger, since our confidence limit would be about 95%. Similarly, we could have gone for a 50% confidence limit, which would have resulted in a smaller expected error. By choosing the 1 sigma limit, we are conforming to a fairly widely accepted industry standard.

The solution of the error equation for the final Bouguer gravity reduces to collecting enough data to determine the 1 sigma confidence limit of each of the factors in the equation. This is done by repeating enough samples to derive a statistically significant error limit. For simplicity, we will look at the probable error in observed gravity. The calculation of the probable errors in the other factors is analogous.

To derive the probable error in the observed gravity, stations are revisited and the gravity reading is taken again. Each reading at a station is compared with the mean of all readings taken at that station. For example, a station with three readings would yield three deviations from the mean value. It is believed that this method yields a much better statistical analysis of the data. Once all the deviations for a survey have been calculated, they are plotted on a histogram. The repeat differences will fit a normal distribution curve with a mean (zero in theory, very close to zero in practice) and a standard deviation (sigma). Statistically, 67% of the repeat differences will fall within ± 1 sigma of the mean.

According to our definition:

$$E_{RPT\ DIFF} = \pm \text{sigma}$$

In other words, the expected repeatability of an observed gravity reading is \pm sigma.

It is very important to realise that expected repeatability is not the expected accuracy of an individual reading. The expected repeatability and expected accuracy of the individual reading are only the same if the repeat reading has an expected error of zero. This follows logically from our definition of expected error, as the square root of the sum of the squares of the expected error of each independent factor (see the formula for expected error of final Bouguer gravity). There may be

other small cross-correlations (ie the observer may look up the previous reading to speed up the repeat reading), but, for our purposes, we assume they are totally independent.

Thus

$$E_{\text{RPT.DIFF}}^2 = E_{\text{RPT RDG}}^2 + E_{\text{FIRST RDG}}^2$$

But we assume:

$$E_{\text{RPT RDG}} = E_{\text{FIRST RDG}}$$

(This assumption is a good one: you expect to be able to read a gravimeter on the same spot with the same precision at different times).

Therefore:

$$E_{\text{RPT RDG}}^2 = 2 \times E_{\text{FIRST RDG}}^2$$

or

$$E_{\text{FIRST RDG}} = 0.707 \times \text{Sigma}$$

The expected error of an individual observed gravity value is equal to 0.707 times the expected repeatability.

The above calculation for observed gravity is carried through for each factor in the final Bouguer value and the end result is a 67% confidence limit of final Bouguer gravity which we have defined as expected accuracy.

APPENDIX E
PRODUCTION REPORTS

PRODUCTION REPORT FOR G2052

DATE	COMMENTS	PROD
2/7/02	mobilisation	
3/7/02	Collect equipment and mobilise to field. Vehicle accident 27km from town (BHPB personnel driving). To Kununurra in evening to collect replacement	mobilisation
4/7/02	Mobilised to camp arriving 1730hrs	standby
5/7/02	Setup camp. Acquisition in afternoon on ANT029	stby/prod
6/7/02	Magnetics ANT029 and ANT030	production
7/7/02	Magnetics and Gravity ANT030	production
8/7/02	Gravity ANT029, Magnetics ANT031	production
9/7/02	Magnetics ANT031, ANT033	production
10/7/02	Gravity tie to Halls Creek, purchase fuel, tyres, supplies	standby
11/7/02	Gravity ANT033	production
12/7/02	Magnetics ANT028, scout access ANT007	production
13/7/02	Magnetics ANT007	production
14/7/02	Magnetics ANT027 - very poor access	production
15/7/02	Magnetics ANT002 - poor access	production
16/7/02	Gravity ANT027 - very poor access	production
17/7/02	Gravity ANT002 - poor access	production
18/7/02	Magnetics ANT012	production
19/7/02	Gravity and Magnetics ANT011	production
20/7/02	Gravity and Magnetics ANT012	production
21/7/02	Gravity ANT028	production
22/7/02	Gravity Base tie to Halls Creek. Completion of BHPB programme	.5 Standby

APPENDIX F
DATA LISTING

APPENDICES

Line 111
 \Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD 08-01-2002
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\Line	Station	North metres	East metres	Latitude dec deg	Longitude dec deg	Elev metres	Ter Cor mgals	G obs. mgals	Free Air mgals	Bouguer 2.20g/cc	Gravity (mgals) 2.40g/cc	2.67g/cc
111	1	7943103	525198	-18.60275	129.23885	379.58	0.0000	978462.92	22.63	-12.36	-15.54	-19.84
111	2	7943061	525194	-18.60312	129.23881	379.79	0.0000	978462.82	22.58	-12.43	-15.61	-19.91
111	3	7943023	525194	-18.60347	129.23881	379.95	0.0000	978462.73	22.51	-12.51	-15.69	-19.99
111	4	7942980	525197	-18.60386	129.23884	380.07	0.0000	978462.74	22.54	-12.49	-15.68	-19.98
111	5	7942939	525204	-18.60423	129.23891	380.21	0.0000	978462.64	22.46	-12.58	-15.77	-20.07
111	6	7942900	525205	-18.60458	129.23892	380.43	0.0000	978462.57	22.44	-12.63	-15.82	-20.12
111	7	7942859	525199	-18.60496	129.23886	380.86	0.0000	978462.46	22.45	-12.66	-15.85	-20.16
111	8	7942818	525199	-18.60532	129.23886	381.17	0.0000	978462.38	22.44	-12.69	-15.89	-20.20
111	9	7942779	525199	-18.60568	129.23886	381.46	0.0000	978462.30	22.43	-12.73	-15.93	-20.24
111	10	7942739	525202	-18.60604	129.23889	381.84	0.0000	978462.10	22.32	-12.87	-16.07	-20.39
111	11	7942700	525201	-18.60639	129.23888	382.29	0.0000	978461.99	22.34	-12.90	-16.10	-20.43
111	12	7942658	525192	-18.60677	129.23880	382.74	0.0000	978461.79	22.25	-13.03	-16.23	-20.56
111	13	7942620	525199	-18.60711	129.23886	383.27	0.0000	978461.67	22.27	-13.05	-16.26	-20.60
111	14	7942578	525200	-18.60749	129.23888	383.88	0.0000	978461.54	22.32	-13.06	-16.28	-20.62
111	15	7942539	525202	-18.60784	129.23889	384.64	0.0000	978461.34	22.33	-13.12	-16.35	-20.70
111	16	7942501	525204	-18.60818	129.23892	385.61	0.0000	978461.06	22.34	-13.21	-16.44	-20.80
111	17	7942456	525201	-18.60859	129.23889	387.04	0.0000	978460.72	22.41	-13.27	-16.51	-20.89
111	18	7942416	525201	-18.60895	129.23888	388.10	0.0000	978460.37	22.37	-13.40	-16.65	-21.04
111	19	7942375	525200	-18.60933	129.23887	388.95	0.0000	978460.14	22.38	-13.47	-16.73	-21.13
111	20	7942333	525201	-18.60970	129.23889	389.25	0.0000	978459.98	22.30	-13.58	-16.84	-21.25
111	21	7942298	525203	-18.61003	129.23891	389.70	0.0000	978459.79	22.22	-13.70	-16.96	-21.37
111	22	7942257	525202	-18.61040	129.23890	389.98	0.0000	978459.71	22.21	-13.74	-17.01	-21.42
111	23	7942218	525201	-18.61074	129.23889	390.22	0.0000	978459.68	22.23	-13.74	-17.01	-21.42
111	24	7942178	525201	-18.61111	129.23889	390.44	0.0000	978459.68	22.28	-13.71	-17.08	-21.40
111	25	7942137	525202	-18.61148	129.23890	390.56	0.0000	978459.65	22.26	-13.73	-17.01	-21.42
111	26	7942097	525203	-18.61184	129.23891	390.63	0.0000	978459.61	22.24	-13.77	-17.04	-21.46
111	27	7942057	525202	-18.61220	129.23890	390.73	0.0000	978459.69	22.32	-13.70	-16.97	-21.39
111	28	7942018	525202	-18.61255	129.23890	390.88	0.0000	978459.78	22.44	-13.59	-16.87	-21.29
111	29	7941978	525199	-18.61292	129.23887	390.98	0.0000	978459.88	22.55	-13.49	-16.77	-21.19
111	30	7941937	525201	-18.61328	129.23889	391.14	0.0000	978459.89	22.59	-13.46	-16.74	-21.17
111	31	7941899	525211	-18.61362	129.23899	391.24	0.0000	978459.94	22.65	-13.41	-16.69	-21.12

Line 112
 \Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD 08-01-2002
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\Line	Station	North metres	East metres	Latitude dec deg	Longitude dec deg	Elev metres	Ter Cor mgals	G obs. mgals	Free Air mgals	Bouguer 2.20g/cc	Gravity (mgals) 2.40g/cc	2.67g/cc
112	1	7942499	524598	-18.60822	129.23317	385.83	0.0000	978461.02	22.35	-13.21	-16.44	-20.81
112	2	7942501	524639	-18.60819	129.23356	385.74	0.0000	978461.09	22.40	-13.15	-16.39	-20.75
112	3	7942500	524679	-18.60820	129.23394	385.57	0.0000	978461.12	22.38	-13.16	-16.39	-20.75
112	4	7942502	524719	-18.60819	129.23432	385.36	0.0000	978461.17	22.36	-13.15	-16.38	-20.74
112	5	7942500	524758	-18.60820	129.23468	385.27	0.0000	978461.18	22.35	-13.16	-16.39	-20.75
112	6	7942502	524799	-18.60818	129.23508	385.18	0.0000	978461.21	22.35	-13.15	-16.38	-20.74
112	7	7942499	524837	-18.60821	129.23544	385.15	0.0000	978461.29	22.42	-13.08	-16.31	-20.66
112	8	7942497	524879	-18.60823	129.23583	385.14	0.0000	978461.24	22.37	-13.13	-16.36	-20.72
112	9	7942497	524919	-18.60823	129.23621	385.08	0.0000	978461.28	22.39	-13.10	-16.33	-20.69
112	10	7942500	524958	-18.60820	129.23658	385.01	0.0000	978461.26	22.35	-13.14	-16.36	-20.72
112	11	7942501	524997	-18.60819	129.23695	385.01	0.0000	978461.28	22.36	-13.13	-16.35	-20.71
112	12	7942499	525036	-18.60821	129.23732	384.97	0.0000	978461.30	22.37	-13.12	-16.34	-20.70
112	13	7942499	525076	-18.60821	129.23770	384.98	0.0000	978461.25	22.32	-13.16	-16.39	-20.74
112	14	7942503	525116	-18.60817	129.23808	385.10	0.0000	978461.20	22.31	-13.19	-16.41	-20.77
112	15	7942499	525158	-18.60821	129.23847	385.50	0.0000	978461.08	22.32	-13.21	-16.44	-20.80
112	16	7942501	525204	-18.60818	129.23892	385.61	0.0000	978461.03	22.30	-13.24	-16.47	-20.83
112	17	7942498	525240	-18.60822	129.23925	385.87	0.0000	978461.00	22.35	-13.22	-16.45	-20.82
112	18	7942496	525282	-18.60823	129.23965	386.03	0.0000	978461.07	22.47	-13.11	-16.35	-20.72
112	19	7942502	525320	-18.60817	129.24001	385.80	0.0000	978461.18	22.51	-13.05	-16.28	-20.65
112	20	7942503	525360	-18.60817	129.24039	385.73	0.0000	978461.27	22.58	-12.97	-16.21	-20.57
112	21	7942503	525399	-18.60817	129.24076	385.48	0.0000	978461.38	22.61	-12.92	-16.15	-20.51
112	22	7942503	525442	-18.60817	129.24117	385.18	0.0000	978461.37	22.51	-12.99	-16.22	-20.58
112	23	7942503	525481	-18.60817	129.24154	384.82	0.0000	978461.51	22.53	-12.94	-16.16	-20.51
112	24	7942508	525523	-18.60812	129.24193	384.42	0.0000	978461.64	22.54	-12.89	-16.11	-20.46
112	25	7942505	525560	-18.60815	129.24229	384.18	0.0000	978461.86	22.69	-12.72	-15.94	-20.28
112	26	7942506	525601	-18.60814	129.24268	383.93	0.0000	978461.98	22.74	-12.65	-15.87	-20.21
112	27	7942497	525641	-18.60822	129.24305	383.79	0.0000	978462.04	22.75	-12.62	-15.84	-20.18
112	28	7942502	525681	-18.60817	129.24344	383.40	0.0000	978462.15	22.74	-12.60	-15.82	-20.15
112	29	7942506	525721	-18.60813	129.24382	383.06	0.0000	978462.16	22.64	-12.66	-15.87	-20.21
112	30	7942504	525760	-18.60815	129.24418	382.86	0.0000	978462.31	22.73	-12.56	-15.76	-20.09
112	31	7942504	525801	-18.60815	129.24457	382.60	0.0000	978462.36	22.70	-12.56	-15.77	-20.09

Line 121
 \Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD 08-01-2002
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\Line	Station	North metres	East metres	Latitude dec deg	Longitude dec deg	Elev metres	Ter Cor mgals	G obs. mgals	Free Air mgals	Bouguer 2.20g/cc	Gravity (mgals) 2.40g/cc	2.67g/cc
121	1	7942848	528601	-18.60501	129.27111	370.90	0.0000	978466.39	23.30	-10.89	-14.00	-18.19
121	2	7942809	528601	-18.60536	129.27111	371.02	0.0000	978466.25	23.17	-11.02	-14.13	-18.33
121	3	7942769	528596	-18.60572	129.27106	371.12	0.0000	978466.18	23.11	-11.09	-14.20	-18.40
121	4	7942727	528596	-18.60610	129.27106	371.27	0.0000	978466.11	23.07	-11.16	-14.27	-18.47
121	5	7942687	528600	-18.60646	129.27110	371.36	0.0000	978466.01	22.98	-11.25	-14.36	-18.56
121	6	7942647	528606	-18.60683	129.27116	371.48	0.0000	978465.89	22.87	-11.37	-14.48	-18.68
121	7	7942606	528601	-18.60719	129.27112	371.59	0.0000	978465.78	22.78	-11.47	-14.59	-18.79
121	8	7942567	528596	-18.60755	129.27106	371.71	0.0000	978465.71	22.73	-11.53	-14.65	-18.85
121	9	7942528	528595	-18.60790	129.27106	371.82	0.0000	978465.63	22.66	-11.61	-14.72	-18.93
121	10	7942487	528599	-18.60827	129.27109	371.96	0.0000	978465.60	22.65	-11.63	-14.75	-18.95
121	11	7942448	528606	-18.60863	129.27116	372.08	0.0000	978465.53	22.60	-11.70	-14.81	-19.02
121	12	7942406	528591	-18.60900	129.27102	372.24	0.0000	978465.45	22.56	-11.75	-14.87	-19.08

APPENDICES

121	13	7942366	528601	-18.60937	129.27111	372.38	0.0000	978465.41	22.54	-11.79	-14.91	-19.12
121	14	7942325	528610	-18.60973	129.27120	372.53	0.0000	978465.37	22.52	-11.82	-14.94	-19.15
121	15	7942282	528605	-18.61012	129.27116	372.69	0.0000	978465.34	22.52	-11.84	-14.96	-19.17
121	16	7942247	528605	-18.61044	129.27115	372.82	0.0000	978465.31	22.51	-11.86	-14.98	-19.20
121	17	7942205	528609	-18.61082	129.27120	373.00	0.0000	978465.31	22.55	-11.83	-14.96	-19.17
121	18	7942167	528597	-18.61116	129.27108	373.09	0.0000	978465.30	22.55	-11.84	-14.97	-19.19
121	19	7942125	528593	-18.61154	129.27104	373.26	0.0000	978465.25	22.53	-11.88	-15.01	-19.23
121	20	7942087	528605	-18.61189	129.27116	373.40	0.0000	978465.22	22.52	-11.90	-15.03	-19.25
121	21	7942047	528602	-18.61225	129.27113	373.55	0.0000	978465.22	22.54	-11.89	-15.02	-19.24
121	22	7942005	528600	-18.61263	129.27111	373.40	0.0000	978465.22	22.49	-11.93	-15.06	-19.28
121	23	7941966	528602	-18.61298	129.27113	373.57	0.0000	978465.21	22.51	-11.93	-15.06	-19.28
121	24	7941924	528602	-18.61335	129.27113	373.78	0.0000	978465.20	22.54	-11.91	-15.05	-19.27
121	25	7941886	528598	-18.61370	129.27109	374.17	0.0000	978465.18	22.62	-11.87	-15.00	-19.24
121	26	7941845	528605	-18.61407	129.27116	374.27	0.0000	978465.16	22.61	-11.89	-15.03	-19.26
121	27	7941805	528606	-18.61443	129.27117	374.39	0.0000	978465.13	22.60	-11.91	-15.04	-19.28
121	28	7941767	528597	-18.61478	129.27109	374.47	0.0000	978465.10	22.58	-11.94	-15.08	-19.31
121	29	7941726	528603	-18.61515	129.27114	374.58	0.0000	978465.05	22.54	-11.99	-15.13	-19.36
121	30	7941686	528608	-18.61551	129.27119	374.75	0.0000	978465.02	22.54	-12.00	-15.14	-19.38
121	31	7941646	528597	-18.61587	129.27109	374.91	0.0000	978465.04	22.59	-11.97	-15.11	-19.35
Line 122												
\Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD 08-01-2002												
\=====												
\	Line	Station	North	East	Latitude	Longitude	Elev	Ter Cor	G obs.	Free Air	Bouguer	Gravity (mgals)
\			metres	metres	dec deg	dec deg	metres	mgals	mgals	mgals	2.20g/cc	2.40g/cc 2.67g/cc
\=====												
122	1	7942254	529207	-18.61037	129.27686	373.16	0.0000	978466.01	23.32	-11.07	-14.20	-18.42
122	2	7942242	529157	-18.61047	129.27639	373.09	0.0000	978465.85	23.14	-11.25	-14.38	-18.60
122	3	7942246	529117	-18.61044	129.27600	372.99	0.0000	978465.83	23.09	-11.29	-14.42	-18.64
122	4	7942252	529080	-18.61039	129.27566	372.89	0.0000	978465.77	23.00	-11.37	-14.50	-18.72
122	5	7942245	529040	-18.61045	129.27528	372.88	0.0000	978465.75	22.97	-11.40	-14.53	-18.74
122	6	7942248	529000	-18.61043	129.27490	372.85	0.0000	978465.77	22.98	-11.39	-14.51	-18.73
122	7	7942246	528959	-18.61045	129.27451	372.78	0.0000	978465.71	22.90	-11.46	-14.58	-18.80
122	8	7942246	528919	-18.61045	129.27413	372.78	0.0000	978465.66	22.85	-11.51	-14.63	-18.85
122	9	7942241	528880	-18.61049	129.27376	372.76	0.0000	978465.58	22.76	-11.60	-14.72	-18.94
122	10	7942241	528839	-18.61050	129.27337	372.79	0.0000	978465.48	22.67	-11.69	-14.81	-19.03
122	11	7942249	528800	-18.61042	129.27301	372.76	0.0000	978465.45	22.64	-11.72	-14.85	-19.06
122	12	7942246	528759	-18.61045	129.27261	372.76	0.0000	978465.42	22.60	-11.76	-14.88	-19.10
122	13	7942247	528719	-18.61043	129.27224	372.79	0.0000	978465.40	22.59	-11.77	-14.89	-19.11
122	14	7942248	528679	-18.61042	129.27186	372.80	0.0000	978465.35	22.54	-11.82	-14.94	-19.16
122	15	7942250	528638	-18.61041	129.27147	372.81	0.0000	978465.34	22.54	-11.82	-14.94	-19.16
122	16	7942249	528604	-18.61042	129.27115	372.80	0.0000	978465.32	22.52	-11.84	-14.97	-19.18
122	17	7942246	528560	-18.61045	129.27073	372.81	0.0000	978465.21	22.41	-11.96	-15.08	-19.30
122	18	7942247	528518	-18.61044	129.27033	372.82	0.0000	978465.15	22.35	-12.02	-15.14	-19.36
122	19	7942251	528479	-18.61041	129.26997	372.77	0.0000	978465.17	22.36	-12.00	-15.12	-19.34
122	20	7942248	528441	-18.61043	129.26960	372.77	0.0000	978465.12	22.31	-12.05	-15.17	-19.39
122	21	7942248	528401	-18.61043	129.26922	372.76	0.0000	978465.14	22.32	-12.03	-15.16	-19.37
122	22	7942252	528361	-18.61040	129.26884	372.77	0.0000	978465.10	22.29	-12.07	-15.20	-19.41
122	23	7942250	528320	-18.61041	129.26846	372.75	0.0000	978465.10	22.28	-12.08	-15.20	-19.42
122	24	7942246	528280	-18.61045	129.26807	372.81	0.0000	978465.04	22.24	-12.12	-15.24	-19.46
122	25	7942252	528241	-18.61040	129.26771	372.82	0.0000	978465.08	22.29	-12.08	-15.20	-19.42
122	26	7942255	528201	-18.61037	129.26733	372.87	0.0000	978465.03	22.25	-12.12	-15.24	-19.46
122	27	7942255	528161	-18.61038	129.26695	372.94	0.0000	978465.10	22.34	-12.03	-15.16	-19.37
122	28	7942251	528121	-18.61041	129.26657	373.12	0.0000	978465.08	22.38	-12.02	-15.14	-19.36
122	29	7942248	528080	-18.61044	129.26618	373.20	0.0000	978465.06	22.38	-12.02	-15.15	-19.37
122	30	7942247	528040	-18.61044	129.26580	373.36	0.0000	978465.04	22.41	-12.01	-15.14	-19.36
122	31	7942254	528002	-18.61039	129.26544	373.49	0.0000	978464.98	22.39	-12.04	-15.17	-19.39
Line 21												
\Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD 08-01-2002												
\=====												
\	Line	Station	North	East	Latitude	Longitude	Elev	Ter Cor	G obs.	Free Air	Bouguer	Gravity (mgals)
\			metres	metres	dec deg	dec deg	metres	mgals	mgals	mgals	2.20g/cc	2.40g/cc 2.67g/cc
\=====												
21	1	7995499	585901	-18.12761	129.81200	437.70	0.0000	978430.93	34.20	-6.14	-9.81	-14.76
21	2	7995494	585941	-18.12766	129.81237	437.80	0.0000	978430.91	34.21	-6.15	-9.82	-14.77
21	3	7995505	585981	-18.12756	129.81275	437.98	0.0000	978430.83	34.18	-6.19	-9.86	-14.81
21	4	7995503	586019	-18.12758	129.81312	438.84	0.0000	978430.75	34.38	-6.07	-9.75	-14.71
21	5	7995499	586059	-18.12761	129.81349	438.23	0.0000	978430.82	34.26	-6.14	-9.81	-14.77
21	6	7995500	586099	-18.12760	129.81387	438.14	0.0000	978430.92	34.33	-6.05	-9.73	-14.68
21	7	7995498	586137	-18.12762	129.81423	437.93	0.0000	978430.99	34.33	-6.03	-9.70	-14.65
21	8	7995497	586179	-18.12763	129.81463	438.84	0.0000	978431.08	34.71	-5.74	-9.42	-14.38
21	9	7995503	586220	-18.12756	129.81502	438.55	0.0000	978431.16	34.69	-5.73	-9.41	-14.37
21	10	7995506	586259	-18.12754	129.81538	438.36	0.0000	978431.24	34.71	-5.69	-9.36	-14.32
21	11	7995504	586299	-18.12756	129.81576	437.10	0.0000	978431.34	34.42	-5.86	-9.53	-14.47
21	12	7995500	586338	-18.12759	129.81613	436.78	0.0000	978431.42	34.40	-5.85	-9.51	-14.46
21	13	7995499	586379	-18.12760	129.81652	436.17	0.0000	978431.57	34.37	-5.83	-9.49	-14.42
21	14	7995502	586419	-18.12757	129.81689	437.41	0.0000	978431.77	34.95	-5.36	-9.03	-13.98
21	15	7995504	586458	-18.12755	129.81727	435.59	0.0000	978431.94	34.57	-5.58	-9.23	-14.16
21	16	7995498	586499	-18.12760	129.81765	434.70	0.0000	978432.14	34.48	-5.58	-9.23	-14.14
21	17	7995497	586539	-18.12761	129.81803	433.61	0.0000	978432.37	34.38	-5.59	-9.22	-14.13
21	18	7995497	586581	-18.12761	129.81842	433.65	0.0000	978432.51	34.53	-5.44	-9.07	-13.98
21	19	7995498	586619	-18.12759	129.81879	433.28	0.0000	978432.73	34.63	-5.30	-8.93	-13.83
21	20	7995500	586659	-18.12757	129.81916	433.43	0.0000	978432.74	34.69	-5.26	-8.89	-13.79
21	21	7995516	586699	-18.12743	129.81955	433.16	0.0000	978432.73	34.60	-5.32	-8.95	-13.85
21	22	7995512	586740	-18.12747	129.81993	432.64	0.0000	978432.94	34.66	-5.22	-8.85	-13.74
21	23	7995501	586781	-18.12757	129.82032	431.79	0.0000	978433.34	34.79	-5.01	-8.63	-13.52
21	24	7995496	586818	-18.12760	129.82066	429.23	0.0000	978433.62	34.27	-5.29	-8.89	-13.74
21	25	7995497	586857	-18.12760	129.82104	428.84	0.0000	978433.88	34.42	-5.11	-8.70	-13.55
21	26	7995507	586899	-18.12750	129.82143	427.71</						

Line 22 Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD											08-01-2002		
Line	Station	North metres	East metres	Latitude dec deg	Longitude dec deg	Elev metres	Ter mgals	Cor mgals	G obs. mgals	Free Air mgals	Bouguer 2.20g/cc	Gravity (mgals) 2.40g/cc 2.67g/cc	
22	1	7996000	586401	-18.12307	129.81671	439.22	0.0000		978431.92	35.90	-4.58	-8.26 -13.23	
22	2	7995962	586399	-18.12341	129.81669	439.92	0.0000		978431.83	36.01	-4.54	-8.23 -13.20	
22	3	7995922	586398	-18.12377	129.81668	439.10	0.0000		978431.86	35.77	-4.70	-8.38 -13.35	
22	4	7995879	586397	-18.12416	129.81667	439.19	0.0000		978431.76	35.68	-4.81	-8.49 -13.45	
22	5	7995839	586397	-18.12453	129.81667	438.84	0.0000		978431.61	35.40	-5.05	-8.73 -13.69	
22	6	7995803	586402	-18.12485	129.81672	438.59	0.0000		978431.60	35.29	-5.13	-8.81 -13.77	
22	7	7995762	586392	-18.12522	129.81663	438.51	0.0000		978431.48	35.13	-5.29	-8.96 -13.92	
22	8	7995724	586403	-18.12557	129.81673	438.26	0.0000		978431.57	35.12	-5.28	-8.95 -13.91	
22	9	7995682	586399	-18.12595	129.81670	438.06	0.0000		978431.59	35.06	-5.32	-8.99 -13.94	
22	10	7995642	586401	-18.12631	129.81672	437.79	0.0000		978431.65	35.02	-5.33	-9.00 -13.95	
22	11	7995597	586402	-18.12671	129.81673	436.85	0.0000		978431.58	34.64	-5.63	-9.29 -14.23	
22	12	7995561	586395	-18.12704	129.81666	436.13	0.0000		978431.61	34.42	-5.78	-9.43 -14.36	
22	13	7995521	586388	-18.12740	129.81660	435.81	0.0000		978431.65	34.35	-5.82	-9.47 -14.40	
22	14	7995480	586399	-18.12777	129.81671	435.27	0.0000		978431.70	34.21	-5.91	-9.56 -14.48	
22	15	7995440	586406	-18.12813	129.81678	434.88	0.0000		978431.73	34.10	-5.98	-9.63 -14.55	
22	16	7995400	586404	-18.12849	129.81676	434.39	0.0000		978431.76	33.96	-6.08	-9.72 -14.63	
22	17	7995359	586396	-18.12887	129.81668	434.02	0.0000		978431.82	33.88	-6.12	-9.76 -14.67	
22	18	7995319	586402	-18.12922	129.81675	433.46	0.0000		978431.79	33.66	-6.29	-9.92 -14.82	
22	19	7995282	586396	-18.12956	129.81668	433.14	0.0000		978431.92	33.68	-6.24	-9.87 -14.77	
22	20	7995239	586403	-18.12995	129.81676	433.62	0.0000		978432.17	34.06	-5.91	-9.55 -14.45	
22	21	7995197	586399	-18.13033	129.81672	433.05	0.0000		978432.16	33.85	-6.06	-9.69 -14.59	
22	22	7995156	586398	-18.13069	129.81671	432.52	0.0000		978432.30	33.81	-6.06	-9.69 -14.58	
22	23	7995117	586402	-18.13105	129.81675	431.90	0.0000		978432.40	33.70	-6.11	-9.73 -14.62	
22	24	7995076	586404	-18.13142	129.81678	431.32	0.0000		978432.37	33.47	-6.28	-9.90 -14.78	
22	25	7995037	586395	-18.13178	129.81669	431.16	0.0000		978432.23	33.26	-6.48	-10.09 -14.97	
22	26	7994993	586397	-18.13217	129.81671	430.72	0.0000		978432.21	33.08	-6.62	-10.23 -15.10	

Line 271													
\Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD													
08-01-2002													
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\Line	Station	North	East	Latitude	Longitude	Elev	Ter	Cor	G obs.	Free Air	Bouguer	Gravity (mgals)	
\		metres	metres	dec deg	dec deg	metres			mgals	mgals	2.20g/cc	2.40g/cc	
\											2.40g/cc	2.67g/cc	
=====													
271	1	7994452	587111	-18.13703	129.82349	415.11	0.0000		978436.24	32.04	-6.22	-9.70	-14.40
271	2	7994448	587138	-18.13707	129.82374	415.23	0.0000		978436.26	32.09	-6.18	-9.66	-14.36
271	3	7994444	587180	-18.13710	129.82413	415.66	0.0000		978436.19	32.15	-6.16	-9.64	-14.34
271	4	7994452	587219	-18.13703	129.82450	415.80	0.0000		978436.25	32.26	-6.06	-9.55	-14.25
271	5	7994444	587260	-18.13709	129.82488	415.80	0.0000		978436.29	32.29	-6.03	-9.52	-14.22
271	6	7994447	587300	-18.13707	129.82526	415.91	0.0000		978436.36	32.40	-5.94	-9.42	-14.13
271	7	7994449	587338	-18.13705	129.82563	416.03	0.0000		978436.41	32.49	-5.86	-9.34	-14.05
271	8	7994446	587378	-18.13708	129.82600	416.57	0.0000		978436.30	32.54	-5.85	-9.34	-14.06
271	9	7994448	587418	-18.13705	129.82638	417.19	0.0000		978436.13	32.56	-5.89	-9.39	-14.10
271	10	7994449	587458	-18.13705	129.82676	417.31	0.0000		978436.17	32.64	-5.82	-9.32	-14.04
271	11	7994449	587499	-18.13704	129.82715	417.60	0.0000		978436.27	32.84	-5.66	-9.15	-13.88
271	12	7994452	587538	-18.13702	129.82752	417.74	0.0000		978436.33	32.94	-5.56	-9.06	-13.79
271	13	7994456	587578	-18.13698	129.82790	417.60	0.0000		978436.25	32.82	-5.67	-9.17	-13.89
271	14	7994443	587618	-18.13710	129.82828	417.97	0.0000		978436.22	32.89	-5.63	-9.14	-13.87
271	15	7994445	587658	-18.13707	129.82865	419.05	0.0000		978436.06	33.07	-5.55	-9.06	-13.80
271	16	7994454	587698	-18.13699	129.82903	419.73	0.0000		978435.84	33.07	-5.62	-9.14	-13.89
271	17	7994450	587739	-18.13703	129.82941	420.12	0.0000		978435.79	33.14	-5.59	-9.11	-13.86
271	18	7994450	587779	-18.13702	129.82979	420.65	0.0000		978435.85	33.35	-5.42	-8.94	-13.70
271	19	7994448	587819	-18.13704	129.83017	420.99	0.0000		978436.07	33.68	-5.12	-8.65	-13.41
271	20	7994456	587859	-18.13696	129.83055	421.39	0.0000		978436.30	34.04	-4.81	-8.34	-13.10
271	21	7994458	587903	-18.13695	129.83097	421.87	0.0000		978436.41	34.30	-4.59	-8.12	-12.89
271	22	7994449	587939	-18.13702	129.83131	422.13	0.0000		978436.48	34.45	-4.46	-8.00	-12.77
271	23	7994454	587981	-18.13698	129.83170	422.48	0.0000		978436.51	34.58	-4.36	-7.90	-12.68
271	24	7994454	588020	-18.13697	129.83208	422.80	0.0000		978436.48	34.65	-4.32	-7.86	-12.65
271	25	7994450	588057	-18.13701	129.83243	423.17	0.0000		978436.50	34.78	-4.22	-7.77	-12.55
271	26	7994449	588100	-18.13702	129.83283	423.60	0.0000		978436.48	34.90	-4.15	-7.69	-12.49

Line 272												
\Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD 08-01-2002												
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\Line	Station	North	East	Latitude	Longitude	Elev	Ter	Cor	G obs.	Free Air	Bouguer	Gravity (mgals)
\		metres	metres	dec deg	dec deg	metres			mgals	mgals	2.20g/cc	2.40g/cc 2.67g/cc
\		metres	metres	dec deg	dec deg	metres			mgals	mgals	2.20g/cc	2.40g/cc 2.67g/cc
=====												
272	1	7993952	587602	-18.14153	129.82815	421.70	0.0000		978435.21	32.80	-6.07	-9.61 -14.38
272	2	7993994	587599	-18.14115	129.82811	421.69	0.0000		978435.28	32.89	-5.98	-9.51 -14.28
272	3	7994034	587590	-18.14079	129.82803	422.60	0.0000		978435.20	33.11	-5.84	-9.38 -14.16
272	4	7994074	587596	-18.14043	129.82809	423.08	0.0000		978435.06	33.14	-5.86	-9.40 -14.19
272	5	7994116	587594	-18.14005	129.82806	423.14	0.0000		978435.06	33.17	-5.83	-9.38 -14.16
272	6	7994164	587599	-18.13961	129.82811	422.89	0.0000		978435.33	33.39	-5.59	-9.13 -13.91
272	7	7994195	587603	-18.13934	129.82814	422.28	0.0000		978435.52	33.40	-5.52	-9.06 -13.83
272	8	7994232	587594	-18.13900	129.82806	420.20	0.0000		978435.98	33.24	-5.49	-9.01 -13.77
272	9	7994273	587594	-18.13863	129.82805	419.37	0.0000		978436.13	33.16	-5.50	-9.01 -13.76
272	10	7994313	587595	-18.13827	129.82807	418.86	0.0000		978436.23	33.11	-5.49	-9.00 -13.74
272	11	7994352	587594	-18.13792	129.82805	418.65	0.0000		978436.19	33.03	-5.56	-9.07 -13.80
272	12	7994392	587598	-18.13756	129.82809	418.45	0.0000		978436.22	33.02	-5.55	-9.06 -13.79
272	13	7994431	587595	-18.13720	129.82806	418.40	0.0000		978436.31	33.12	-5.45	-8.95 -13.69
272	14	7994469	587591	-18.13686	129.82802	418.46	0.0000		978436.29	33.12	-5.45	-8.95 -13.69
272	15	7994506	587593	-18.13653	129.82803	418.83	0.0000		978436.25	33.22	-5.39	-8.90 -13.63
272	16	7994547	587596	-18.13615	129.82806	419.14	0.0000		978436.21	33.30	-5.34	-8.85 -13.59
272	17	7994586	587594	-18.13580	129.82804	419.31	0.0000		978436.32	33.48	-5.17	-8.68 -13.42
272	18	7994625	587589	-18.13545	129.82799	419.70	0.0000		978436.38	33.67	-5.01	-8.53 -13.28
272	19	7994667	587586	-18.13507	129.82796	420.25	0.0000		978436.36	33.84	-4.89	-8.41 -13.17
272	20	7994704	587595	-18.13473	129.82805	421.08	0.0000		978436.33	34.09	-4.72	-8.25 -13.01

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272	21	7994745	587593	-18.13437	129.82803	421.69	0.0000	978436.24	34.21	-4.66	-8.19	-12.96
272	22	7994787	587587	-18.13399	129.82797	422.17	0.0000	978436.16	34.30	-4.61	-8.15	-12.93
272	23	7994826	587597	-18.13363	129.82806	422.84	0.0000	978436.07	34.43	-4.54	-8.08	-12.87
272	24	7994865	587593	-18.13328	129.82801	423.33	0.0000	978436.04	34.57	-4.45	-8.00	-12.79
272	25	7994905	587595	-18.13292	129.82803	423.62	0.0000	978435.99	34.63	-4.42	-7.97	-12.76

Line 281

\Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD 08-01-2002

\Line	Station	North	East	Latitude	Longitude	Elev	Ter Cor	G obs.	Free Air	Bouguer	Gravity (mgals)		
\		metres	metres	dec deg	dec deg	metres	mgals	mgals	mgals	2.20g/cc	2.40g/cc	2.67g/cc	
\													
	281	1	7966305	555207	-18.39248	129.52266	380.39	0.0000	978456.49	27.86	-7.20	-10.39	-14.69
	281	2	7966337	555205	-18.39219	129.52264	380.95	0.0000	978456.34	27.90	-7.21	-10.41	-14.72
	281	3	7966381	555202	-18.39179	129.52261	381.62	0.0000	978456.01	27.79	-7.38	-10.58	-14.90
	281	4	7966420	555197	-18.39144	129.52256	382.21	0.0000	978455.70	27.69	-7.54	-10.74	-15.07
	281	5	7966459	555199	-18.39109	129.52258	382.72	0.0000	978455.50	27.66	-7.61	-10.82	-15.15
	281	6	7966495	555198	-18.39076	129.52257	383.24	0.0000	978455.38	27.72	-7.61	-10.82	-15.15
	281	7	7966541	555204	-18.39035	129.52262	383.96	0.0000	978455.23	27.82	-7.57	-10.79	-15.13
	281	8	7966581	555197	-18.38998	129.52256	384.48	0.0000	978455.15	27.92	-7.52	-10.74	-15.09
	281	9	7966619	555200	-18.38964	129.52258	384.86	0.0000	978454.94	27.84	-7.63	-10.86	-15.21
	281	10	7966658	555201	-18.38928	129.52259	385.44	0.0000	978454.80	27.90	-7.63	-10.86	-15.22
	281	11	7966698	555199	-18.38892	129.52257	385.93	0.0000	978454.62	27.89	-7.68	-10.91	-15.28
	281	12	7966738	555198	-18.38857	129.52256	386.29	0.0000	978454.52	27.92	-7.68	-10.92	-15.29
	281	13	7966784	555204	-18.38814	129.52262	386.56	0.0000	978454.49	28.00	-7.63	-10.87	-15.24
	281	14	7966818	555199	-18.38784	129.52257	386.81	0.0000	978454.41	28.01	-7.64	-10.88	-15.26
	281	16	7966906	555176	-18.38704	129.52235	387.63	0.0000	978454.19	28.08	-7.65	-10.89	-15.28
	281	17	7966939	555195	-18.38675	129.52252	387.95	0.0000	978454.04	28.05	-7.70	-10.96	-15.34
	281	18	7966980	555206	-18.38637	129.52263	388.38	0.0000	978453.95	28.11	-7.68	-10.94	-15.33
	281	19	7967019	555197	-18.38603	129.52254	388.89	0.0000	978453.82	28.16	-7.69	-10.95	-15.34
	281	20	7967059	555188	-18.38566	129.52246	389.42	0.0000	978453.66	28.19	-7.71	-10.97	-15.37
	281	21	7967100	555195	-18.38529	129.52253	389.75	0.0000	978453.55	28.20	-7.73	-10.99	-15.40
	281	22	7967138	555199	-18.38494	129.52256	390.22	0.0000	978453.49	28.30	-7.67	-10.94	-15.35
	281	23	7967178	555196	-18.38459	129.52253	390.68	0.0000	978453.39	28.36	-7.65	-10.93	-15.35
	281	24	7967218	555197	-18.38422	129.52254	391.14	0.0000	978453.25	28.39	-7.67	-10.94	-15.37
	281	25	7967260	555200	-18.38385	129.52257	391.70	0.0000	978453.20	28.53	-7.58	-10.86	-15.29
	281	26	7967297	555199	-18.38351	129.52256	392.27	0.0000	978453.13	28.65	-7.51	-10.79	-15.23

Line 282

\Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD 08-01-2002

\Line	Station	North	East	Latitude	Longitude	Elev	Ter	Cor	G obs.	Free Air	Bouguer	Gravity (mgals)	
\		metres	metres	dec deg	dec deg	metres			mgals	mgals	2.20g/cc	2.40g/cc	2.67g/cc
\													
282	1	7966796	555699	-18.38803	129.52730	381.66	0.0000		978456.04	28.05	-7.13	-10.33	-14.65
282	2	7966798	555658	-18.38801	129.52692	382.29	0.0000		978455.92	28.12	-7.12	-10.32	-14.65
282	3	7966793	555619	-18.38805	129.52655	382.76	0.0000		978455.81	28.15	-7.13	-10.34	-14.67
282	4	7966795	555580	-18.38804	129.52617	383.37	0.0000		978455.63	28.16	-7.17	-10.39	-14.72
282	5	7966797	555540	-18.38802	129.52579	383.80	0.0000		978455.46	28.12	-7.25	-10.47	-14.81
282	6	7966800	555501	-18.38800	129.52543	384.09	0.0000		978455.23	27.98	-7.42	-10.64	-14.99
282	7	7966793	555460	-18.38806	129.52504	384.38	0.0000		978455.05	27.89	-7.54	-10.76	-15.11
282	8	7966797	555415	-18.38803	129.52461	384.87	0.0000		978454.87	27.86	-7.62	-10.84	-15.19
282	9	7966799	555378	-18.38801	129.52426	385.21	0.0000		978454.74	27.84	-7.66	-10.89	-15.25
282	10	7966792	555337	-18.38807	129.52388	385.53	0.0000		978454.60	27.79	-7.74	-10.97	-15.33
282	11	7966792	555298	-18.38808	129.52350	385.96	0.0000		978454.53	27.85	-7.72	-10.96	-15.32
282	12	7966790	555258	-18.38810	129.52312	386.36	0.0000		978454.47	27.91	-7.70	-10.94	-15.31
282	13	7966789	555215	-18.38810	129.52272	386.57	0.0000		978454.53	28.04	-7.59	-10.83	-15.21
282	14	7966786	555176	-18.38813	129.52235	386.59	0.0000		978454.43	27.95	-7.69	-10.92	-15.30
282	15	7966792	555133	-18.38808	129.52194	386.67	0.0000		978454.29	27.83	-7.81	-11.05	-15.42
282	16	7966800	555097	-18.38801	129.52160	386.69	0.0000		978454.11	27.67	-7.98	-11.22	-15.59
282	17	7966799	555056	-18.38802	129.52122	386.63	0.0000		978454.07	27.60	-8.03	-11.27	-15.65
282	18	7966793	555009	-18.38807	129.52077	386.58	0.0000		978454.16	27.68	-7.96	-11.20	-15.57
282	19	7966809	554975	-18.38793	129.52045	386.69	0.0000		978454.10	27.65	-7.99	-11.23	-15.60
282	20	7966801	554934	-18.38800	129.52006	386.61	0.0000		978454.28	27.81	-7.83	-11.07	-15.44
282	21	7966807	554896	-18.38795	129.51970	386.71	0.0000		978454.15	27.72	-7.93	-11.17	-15.54
282	22	7966801	554858	-18.38801	129.51934	386.56	0.0000		978454.23	27.75	-7.88	-11.12	-15.50
282	23	7966791	554815	-18.38810	129.51893	386.42	0.0000		978454.28	27.75	-7.87	-11.11	-15.48
282	24	7966801	554777	-18.38800	129.51857	386.39	0.0000		978454.18	27.64	-7.98	-11.21	-15.58
282	25	7966794	554737	-18.38807	129.51819	386.09	0.0000		978454.28	27.64	-7.94	-11.18	-15.55
282	26	7966802	554697	-18.38800	129.51781	386.05	0.0000		978454.31	27.66	-7.92	-11.16	-15.52

Line 291

\Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD 08-01-2002

\Line	Station	North	East	Latitude	Longitude	Elev	Ter	Cor	G obs.	Free Air	Bouguer	Gravity (mgals)	
		metres	metres	dec deg	dec deg	metres		mgals	mgals	mgals	2.20g/cc	2.40g/cc	2.67g/cc
291	1	7955506	541201	-18.49040	129.39028	369.57	0.0000		978455.34	18.07	-15.99	-19.09	-23.27
291	2	7955539	541204	-18.49010	129.39031	369.43	0.0000		978455.30	18.00	-16.05	-19.14	-23.32
291	3	7955580	541207	-18.48972	129.39034	369.32	0.0000		978455.34	18.03	-16.01	-19.10	-23.28
291	4	7955621	541211	-18.48936	129.39038	369.15	0.0000		978455.28	17.94	-16.08	-19.18	-23.35
291	5	7955662	541214	-18.48899	129.39040	368.99	0.0000		978455.26	17.88	-16.13	-19.22	-23.39
291	6	7955700	541216	-18.48864	129.39042	368.82	0.0000		978455.20	17.79	-16.21	-19.30	-23.47
291	7	7955740	541216	-18.48828	129.39042	368.68	0.0000		978455.08	17.65	-16.33	-19.42	-23.59
291	8	7955781	541217	-18.48791	129.39043	368.51	0.0000		978455.08	17.61	-16.35	-19.44	-23.61
291	9	7955820	541217	-18.48755	129.39043	368.38	0.0000		978455.03	17.54	-16.41	-19.50	-23.67
291	10	7955861	541219	-18.48719	129.39045	368.25	0.0000		978455.00	17.49	-16.45	-19.54	-23.70
291	11	7955901	541220	-18.48682	129.39046	368.06	0.0000		978455.00	17.45	-16.47	-19.56	-23.72
291	12	7955941	541223	-18.48646	129.39048	367.91	0.0000		978454.83	17.26	-16.65	-19.73	-23.89
291	13	7955983	541227	-18.48608	129.39052	367.68	0.0000		978454.68	17.06	-16.83	-19.91	-24.07
291	14	7956021	541230	-18.48574	129.39055	367.49	0.0000		978454.61	16.95	-16.92	-20.00	-24.16
291	15	7956061	541233	-18.48538	129.39057	367.31	0.0000		978454.83	17.13	-16.73	-19.80	-23.96
291	16	7956100	541234	-18.48503	129.39058	367.19	0.0000		978454.86	17.14	-16.70	-19.78	-23.93
291	17	7956139	541238	-18.48467	129.39062	367.20	0.0000		978454.84	17.15	-16.70	-19.78	-23.93
291	18	7956180	541236	-18.48430	129.39060	367.26	0.0000		978454.86	17.20	-16.65	-19.72	-23.88

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291	19	7956222	541239	-18.48393	129.39062	367.11	0.0000	978454.84	17.16	-16.68	-19.75	-23.91
291	20	7956260	541240	-18.48358	129.39063	366.62	0.0000	978454.88	17.07	-16.72	-19.80	-23.94
291	21	7956300	541247	-18.48322	129.39070	366.29	0.0000	978454.90	17.01	-16.76	-19.83	-23.97
291	22	7956350	541253	-18.48276	129.39076	365.89	0.0000	978454.93	16.94	-16.79	-19.85	-23.99
291	23	7956386	541239	-18.48244	129.39063	365.61	0.0000	978454.96	16.90	-16.80	-19.86	-24.00
291	24	7956420	541231	-18.48213	129.39055	365.48	0.0000	978454.91	16.83	-16.86	-19.92	-24.06
291	25	7956460	541211	-18.48177	129.39036	365.32	0.0000	978454.86	16.74	-16.93	-19.99	-24.12
291	26	7956501	541201	-18.48140	129.39026	365.42	0.0000	978454.72	16.65	-17.03	-20.09	-24.22
Line 292												
\Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD 08-01-2002												
=====												
\Line	Station	North	East	Latitude	Longitude	Elev	Ter	Cor	G obs.	Free Air	Bouguer	Gravity (mgals)
\		metres	metres	dec deg	dec deg	metres			mgals	mgals	2.20g/cc	2.40g/cc 2.67g/cc
=====												
292	1	7956002	540699	-18.48592	129.38552	366.40	0.0000	978455.00	16.99	-16.78	-19.85	-23.99
292	2	7956002	540736	-18.48592	129.38587	366.37	0.0000	978455.03	17.01	-16.76	-19.83	-23.97
292	3	7956002	540776	-18.48592	129.38625	366.36	0.0000	978455.13	17.11	-16.66	-19.73	-23.87
292	4	7956001	540816	-18.48593	129.38663	366.42	0.0000	978455.17	17.17	-16.60	-19.68	-23.82
292	5	7956000	540857	-18.48594	129.38702	366.43	0.0000	978455.23	17.23	-16.54	-19.61	-23.76
292	6	7955999	540897	-18.48595	129.38739	366.48	0.0000	978455.14	17.15	-16.63	-19.70	-23.84
292	7	7955998	540939	-18.48595	129.38779	366.57	0.0000	978455.19	17.23	-16.56	-19.63	-23.77
292	8	7955998	540979	-18.48595	129.38817	366.75	0.0000	978455.14	17.24	-16.57	-19.64	-23.79
292	9	7955997	541019	-18.48596	129.38855	366.87	0.0000	978455.03	17.17	-16.65	-19.72	-23.87
292	10	7955996	541059	-18.48597	129.38893	366.96	0.0000	978455.07	17.24	-16.59	-19.66	-23.81
292	11	7955995	541100	-18.48598	129.38932	367.13	0.0000	978454.94	17.15	-16.68	-19.76	-23.91
292	12	7955995	541142	-18.48597	129.38971	367.27	0.0000	978454.48	16.74	-17.11	-20.19	-24.35
292	13	7955993	541180	-18.48600	129.39007	367.46	0.0000	978454.36	16.67	-17.20	-20.28	-24.43
292	14	7955988	541220	-18.48604	129.39045	367.63	0.0000	978454.61	16.97	-16.91	-19.99	-24.15
292	15	7955986	541260	-18.48606	129.39083	367.85	0.0000	978454.84	17.27	-16.63	-19.71	-23.88
292	16	7955983	541300	-18.48608	129.39121	368.21	0.0000	978454.97	17.51	-16.42	-19.51	-23.67
292	17	7955979	541339	-18.48612	129.39158	368.60	0.0000	978454.97	17.63	-16.34	-19.43	-23.60
292	18	7955976	541381	-18.48614	129.39198	369.17	0.0000	978454.84	17.67	-16.35	-19.45	-23.62
292	19	7955986	541422	-18.48606	129.39236	368.89	0.0000	978454.89	17.64	-16.36	-19.45	-23.62
292	20	7955979	541463	-18.48612	129.39275	368.65	0.0000	978454.93	17.60	-16.38	-19.47	-23.64
292	21	7955982	541490	-18.48609	129.39301	368.42	0.0000	978455.00	17.61	-16.35	-19.43	-23.60
292	22	7955982	541538	-18.48609	129.39346	368.06	0.0000	978455.03	17.53	-16.39	-19.48	-23.64
292	23	7955993	541580	-18.48599	129.39386	367.70	0.0000	978455.11	17.51	-16.39	-19.47	-23.63
292	24	7955998	541620	-18.48594	129.39425	367.42	0.0000	978455.23	17.54	-16.32	-19.40	-23.56
292	25	7956004	541658	-18.48589	129.39461	367.17	0.0000	978455.25	17.49	-16.36	-19.43	-23.59
292	26	7956008	541698	-18.48585	129.39498	366.96	0.0000	978455.28	17.45	-16.37	-19.45	-23.60
Line 301												
\Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD 08-01-2002												
=====												
\Line	Station	North	East	Latitude	Longitude	Elev	Ter	Cor	G obs.	Free Air	Bouguer	Gravity (mgals)
\		metres	metres	dec deg	dec deg	metres			mgals	mgals	2.20g/cc	2.40g/cc 2.67g/cc
=====												
301	1	7956502	542789	-18.48136	129.40530	366.17	0.0000	978454.52	16.69	-17.06	-20.13	-24.27
301	2	7956537	542789	-18.48105	129.40530	366.10	0.0000	978454.52	16.68	-17.06	-20.13	-24.27
301	3	7956576	542788	-18.48070	129.40529	366.05	0.0000	978454.49	16.66	-17.08	-20.15	-24.29
301	4	7956618	542787	-18.48032	129.40528	365.93	0.0000	978454.46	16.61	-17.12	-20.19	-24.33
301	5	7956659	542789	-18.47994	129.40530	365.86	0.0000	978454.49	16.64	-17.08	-20.15	-24.29
301	6	7956698	542798	-18.47959	129.40539	365.87	0.0000	978454.47	16.64	-17.08	-20.15	-24.29
301	7	7956738	542799	-18.47923	129.40539	365.79	0.0000	978454.44	16.60	-17.11	-20.18	-24.32
301	8	7956778	542798	-18.47887	129.40539	365.69	0.0000	978454.36	16.52	-17.19	-20.25	-24.39
301	9	7956819	542796	-18.47850	129.40536	365.71	0.0000	978454.23	16.41	-17.29	-20.36	-24.50
301	10	7956859	542801	-18.47814	129.40541	365.63	0.0000	978454.07	16.25	-17.45	-20.52	-24.65
301	11	7956898	542802	-18.47778	129.40542	365.67	0.0000	978453.83	16.04	-17.66	-20.72	-24.86
301	12	7956938	542805	-18.47742	129.40545	365.61	0.0000	978453.62	15.83	-17.87	-20.93	-25.07
301	13	7956978	542792	-18.47706	129.40532	365.53	0.0000	978453.58	15.78	-17.91	-20.97	-25.10
301	14	7957019	542791	-18.47669	129.40531	365.54	0.0000	978453.63	15.86	-17.83	-20.90	-25.03
301	15	7957058	542802	-18.47633	129.40541	365.53	0.0000	978453.70	15.95	-17.75	-20.81	-24.94
301	16	7957099	542799	-18.47597	129.40538	365.52	0.0000	978453.75	16.01	-17.68	-20.74	-24.88
301	17	7957139	542799	-18.47560	129.40539	365.51	0.0000	978453.73	16.01	-17.68	-20.74	-24.88
301	18	7957180	542803	-18.47523	129.40542	365.50	0.0000	978453.78	16.08	-17.61	-20.68	-24.81
301	19	7957218	542802	-18.47489	129.40541	365.50	0.0000	978453.75	16.06	-17.63	-20.69	-24.82
301	20	7957257	542797	-18.47454	129.40537	365.48	0.0000	978453.66	15.98	-17.70	-20.77	-24.90
301	21	7957299	542800	-18.47416	129.40539	365.47	0.0000	978453.57	15.91	-17.78	-20.84	-24.97
301	22	7957339	542800	-18.47380	129.40539	365.54	0.0000	978453.48	15.87	-17.82	-20.89	-25.02
301	23	7957380	542798	-18.47343	129.40537	365.55	0.0000	978453.43	15.84	-17.85	-20.91	-25.05
301	24	7957420	542799	-18.47307	129.40538	365.52	0.0000	978453.42	15.84	-17.85	-20.91	-25.05
301	25	7957461	542802	-18.47270	129.40541	365.46	0.0000	978453.37	15.79	-17.89	-20.95	-25.09
301	26	7957500	542798	-18.47234	129.40537	365.51	0.0000	978453.30	15.76	-17.93	-21.00	-25.13
Line 302												
\Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD 08-01-2002												
=====												
\Line	Station	North	East	Latitude	Longitude	Elev	Ter	Cor	G obs.	Free Air	Bouguer	Gravity (mgals)
\		metres	metres	dec deg	dec deg	metres			mgals	mgals	2.20g/cc	2.40g/cc 2.67g/cc
=====												
302	1	7956992	542296	-18.47694	129.40063	365.36	0.0000	978454.00	16.16	-17.52	-20.58	-24.71
302	2	7956997	542335	-18.47690	129.40100	365.33	0.0000	978453.98	16.13	-17.54	-20.61	-24.74
302	3	7956999	542376	-18.47687	129.40139	365.39	0.0000	978453.93	16.10	-17.58	-20.64	-24.77
302	4	7956999	542416	-18.47688	129.40176	365.48	0.0000	978454.01	16.21	-17.48	-20.54	-24.68
302	5	7957002	542457	-18.47686	129.40215	365.40	0.0000	978453.95	16.12	-17.56	-20.62	-24.75
302	6	7957001	542497	-18.47686	129.40252	365.45	0.0000	978453.93	16.12	-17.56	-20.63	-24.76
302	7	7957000	542535	-18.47687	129.40289	365.38	0.0000	978453.92	16.09	-17.59	-20.65	-24.78
302	8	7957002	542576	-18.47685	129.40328	365.49	0.0000	978453.86	16.06	-17.62	-20.69	-24.82
302	9	7957001	542613	-18.47685	129.40363	365.48	0.0000	978453.65	15.85	-17.84	-20.90	-25.03
302	10	7956997	542655	-18.47689	129.40403	365.50	0.0000	978453.64	15.8			

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302	15	7956998	542858	-18.47688	129.40594	365.63	0.0000	978453.64	15.88	-17.82	-20.88	-25.02
302	16	7956997	542896	-18.47688	129.40631	365.63	0.0000	978453.77	16.02	-17.68	-20.75	-24.88
302	17	7956997	542935	-18.47688	129.40667	365.65	0.0000	978453.90	16.16	-17.55	-20.61	-24.75
302	18	7956996	542976	-18.47689	129.40706	365.69	0.0000	978454.04	16.30	-17.40	-20.47	-24.60
302	19	7956995	543016	-18.47690	129.40745	365.70	0.0000	978454.13	16.40	-17.31	-20.37	-24.51
302	20	7956993	543056	-18.47692	129.40782	365.74	0.0000	978454.18	16.46	-17.25	-20.31	-24.45
302	21	7956990	543096	-18.47694	129.40820	365.79	0.0000	978454.22	16.51	-17.21	-20.27	-24.41
302	22	7956990	543135	-18.47695	129.40858	365.78	0.0000	978454.21	16.50	-17.22	-20.28	-24.42
302	23	7956991	543176	-18.47694	129.40896	365.80	0.0000	978454.28	16.58	-17.14	-20.21	-24.34
302	24	7956989	543215	-18.47696	129.40933	365.85	0.0000	978454.29	16.60	-17.12	-20.18	-24.32
302	25	7956989	543255	-18.47696	129.40971	365.90	0.0000	978454.38	16.70	-17.02	-20.09	-24.23
302	26	7956998	543303	-18.47687	129.41016	365.86	0.0000	978454.45	16.77	-16.95	-20.02	-24.16
Line 331												
\Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD 08-01-2002												
=====												
\Line	Station	North	East	Latitude	Longitude	Elev	Ter Cor	G obs.	Free Air	Bouguer	Gravity (mgals)	
\		metres	metres	dec deg	dec deg	metres	mgals	mgals	mgals	2.20g/cc	2.40g/cc	2.67g/cc
=====												
331	1	7960497	569604	-18.44454	129.65916	368.51	0.0000	978464.51	29.39	-4.57	-7.66	-11.83
331	2	7960537	569603	-18.44418	129.65915	368.59	0.0000	978464.49	29.42	-4.55	-7.64	-11.81
331	3	7960577	569602	-18.44382	129.65913	368.67	0.0000	978464.50	29.48	-4.51	-7.59	-11.77
331	4	7960617	569602	-18.44346	129.65912	368.70	0.0000	978464.48	29.49	-4.50	-7.59	-11.76
331	5	7960657	569600	-18.44309	129.65911	368.86	0.0000	978464.45	29.53	-4.47	-7.56	-11.74
331	6	7960697	569599	-18.44274	129.65910	369.10	0.0000	978464.42	29.59	-4.43	-7.52	-11.70
331	7	7960737	569602	-18.44237	129.65912	369.40	0.0000	978464.37	29.65	-4.40	-7.49	-11.67
331	8	7960776	569602	-18.44202	129.65912	369.65	0.0000	978464.30	29.68	-4.39	-7.49	-11.67
331	9	7960817	569601	-18.44165	129.65911	369.98	0.0000	978464.16	29.66	-4.44	-7.54	-11.73
331	10	7960858	569599	-18.44128	129.65909	370.36	0.0000	978464.00	29.63	-4.50	-7.61	-11.80
331	11	7960897	569601	-18.44093	129.65911	370.76	0.0000	978463.84	29.61	-4.56	-7.67	-11.86
331	12	7960937	569600	-18.44057	129.65910	371.07	0.0000	978463.72	29.61	-4.59	-7.70	-11.90
331	13	7960977	569602	-18.44021	129.65912	371.33	0.0000	978463.56	29.56	-4.67	-7.78	-11.98
331	14	7961017	569600	-18.43985	129.65910	371.56	0.0000	978463.42	29.50	-4.74	-7.86	-12.06
331	15	7961057	569601	-18.43948	129.65910	371.77	0.0000	978463.45	29.62	-4.65	-7.76	-11.97
331	16	7961097	569604	-18.43912	129.65913	372.04	0.0000	978463.37	29.64	-4.65	-7.77	-11.97
331	17	7961139	569599	-18.43874	129.65908	372.32	0.0000	978463.26	29.64	-4.68	-7.80	-12.01
331	18	7961179	569601	-18.43838	129.65910	372.67	0.0000	978463.17	29.68	-4.67	-7.80	-12.01
331	19	7961218	569599	-18.43803	129.65908	372.99	0.0000	978463.03	29.65	-4.73	-7.85	-12.07
331	20	7961259	569599	-18.43766	129.65908	373.25	0.0000	978462.98	29.70	-4.70	-7.83	-12.05
331	21	7961298	569600	-18.43730	129.65908	373.55	0.0000	978462.88	29.71	-4.72	-7.85	-12.08
331	22	7961336	569601	-18.43696	129.65910	373.86	0.0000	978462.81	29.75	-4.70	-7.84	-12.07
331	23	7961378	569601	-18.43658	129.65909	374.19	0.0000	978462.73	29.81	-4.68	-7.82	-12.05
331	24	7961419	569600	-18.43621	129.65909	374.54	0.0000	978462.59	29.79	-4.73	-7.87	-12.11
331	25	7961458	569602	-18.43586	129.65910	374.86	0.0000	978462.58	29.90	-4.65	-7.79	-12.03
331	26	7961498	569601	-18.43549	129.65908	375.29	0.0000	978462.52	29.99	-4.60	-7.74	-11.99
331	27	7961537	569601	-18.43515	129.65909	375.59	0.0000	978462.48	30.06	-4.56	-7.70	-11.95
331	28	7961578	569601	-18.43477	129.65909	375.94	0.0000	978462.49	30.20	-4.45	-7.60	-11.85
331	29	7961622	569600	-18.43438	129.65907	376.40	0.0000	978462.48	30.35	-4.34	-7.49	-11.75
331	30	7961659	569599	-18.43404	129.65906	376.71	0.0000	978462.45	30.44	-4.29	-7.44	-11.70
331	31	7961700	569601	-18.43367	129.65908	377.17	0.0000	978462.41	30.56	-4.21	-7.37	-11.63
Line 332												
\Bouguer Gravity Data collected and processed by Fugro Ground Geophysics PTY LTD 08-01-2002												
=====												
\Line	Station	North	East	Latitude	Longitude	Elev	Ter Cor	G obs.	Free Air	Bouguer	Gravity (mgals)	
\		metres	metres	dec deg	dec deg	metres	mgals	mgals	mgals	2.20g/cc	2.40g/cc	2.67g/cc
=====												
332	1	7961104	569006	-18.43908	129.65347	370.21	0.0000	978464.70	30.41	-3.71	-6.81	-11.00
332	2	7961104	569037	-18.43907	129.65376	370.34	0.0000	978464.61	30.36	-3.78	-6.88	-11.07
332	3	7961104	569078	-18.43908	129.65415	370.52	0.0000	978464.60	30.40	-3.75	-6.85	-11.04
332	4	7961101	569119	-18.43910	129.65454	370.64	0.0000	978464.55	30.39	-3.77	-6.88	-11.07
332	5	7961103	569157	-18.43908	129.65490	370.83	0.0000	978464.54	30.44	-3.74	-6.85	-11.05
332	6	7961105	569197	-18.43907	129.65527	371.04	0.0000	978464.47	30.43	-3.77	-6.88	-11.08
332	7	7961103	569236	-18.43908	129.65565	371.19	0.0000	978464.27	30.28	-3.93	-7.04	-11.24
332	8	7961102	569277	-18.43909	129.65603	371.35	0.0000	978464.25	30.31	-3.92	-7.03	-11.23
332	9	7961102	569316	-18.43909	129.65640	371.49	0.0000	978464.23	30.33	-3.91	-7.02	-11.22
332	10	7961103	569358	-18.43908	129.65680	371.60	0.0000	978464.18	30.31	-3.94	-7.05	-11.25
332	11	7961101	569398	-18.43909	129.65718	371.70	0.0000	978464.07	30.23	-4.03	-7.14	-11.35
332	12	7961101	569437	-18.43909	129.65755	371.81	0.0000	978463.97	30.17	-4.10	-7.21	-11.42
332	13	7961101	569477	-18.43909	129.65792	371.87	0.0000	978463.80	30.02	-4.26	-7.37	-11.58
332	14	7961100	569517	-18.43910	129.65830	371.92	0.0000	978463.63	29.87	-4.41	-7.53	-11.74
332	15	7961098	569557	-18.43911	129.65869	371.95	0.0000	978463.44	29.68	-4.60	-7.72	-11.92
332	16	7961097	569603	-18.43912	129.65912	372.02	0.0000	978463.40	29.66	-4.63	-7.74	-11.95
332	17	7961098	569638	-18.43911	129.65945	372.07	0.0000	978463.44	29.72	-4.58	-7.69	-11.90
332	18	7961101	569678	-18.43908	129.65983	372.17	0.0000	978463.41	29.72	-4.59	-7.70	-11.91
332	19	7961099	569719	-18.43910	129.66022	372.22	0.0000	978463.34	29.67	-4.64	-7.76	-11.97
332	20	7961099	569757	-18.43910	129.66058	372.26	0.0000	978463.36	29.70	-4.61	-7.73	-11.94
332	21	7961099	569797	-18.43910	129.66096	372.34	0.0000	978463.41	29.78	-4.54	-7.66	-11.87
332	22	7961099	569838	-18.43910	129.66135	372.43	0.0000	978463.44	29.83	-4.49	-7.61	-11.83
332	23	7961098	569876	-18.43910	129.66171	372.64	0.0000	978463.54	30.00	-4.35	-7.47	-11.69
332	24	7961097	569917	-18.43911	129.66209	372.78	0.0000	978463.66	30.16	-4.20	-7.32	-11.54
332	25	7961096	569958	-18.43912	129.66249	372.94	0.0000	978463.73	30.28	-4.09	-7.22	-11.44
332	26	7961098	569999	-18.43910	129.66287	373.17	0.0000	978463.81	30.43	-3.96	-7.09	-11.31
332	27	7961096	570037	-18.43912	129.66323	373.28	0.0000	978463.91	30.57	-3.84	-6.97	-11.19
332	28	7961095	570078	-18.43913	129.66361	373.45	0.0000	978463.86	30.56	-3.86	-6.99	-11.21
332	29	7961097	570117	-18.43910	129.66399	373.70	0.0000	978463.83	30.61	-3.83	-6.96	-11.19
332	30	7961095	570156	-18.43912	129.66436	373.75	0.0000	978463.85	30.64	-3.80	-6.94	-11.16
332	31	7961097	570198	-18.43910	129.66476	373.89	0.0000	978463.84	30.68	-3.78	-6.92	-11.15